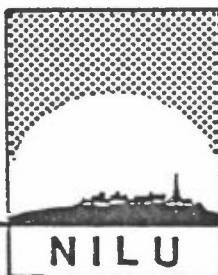


NILU OR : 32/84
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DATO : JUNI 1984

**METEOROLOGISKE DATA FRA
NEDRE TELEMARK, HØSTEN 1983**

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SAMMENDRAG

De meteorologiske målingene fra nedre Telemark i perioden 1.9.83-30.11.83 er presentert. Vinddataene viser en vindretningsfordeling som likner på fordelingen for de siste fem års høstperioder. Vind fra nord-nordvest og sørvest var imidlertid noe mer dominerende enn vanlig. Gjennomsnittlig vindstyrke, 3.2 m/s, var noe høyere enn normalt.

September hadde dobbelt så mye nedbør som en normal september måned. Oktober og november hadde mindre nedbør enn normalt. Oktober var ca 1.5°C varmere enn gjennomsnittet for de ti siste åra, mens temperaturen i september og november var nær gjennomsnittet.

Fordelingen av stabilitetsklassene var nær 10 års-snittet.

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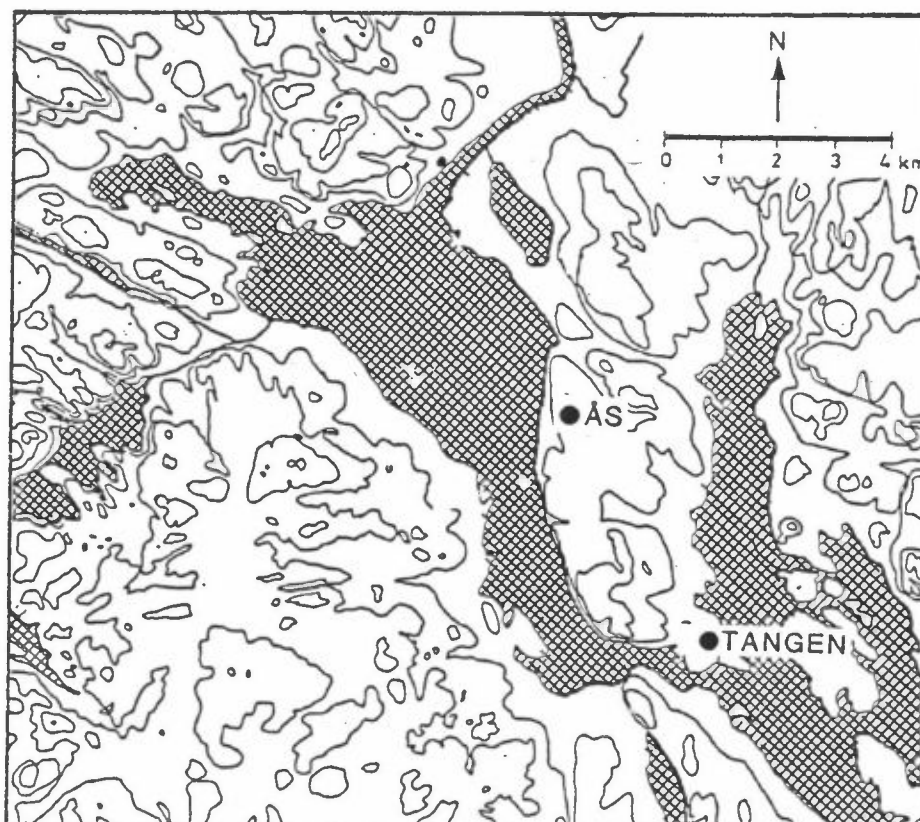
METEOROLOGISKE DATA FRA NEDRE TELEMARK. HØSTEN 1983

1 INNLEDNING

Denne presentasjonen av meteorologiske data fra nedre Telemark i perioden 1.9.83-30.11.83 (høst), er et ledd i det koordinerte måleprogram av meteorologi og spredningsforhold i området. Bearbeidelsen er utført på oppdrag fra Statens forurensningstilsyn, kontrollseksjonen nedre Telemark, og er en videreføring av tidligere tilsendte data (se Referanselisten).

2 INSTRUMENTERING, STASJONSPLASSERING

Målestasjonenes plassering er angitt i figur 1.



Figur 1: Lokalisering av meteorologiske målestasjoner i nedre Telemark.

Følgende instrumentering er anvendt ved de forskjellige stasjonene:

Ås : NILU automatiske værstasjon (AWS) med 25 m høy mast hvor det timevis måles: vindretning og vindstyrke (i 25 m), temperatur og relativ fuktighet (i 3 m), stabilitet (temperaturforskjell mellom 25 og 10 m). Stasjonene er plassert 90 m o.h.

Tangen,

Brevik : Pluviograf av type Fuess nr 95 nach Hellmann (hevert-pluviograf) plassert ca 20 m o.h.
Termohygrograf av type Fuess plassert 2 m over bakken ca 20 m o.h. med timevise målinger av temperatur og fuktighet.

3 DATAKVALITET

Datatilgjengeligheten ved Ås for denne perioden var god. Pluviografdataene fra Tangen, Brevik, manglet for mer enn halve september samt for korte perioder i oktober og november. Datatilgjengeligheten for perioden var følgende:

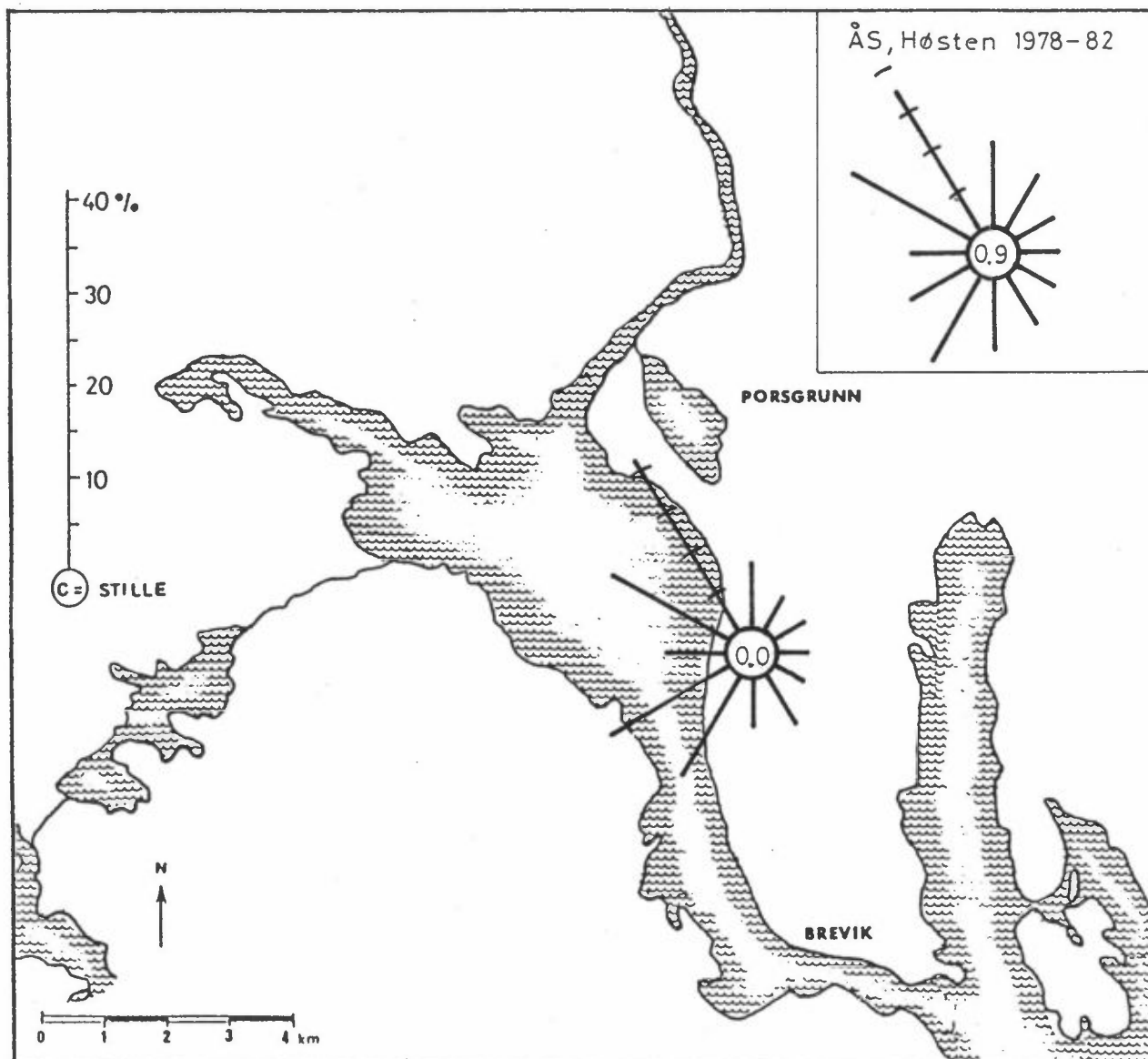
Ås : 99.8% for vindstyrke, vindretning, temperaturdifferens og relativ fuktighet.
99.4% for vindretning og vindhastighet.
99.7% for temperatur.

Tangen,

Brevik : 79.9% for nedbør.
99.4% for relativ fuktighet
98.7% for temperatur

4 VINDFORHOLDENE

Vindrose fra Ås for høsten 1983 er vist i figur 2 sammen med rosen for femårsperioden 1978-82.



Figur 2: Vindrose (frekvens av vind i % i 12 sektorer) fra Ås for perioden 1.9.83-30.11.83 og høstperiodene 1978-82.

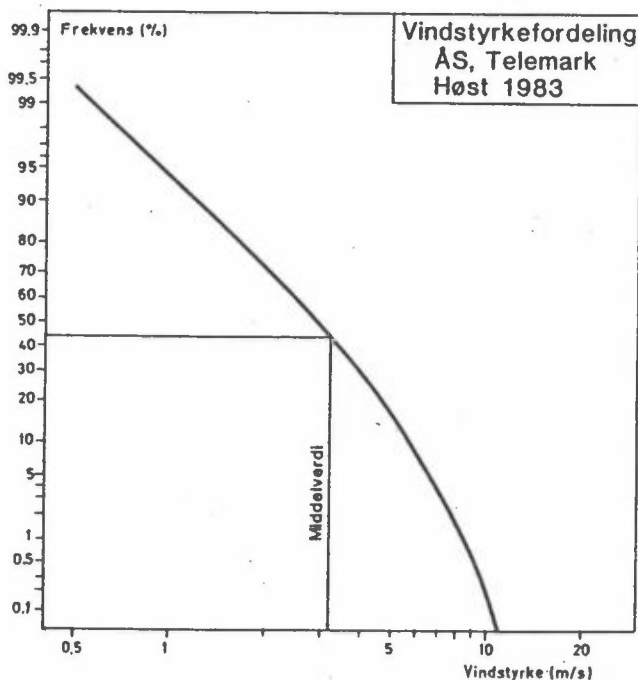
Kvartalsvise vindfrekvensfordelinger (i %) er også presentert i tabellene A.1-2. Vindobservasjoner fra Ås er dessuten presentert som månedsvise frekvensfordelinger i tabell A.9.

Høsten 1983 blåste det oftest fra nordvestlig kant ved Ås. Dette stemmer godt med målinger foretatt i tidligere høstperioder. Vind fra nord-nordvest var imidlertid noe mer dominerende enn vanlig. Det samme gjelder også vind fra vest-sørvest.

Dominerende vindretning ved Ås var i september og november nord-nordvest og i oktober vest-sørvest.

Middelvindstyrken stemte bra med det som er målt i området høst-periodene 1978-82. Middelvindstyrken ved Ås høsten 1983 var imidlertid noe høyere (3.2 m/s) enn høstene 1978-82 (2.9 m/s). Gjennomsnittlig vindstyrke for september 1983 var 3.0 m/s, oktober 3.6 m/s og november 3.1 m/s.

Figur 3 viser vindstyrkefordelingen ved Ås.



Figur 3: Kumulativ frekvensfordeling av vindstyrke ved Ås høsten 1983. Figuren viser frekvens av vindstyrke større enn verdiene angitt på x-aksen.

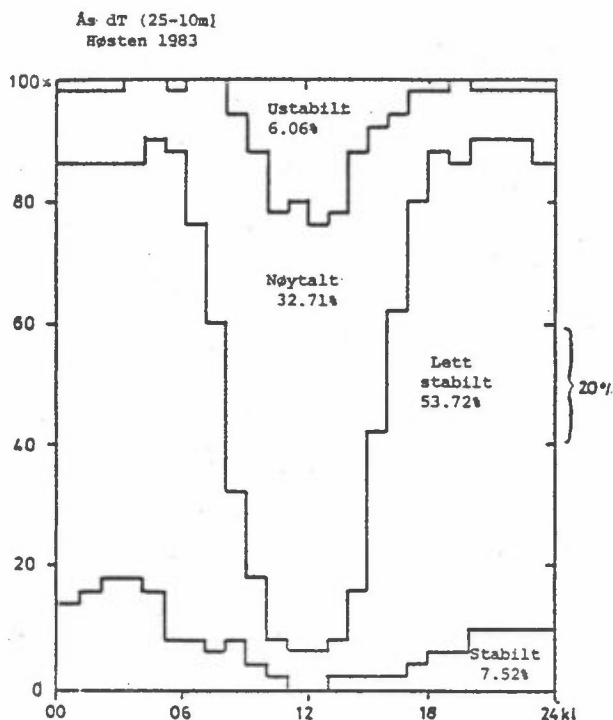
Vindstyrker over 6 m/s ved Ås forekom i 8.1% av tiden. Svake vinder, mindre enn 2 m/s forekom i 22.9% av tiden. I gjennomsnitt blåste det svakest fra nordlig kant ved Ås. Kraftigst blåste det fra vest-sørvest. Det var ingen observasjoner av vindstille ved Ås høsten 1983.

5 STABILITETSFORHOLDENE

Stabilitetsforholdene i fire klasser er fordelt over døgnet i tabell A.3 og A.10, og i figur 4 basert på temperaturdifferansen 25-10 m på Ås (dT).

Ustabil : $dT < -0.5$
 Nøytral : $-0.5 \leq dT < 0$
 Lett stabilt : $0 \leq dT < 0.5$
 Stabilt : $dT > 0.5$

Høsten 1983 var det 7.5% stabil, 53.7% lett stabil, 32.7% nøytral og 6.0% ustabil sjikting. Denne fordelingen gir tilnærmet den samme frekvens av de forskjellige stabilitetsforhold som det som har vært vanlig tidligere.



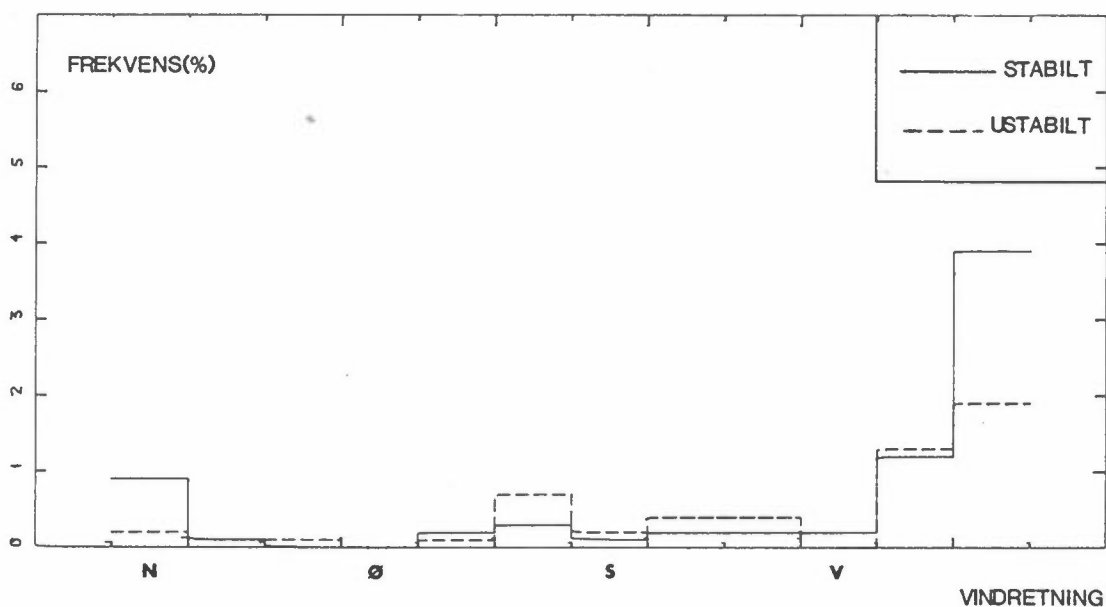
Figur 4: Døgnfordelingen av fire stabilitetsklasser basert på målinger av temperaturforskjellen mellom 25 m og 10 m i masten på Ås 1.9.83-30.11.83.

6 FREKVENS AV VIND/STABILITET

Tabell A.4 og A.11 viser frekvensen (i %) i 196 klasser av vind og stabilitet, basert på stabilitetsdata og vinddata fra 25 m masta på Ås.

Figur 5 viser frekvensen av stabil sjikting (inversjoner) og ustabil sjikting som funksjon av vindretningen.

FREKVENS AV STABILE OG USTABILE SITUASJONER ÅS, TELEMARCK



Figur 5: Frekvens av stabil og ustabil sjikting som funksjon av vindretningen ved Ås høsten 1983.

Figur 5 viser at ustabile tilfeller høsten 1983 oftest forekom ved vind fra nord-nordvest på Ås. Dette kommer av at denne vindretningen vanligvis totalt sett er den som forekommer oftest om høsten. Dette gjelder også for høsten 1983. Tabell A.4 viser at stabil sjikting oftest forekom ved vindhastigheter på 2-4 m/s fra nord-nordvestlig kant.

7 TEMPERATUR

Tabell A.5 og A.6 viser månedsvise temperatursammendrag for henholdsvis Ås og Brevik i perioden 1.9.83-30.11.83. Middelttemperaturen for september var ved Ås 12.2°C , oktober 7.5°C og for november 1.9°C . Middelttemperaturen for september og november var nær normaltemperaturen for de 10 siste åra. Oktober var imidlertid svært varm, og middelttemperaturen var hele 1.5°C høyere enn 10-årsnormalen. Den høyeste temperaturen ble målt den 1.9.83 kl 17 til 21.9°C . Den laveste temperaturen ble målt den 30.11.83 kl 24 til -8.7°C .

Middelttemperaturen for september var ved Brevik 11.4°C , oktober 7.7°C og for november 2.3°C . Middelttemperaturene er svært like de ved Ås, men en aning høyere mot slutten av perioden. Den høyeste temperaturen ble målt den 1.9.83 kl 16 til 22.0°C . Den laveste temperaturen ble målt den 30.11.83 kl 24 til -9.2°C .

8 RELATIV FUKTIGHET

Tabell A.7 og A.8 viser en statistisk fordeling av den relative fuktigheten ved henholdsvis Ås og Brevik for høsten 1983. Månedsmiddelveiene viser relativ fuktighet på henholdsvis 83% og 78% i september, 76% og 77% i oktober og 78% og 80% i november. Av observasjonene for høsten 1983 lå henholdsvis 30% og 22% over 95% relativ fuktighet. Målingene for perioden synes å stemme godt med målinger i høstperiodene 1973-82. I september varierer den relative fuktigheten i gjennomsnitt fra henholdsvis 71% og 63% midt på dagen til henholdsvis 93% og 92% om natta. I oktober varierte den fra 64% og 63% til 85% og 86%, og i november var variasjonen fra 71% og 72% til 83% og 85% relativ fuktighet.

9 NEDBØR

Kontinuerlige nedbørmålinger fra Tangen ved Brevik er presentert i vedlegg C. Tabell 1 viser månedsvise nedbørmengder fra Tangen og fra Meteorologisk institutts klima- stasjon ved Jomfruland (hvor det også er etablert en 30-års normal som en kan sammenlikne med). Datatilgjengeligheten fra Tangen Brevik for høstsesongen er ikke spesielt god. Spesielt for september er den dårlig.

Jomfrulanddataene viser at det i september falt det dobbelte av normal nedbør. Oktober lå litt under normalen, mens november var svært nedbørfattig med bare ca 1/3 av normal nedbørmengde.

Ifølge de dataene vi har, falt det ved Tangen i september 21 mm nedbør fordelt på 26 timer (over 6 døgn) og i oktober 32 mm på 55 timer (fordelt på 5 døgn).

Både i oktober og november (hvor dataene fra Tangen er relativt bra), regnet det tildels betydelig mindre ved Tangen enn ved Jomfruland.

Tabell 1: Nedbørmålinger fra Tangen, Brevik og Jomfruland i
a) sep. 1983, b) okt. 1983, c) nov. 1983.

	Tangen, Brevik				Jomfruland		
	Mengde mm	Antall timer med nedbør	Antall registr. timer	Nedbør timer i %	Antall døgn med nedbør	Mengde mm	% normal
Sep.-83	21	26	386	6.7	20	191	201
Okt.-83	32	55	673	8.1	19	85	89
Nov.-83	16	27	687	3.9	8	32	29

10 REFERANSER

- (1) Arnesen, K. Meteorologiske data fra nedre Telemark*)
 Friberg, A.G. Lillestrøm 1978-84.
 Sivertsen, B. (NILU OR).
 Skaug, K.

Periode:	Rapport nr.
Høsten 1977	OR 8/78
Vinteren 1977-78	OR 21/78
Våren 1978	OR 9/79
Sommeren 1978	OR 12/79
Høsten 1978	OR 13/79
Vinteren 1978-79	OR 27/79
Våren 1979	OR 30/79
Sommeren 1979	OR 3/80
Høsten 1979	OR 10/80
Vinteren 1979-80	OR 18/80
Våren 1980	OR 39/80
Sommeren 1980	OR 2/81
Høsten 1980	OR 15/81
Vinteren 1980-81	OR 21/81
Våren 1981	OR 48/81
Sommeren 1981	OR 11/82
Høsten 1981	OR 51/82
Vinteren 1981-82	OR 2/83
Våren 1982	OR 8/83
Sommeren 1982	OR 11/83
Høsten 1982	OR 22/83
Vinteren 1982-83	OR 39/83
Våren 1983	OR 58/83
Sommeren 1983	OR 3/84

VEDLEGG A

Tabeller

- Tabell A.1: Vindfrekvenser (vindrose) fra Ås 1.9.83-30.11.83).
- Tabell A.2: Vindfrekvenser (vindrose) fra Ås høstperiodene 1978-82.
- Tabell A.3: Fire klasser av stabiliteter fordelt over døgnet basert på målinger av temperaturforskjellen mellom 25 m og 10 m i masta på Ås 1.9.83-30.11.83.
- Tabell A.4: Frekvens (i %) av vind og stabilitet fordelt på: fire vindstyrkeklasser og fire stabilitetsklasser (1 = instabilt, 2 = nøytralt, 3 = lett stabilt, 4 = stabilt) vindstille (vind < 0.2 m/s) Basert på data fra Ås i perioden 1.9.83-30.11.83.
- Tabell A.5: Månedsvis temperaturstatistikk fra Ås for sep., okt. og nov. 1983: Middel-, maksimum- og minimumtemperaturer, antall observasjoner og temperatur under gitte grenser, samt midlere døgnfordeling av temperatur.
- Tabell A.6: Månedsvis temperaturstatistikk fra Tangen, Brevik for sep., okt. og nov. 1983: Middel-, maksimum- og minimumtemperaturer, antall observasjoner og temperatur under gitte grenser, samt midlere døgnfordeling av temperatur.
- Tabell A.7: Månedsvis relativ fuktighets-statistikk fra Ås for sep., okt. og nov. 1983. Middel-, maksimum og minimumverdier, antall observasjoner av relativ fuktighet under gitte grenser, samt midlere døgnfordeling.
- Tabell A.8: Månedsvis relativ fuktighetsstatistikk fra Tangen, Brevik for sep., okt. og nov. 1983. Middel-, maksimum og minimumsverdier, antall observasjoner av relativ fuktighet under gitte grenser, samt midlere døgnfordeling.
- Tabell A.9: a) Vindfrekvenser fra Ås for september 1983.
b) Vindfrekvenser fra Ås for oktober 1983.
c) Vindfrekvenser for Ås for november 1983.
- Tabell A.10: Månedsvis stabilitetsfrekvens (i fire klasser) fordelt over døgnet, basert på målinger av temperaturforskjellen mellom 25 m og 10 m i masta på Ås: a) sep. 1983, b) okt. 1983, c) nov. 1983.
- Tabell A.11: Frekvens (i %) av vind og stabilitet fra Ås (klassifisering som tabell 4) i
a) sep. 1983, b) okt. 1983, c) nov. 1983.

Tabell A.1: Vindfrekvenser (vindrose) fra Ås 1.9.83-30.11.83).

VINDROSE FRA ÅS													
1/ 9-83 - 30/11-83													
SEKTOR	VINDROSE KL.									DØGN			
	1	4	7	10	13	16	19	22					
20- 40	3.3	1.1	6.6	4.4	3.4	3.3	4.4	2.2	3.9				
50- 70	4.4	3.3	4.4	1.1	1.1	2.2	3.3	5.5	3.7				
80-100	1.1	4.4	.0	4.4	4.5	3.3	3.3	2.2	2.9				
110-130	4.4	4.4	2.2	1.1	5.6	5.5	3.3	.0	3.3				
140-160	5.5	6.7	6.6	7.8	9.0	7.7	6.7	4.4	6.3				
170-190	2.2	4.4	4.4	1.1	5.6	7.7	8.9	5.5	5.3				
200-220	12.1	11.1	11.0	15.6	9.0	12.1	13.3	13.2	12.3				
230-250	13.2	13.3	7.7	16.7	20.2	14.3	16.7	18.7	14.3				
260-280	9.9	10.0	5.5	4.4	5.6	5.5	6.7	7.7	6.2				
290-310	9.9	12.2	15.4	14.4	13.5	15.4	12.2	12.1	14.3				
320-340	26.4	18.9	30.8	22.2	15.7	16.5	17.8	22.0	21.2				
350- 10	7.7	10.0	5.5	6.7	6.7	6.6	3.3	6.6	6.5				
STILLE	.0	.0	.0	.0	.0	.0	.0	.0	.0				
ANT. OBS.	91	90	91	90	89	91	90	91	2174				
MIDL.VIND	3.2	2.9	2.8	3.3	3.5	3.6	3.3	3.2	3.2				
VINDANALYSE													
DØGNMIDDEL	30	60	90	120	150	180	210	240	270	300	330	360	TOTAL
STILLE													.0
.3- 2.0 M/S	1.7	1.3	1.3	1.7	2.2	1.8	2.3	3.1	2.0	3.4	6.1	2.6	29.5
2.1- 4.0 M/S	1.5	1.6	.9	1.1	3.0	2.0	5.1	4.0	2.0	6.0	12.3	2.9	42.5
4.1- 6.0 M/S	.6	.6	.6	.4	.6	.9	4.1	5.5	1.3	2.7	2.0	.7	20.1
OVER 6.0 M/S	.2	.2	.0	.0	.5	.6	.8	1.7	.8	2.2	.7	.2	7.9
TOTAL	3.9	3.7	2.9	3.3	6.3	5.3	12.3	14.3	6.2	14.3	21.2	6.5	100.0
MIDL.VIND M/S	2.8	2.8	2.6	2.3	3.0	3.2	3.6	3.9	3.4	3.6	2.8	2.6	3.2
ANT. OBS.	85	80	63	71	137	115	268	310	134	310	460	141	2174
MIDLERE VINDSTYRKE FOR HELE DATASETTET ER 3.2 M/S, BASERT PÅ 2180 OBSERVASJONER													

Tabell A.2: Vindfrekvenser (vindrose) fra Ås høstperiodene 1978-82.

VINDROSE FRA ÅS													
1/ 9-78 - 30/11-78													
1/ 9-79 - 30/11-79													
1/ 9-80 - 30/11-80													
1/ 9-81 - 30/11-81													
1/ 9-82 - 30/ 9-82													
1/10-82 - 31/10-82													
1/11-82 - 30/11-82													
SEKTOR	VINDROSE KL.									DØGN			
	1	4	7	10	13	16	19	22					
20- 40	6.6	5.8	6.3	6.7	6.4	8.7	6.4	6.4	6.8				
50- 70	3.2	5.6	6.1	4.9	4.4	5.2	5.4	3.7	4.7				
80-100	3.6	3.6	4.6	4.4	4.7	5.0	3.2	5.6	4.2				
110-130	2.9	4.4	5.4	5.4	7.4	6.7	5.9	4.2	5.1				
140-160	4.9	4.4	4.9	4.9	9.1	8.9	7.6	4.9	6.2				
170-190	7.5	5.4	4.4	5.9	6.9	13.6	9.8	7.8	7.8				
200-220	12.7	8.5	9.0	10.1	8.6	11.9	13.3	10.3	10.5				
230-250	7.3	9.2	7.3	7.1	8.4	5.7	7.4	8.6	7.3				
260-280	5.1	5.8	4.4	3.2	7.1	6.2	8.1	6.6	5.9				
290-310	15.8	16.1	15.4	16.5	11.3	9.4	11.1	15.4	14.2				
320-340	21.4	20.7	20.7	19.7	16.5	9.9	12.3	17.6	17.0				
350- 10	8.3	9.7	10.5	10.3	8.4	7.7	8.6	7.6	9.3				
STILLE	.7	.7	1.0	.7	1.0	1.0	1.0	1.2	.9				
ANT. OBS.	411	411	410	406	407	403	407	408	9784				
MIDL.VIND	2.8	2.8	2.8	2.9	3.2	3.2	3.0	2.9	2.9				
VINDANALYSE													
DØGNMIDDEL	30	60	90	120	150	180	210	240	270	300	330	360	TOTAL
STILLE													.9
.3- 2.0 M/S	1.8	1.8	1.7	2.2	2.5	2.2	2.2	2.1	2.1	4.9	7.5	3.2	34.2
2.1- 4.0 M/S	3.1	1.9	1.4	2.0	2.1	4.0	4.7	3.0	1.8	6.8	7.6	3.6	42.2
4.1- 6.0 M/S	1.6	.8	.9	.6	1.2	1.2	3.0	1.6	1.3	1.6	1.4	2.1	17.2
OVER 6.0 M/S	.2	.2	.2	.3	.5	.3	.6	.5	.7	1.0	.5	.5	5.5
TOTAL	6.8	4.7	4.2	5.1	6.2	7.8	10.5	7.3	5.9	14.2	17.0	9.3	100.0
MIDL.VIND M/S	3.1	2.8	3.0	2.6	3.0	3.0	3.5	3.2	3.4	2.9	2.5	3.0	2.9
ANT. OBS.	663	457	415	500	611	759	1028	714	577	1394	1666	913	9784
MIDLERE VINDSTYRKE FOR HELE DATASETTET ER 2.9 M/S, BASERT PÅ 10700 OBSERVASJONER													

Tabell A.3: Fire klasser av stabiliteter fordelt over døgnet basert på målinger av temperaturforskjellen mellom 25 m og 10 m i masta på Ås 1.9.83-30.11.83.

FREKVENNS AV FORSKJELLIGE STABILITETER				
	GRUPPE 1	GRUPPE 2	GRUPPE 3	GRUPPE 4
	X=(< -.5)	X=(-.5-< .0)	X=(.0-< .5)	X=(.5->)
1	1.10	13.19	71.43	14.29
2	2.20	10.99	70.33	16.48
3	1.10	13.19	68.13	17.58
4	.00	13.19	68.13	18.68
5	.00	9.89	73.63	16.48
6	2.20	9.89	79.12	8.79
7	.00	23.08	69.23	7.69
8	.00	40.66	53.85	5.49
9	6.59	60.44	24.18	8.79
10	12.09	70.33	14.29	3.30
11	21.98	70.33	6.59	1.10
12	19.78	73.63	6.59	.00
13	23.33	70.00	6.67	.00
14	22.47	69.66	6.74	1.12
15	12.22	72.22	14.44	1.11
16	8.79	49.45	40.66	1.10
17	5.49	32.97	60.44	1.10
18	1.10	18.68	75.82	4.40
19	1.10	10.99	82.42	5.49
20	.00	14.29	80.22	5.49
21	1.10	8.79	80.22	9.89
22	1.10	8.79	79.12	10.99
23	1.10	9.89	79.12	9.89
24	1.10	12.09	75.82	10.99
	6.06	32.71	53.72	7.52

2180 OBS.

Tabell A.4: Frekvens (i %) av vind og stabilitet fordelt på: fire vindstyrkeklasser og fire stabilitetsklasser (1 = instabilt, 2 = nøytralt, 3 = lett stabilt, 4 = stabilt) vindstille (vind < 0.2 m/s) Basert på data fra Ås i perioden 1.9.83-30.11.83.

	.0- 2.0 M/S				2.0- 4.0 M/S				4.0- 6.0 M/S				OVER 6.0 M/S				ROSE
	1	2	3	4	1	2	3	4	1	2	3	4	1	2	3	4	
30	.1	.3	.6	.1	.0	1.0	.6	.0	.0	.5	.0	.0	.0	.2	.0	.0	3.6
60	.1	.7	.5	.0	.0	.7	.9	.0	.0	.3	.3	.0	.0	.0	.1	.0	3.7
90	.0	.4	.7	.0	.0	.7	.4	.0	.0	.3	.4	.0	.0	.0	.1	.0	2.9
120	.0	.4	.8	.2	.1	.4	.6	.0	.0	.3	.1	.0	.0	.0	.0	.0	3.0
150	.2	.7	.7	.3	.5	1.8	.8	.0	.0	.5	.3	.0	.0	.1	.3	.0	6.1
180	.1	.5	1.1	.1	.1	1.0	.8	.0	.0	.4	.6	.0	.0	.3	.3	.0	5.3
210	.1	.6	1.3	.2	.2	1.8	3.2	.0	.1	.7	3.5	.0	.0	.2	.7	.0	12.5
240	.2	.6	1.7	.2	.1	1.1	2.5	.0	.1	2.2	3.7	.0	.0	.7	1.1	.0	14.3
270	.0	.5	1.4	.1	.0	.3	1.7	.1	.0	.7	.8	.0	.0	.5	.3	.0	6.4
300	.5	.9	.9	.5	.8	1.3	3.2	.7	.0	.9	1.9	.0	.0	.9	1.2	.0	13.6
330	1.2	1.4	2.3	.8	.4	2.0	7.8	3.1	.3	.8	.9	.0	.0	.7	.0	.0	22.0
360	.2	.9	.6	.4	.0	1.2	1.7	.5	.0	.3	.5	.0	.0	.1	.1	.0	6.6
STILLE	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
TOTAL	2.9	7.8	12.4	2.9	2.3	13.4	24.1	4.4	.7	7.8	13.0	.0	.1	3.8	4.4	.0	100.0
FORDELING PÅ VINDHASTIGHET																	
	.0- 2.0 M/S				2.0- 4.0 M/S				4.0- 6.0 M/S				OVER 6.0 M/S				
	26.0				44.2				21.5				8.3				
FORDELING AV STABILITETSKLASSENE																	
	6.0				32.8				53.9				7.3				
ANTALL TIMER = 2184, ANTALL OBSERVASJONER = 2121																	

Tabell A.5: Månedsvise temperaturstatistikk fra Ås for sep., okt. og nov. 1983: Middell-, maksimum- og minimumtemperaturer, antall observasjoner og temperatur under gitte grenser, samt midlere døgnfordeling av temperatur.

338 ÅS			1 9 83		1 30 9 83		24										
MÅNED	NDAG	TMIDL	MAX		MIN		MIDLERE		T <	.0	T <	10.0	T <	20.0			
			T	DAG KL	T	DAG KL	TMAX	TMIN	DØGN	TIMER	DØGN	TIMER	DØGN	TIMER			
SEP 1983	30	11.4	21.9	1 17	.9	30 4	15.4	7.7	0	0	26	239	30	707			
OKT 1983	31	7.5	18.6	26 13	-2.0	29 7	11.2	4.2	3	13	30	565	31	744			
NOV 1983	30	1.9	14.7	1 14	-8.7	30 24	5.0	-0.9	20	293	30	705	30	720			
MIDDELTEMPERATUR, STANDARDAVVIK OG ANTALL OBS.																	
MÅNED	KL	1	4	7	10	13	16	19	22								
SEP 1983		9.5	9.1	9.6	12.7	14.3	14.4	11.9	10.4								
		3.0	3.2	3.1	2.7	2.9	2.9	2.9	3.3								
		30	30	30	30	29	29	30	30	713							
OKT 1983		6.0	5.7	5.5	8.3	10.6	9.8	7.9	6.9								
		3.1	3.4	3.4	3.0	2.6	2.7	2.6	2.8								
		31	31	31	31	31	31	31	31	744							
NOV 1983		1.5	1.0	.8	2.0	4.2	3.1	2.0	1.5								
		4.3	4.1	4.1	4.4	4.5	4.8	4.7	4.6								
		30	30	30	30	30	30	30	30	720							
		1	0	-3	5	1	8	0	2	1	1	1	3				

Tabell A.6: Månedsvise temperaturstatistikk fra Tangen, Brevik for sep., okt. og nov. 1983: Middell-, maksimum- og minimumtemperaturer, antall observasjoner og temperatur under gitte grenser, samt midlere døgnfordeling av temperatur.

403 BREVIKTANGEN			1 9 83		1 30 9 83		24									
MÅNED	NDAG	TMIDL	MAX		MIN		MIDLERE		T <	.0	T <	10.0	T <	20.0		
			T	DAG KL	T	DAG KL	TMAX	TMIN	DØGN	TIMER	DØGN	TIMER	DØGN	TIMER		
SEP 1983	30	11.4	22.0	1 16	-0.9	30 24	15.6	7.0	2	4	26	228	30	714		
OKT 1983	31	7.7	19.7	26 13	-2.9	29 6	12.0	3.7	6	27	30	524	31	741		
NOV 1983	30	2.3	16.2	1 14	-9.2	30 24	5.4	-1.1	19	246	30	679	30	696		
MIDDELTEMPERATUR, STANDARDAVVIK OG ANTALL OBS.																
MÅNED	KL	1	4	7	10	13	16	19	22							
SEP 1983		9.4	8.7	9.2	13.0	14.7	14.6	11.8	10.1							
		3.2	3.7	3.6	2.7	2.7	2.7	3.1	3.8							
		30	30	30	30	30	30	30	30	720						
OKT 1983		6.2	5.5	5.5	8.8	11.3	9.9	7.7	7.0							
		3.8	3.8	3.6	3.1	2.6	2.6	3.3	3.6							
		31	31	31	31	30	31	31	31	741						
NOV 1983		1.9	1.6	1.4	2.5	4.5	3.6	2.1	1.8							
		4.2	4.2	4.2	4.6	4.5	4.8	4.8	4.9							
		29	29	29	29	30	29	29	29	696						

Tabell A.7: Månedsvise relativ fuktighets-statistikk fra Ås for sep., okt. og nov. 1983. Middell-, maksimum og minimumverdier, antall observasjoner av relativ fuktighet under gitte grenser, samt midlere døgnfordeling.

338 ÅS			1 9 83		1 30 9 83 24		MIDLERE		F< .30		F< .75		F< .95	
MÅNED	NDAG	MIDL	F	DAG KL	F	DAG KL	FMAX	TMIN	DØGN	TIMER	DØGN	TIMER	DØGN	TIMER
SEP 1983	30	.83	.98	1 1	.28	28 16	.96	.63	1	1	20	218	28	396
OKT 1983	31	.76	1.00	11 1	.26	21 15	.91	.58	2	5	24	319	30	529
NOV 1983	30	.78	1.00	25 22	.27	20 14	.91	.62	1	2	24	282	30	582

MIDDELFUKTIGHET , STANDARDAVVIK OG ANTALL OBS.														
MÅNED	KL	1	4	7	10	13	16	19	22					
SEP 1983		.89	.93	.93	.82	.74	.71	.81	.85					
		.15	.10	.09	.15	.21	.22	.19	.18					
	30	30	30	30	29	30	30	30	30	716				
OKT 1983		.84	.83	.05	.76	.64	.66	.76	.80					
		.16	.16	.17	.19	.23	.23	.20	.18					
	31	31	31	31	31	31	31	31	31	744				
NOV 1983		.81	.82	.83	.80	.71	.72	.79	.81					
		.17	.14	.14	.16	.18	.17	.17	.16					
	30	30	30	30	30	30	30	30	30	720				

Tabell A.8: Månedsvise relativ fuktighetsstatistikk fra Tangen, Brevik for sep., okt. og nov. 1983. Middell-, maksimum og minimumsverdier, antall observasjoner av relativ fuktighet under gitte grenser, samt midlere døgnfordeling.

403 BREVIKTANGEN			1 9 83		1 30 9 83 24		MIDLERE		F< .30		F< .75		F< .95	
MÅNED	NDAG	MIDL	F	DAG KL	F	DAG KL	FMAX	TMIN	DØGN	TIMER	DØGN	TIMER	DØGN	TIMER
SEP 1983	30	.78	.99	27 3	.27	28 15	.96	.56	3	9	24	261	30	576
OKT 1983	31	.77	.99	26 4	.29	6 14	.92	.58	1	3	23	316	30	557
NOV 1983	30	.80	1.02	8 21	.34	20 15	.92	.64	0	0	23	245	30	562

MIDDELFUKTIGHET , STANDARDAVVIK OG ANTALL OBS.														
MÅNED	KL	1	4	7	10	13	16	19	22					
SEP 1983		.87	.92	.89	.72	.65	.63	.78	.83					
		.13	.08	.09	.18	.22	.21	.18	.15					
	30	30	30	30	30	29	30	30	30	716				
OKT 1983		.86	.86	.86	.73	.63	.68	.78	.82					
		.14	.15	.15	.18	.22	.21	.16	.14					
	31	31	31	31	30	31	31	31	31	740				
NOV 1983		.84	.85	.85	.80	.72	.74	.82	.84					
		.15	.14	.13	.16	.17	.16	.15	.14					
	30	30	30	29	29	30	30	30	30	714				

Tabell A.9: a) Vindfrekvenser fra Ås for september 1983.
 b) Vindfrekvenser fra Ås for oktober 1983.
 c) Vindfrekvenser for Ås for november 1983.

a)

VINDROSE FRA ÅS
 1/ 9-83 - 30/ 9-83

SEKTOR	VINDROSE KL.								DØGN
	1	4	7	10	13	16	19	22	
20- 40	6.7	.0	10.0	3.3	.0	.0	3.4	.0	2.8
50- 70	10.0	6.7	6.7	3.3	3.6	3.3	6.9	13.3	7.8
80-100	.0	3.3	.0	13.3	10.7	10.0	10.3	6.7	6.7
110-130	10.0	10.0	.0	.0	10.7	3.3	3.4	.0	6.0
140-160	10.0	13.3	16.7	20.0	17.9	16.7	13.8	13.3	12.9
170-190	.0	10.0	3.3	.0	7.1	13.3	17.2	3.3	6.2
200-220	13.3	13.3	10.0	6.7	3.6	10.0	6.9	10.0	11.2
230-250	10.0	6.7	6.7	20.0	17.9	6.7	10.3	13.3	10.1
260-280	.0	6.7	10.0	6.7	7.1	3.3	6.9	.0	4.2
290-310	10.0	6.7	10.0	6.7	10.7	13.3	13.8	10.0	12.2
320-340	20.0	10.0	20.0	20.0	10.7	16.7	3.4	16.7	13.4
350- 10	10.0	13.3	6.7	.0	.0	3.3	3.4	13.3	6.4
STILLE	.0	.0	.0	.0	.0	.0	.0	.0	.0
ANT.OBS.	30	30	30	30	28	30	29	30	714
MIDL.VIND	3.0	2.4	2.3	3.0	3.2	3.7	3.0	3.0	3.0

VINDANALYSE

DØGNMIDDEL	30	60	90	120	150	180	210	240	270	300	330	360	TOTAL
STILLE													.0
.3- 2.0 M/S	2.2	2.2	2.4	2.4	3.6	2.8	2.8	2.5	1.5	3.1	4.8	2.2	32.6
2.1- 4.0 M/S	.4	4.1	2.4	2.2	8.0	2.5	5.5	4.2	1.1	4.9	6.6	3.2	45.1
4.1- 6.0 M/S	.1	1.1	1.8	1.3	1.3	.4	2.4	3.4	1.1	2.9	1.8	.4	18.1
OVER 6.0 M/S	.0	.4	.1	.1	.0	.4	.6	.0	.4	1.3	.3	.6	4.2
TOTAL	2.8	7.8	6.7	6.0	12.9	6.2	11.2	10.1	4.2	12.2	13.4	6.4	100.0
MIDL.VIND M/S	1.6	2.9	3.1	2.7	2.8	2.6	3.2	3.2	3.3	3.5	2.8	2.9	3.0
ANT. OBS.	20	56	48	43	92	44	80	72	30	87	96	46	714

MIDLERE VINDSTYRKE FOR HELE DATASETET ER 3.0 M/S, BASERT PÅ 716 OBSERVASJONER

b)

VINDROSE FRA ÅS
 1/10-83 - 31/10-83

SEKTOR	VINDROSE KL.								DØGN
	1	4	7	10	13	16	19	22	
20- 40	.0	.0	.0	.0	.0	.0	.0	3.2	1.1
50- 70	3.2	.0	.0	.0	.0	.0	.0	.0	.1
80-100	.0	3.2	.0	.0	3.2	.0	.0	.0	.4
110-130	.0	3.2	3.2	3.3	6.5	9.7	6.5	.0	3.1
140-160	3.2	3.2	3.2	3.3	6.5	6.5	3.2	.0	4.6
170-190	6.5	.0	6.5	3.3	6.5	9.7	9.7	9.7	6.9
200-220	9.7	12.9	16.1	16.7	9.7	9.7	12.9	16.1	12.5
230-250	19.4	22.6	6.5	20.0	25.8	16.1	29.0	29.0	21.4
260-280	22.6	16.1	3.2	3.3	6.5	12.9	9.7	12.9	9.0
290-310	12.9	16.1	22.6	26.7	16.1	19.4	9.7	12.9	19.9
320-340	22.6	16.1	32.3	20.0	12.9	16.1	19.4	16.1	18.4
350- 10	.0	6.5	6.5	3.3	6.5	.0	.0	.0	2.6
STILLE	.0	.0	.0	.0	.0	.0	.0	.0	.0
ANT.OBS.	31	31	31	30	31	31	31	31	743
MIDL.VIND	3.5	3.4	3.1	3.7	4.0	4.0	3.6	3.4	3.6

VINDANALYSE

DØGNMIDDEL	30	60	90	120	150	180	210	240	270	300	330	360	TOTAL
STILLE													.0
.3- 2.0 M/S	1.1	.1	.4	1.9	1.6	.7	1.2	4.0	2.6	4.6	6.6	1.5	26.2
2.1- 4.0 M/S	.0	.0	.0	1.2	.9	2.8	4.8	5.1	3.6	9.0	8.6	.7	36.9
4.1- 6.0 M/S	.0	.0	.0	.0	.7	2.2	4.7	8.6	1.9	3.8	2.2	.4	24.4
OVER 6.0 M/S	.0	.0	.0	.0	1.3	1.2	1.7	3.6	.9	2.6	1.1	.0	12.5
TOTAL	1.1	.1	.4	3.1	4.6	6.9	12.5	21.4	9.0	19.9	18.4	2.6	100.0
MIDL.VIND M/S	1.1	1.3	.8	1.8	4.0	4.2	4.1	4.3	3.4	3.5	2.9	2.1	3.6
ANT. OBS.	8	1	3	23	34	51	93	159	67	148	137	19	743

MIDLERE VINDSTYRKE FOR HELE DATASETET ER 3.6 M/S, BASERT PÅ 744 OBSERVASJONER

VINDROSE FRA ÅS
1/11-83 - 30/11-83

c)

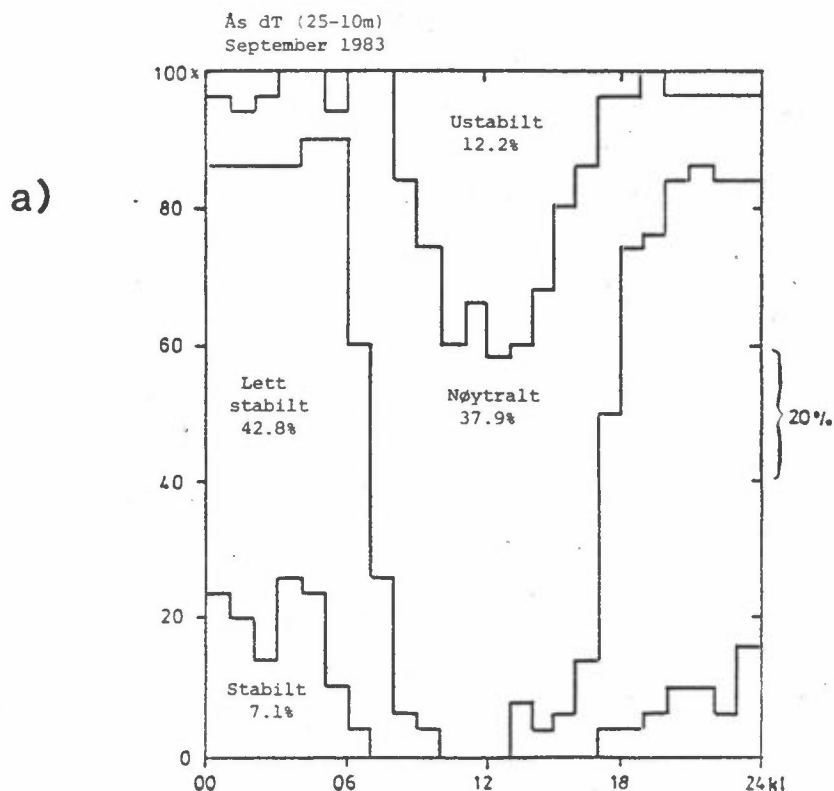
SEKTOR	VINDROSE KL.								DØGN
	1	4	7	10	13	16	19	22	
20- 40	3.3	3.4	10.0	10.0	10.0	10.0	10.0	3.3	7.9
50- 70	.0	3.4	6.7	.0	.0	3.3	3.3	3.3	3.2
80-100	3.3	6.9	.0	.0	.0	.0	.0	.0	1.7
110-130	3.3	.0	3.3	.0	.0	3.3	.0	.0	.7
140-160	3.3	3.4	.0	.0	3.3	.0	3.3	.0	1.5
170-190	.0	3.4	3.3	.0	3.3	.0	.0	3.3	2.8
200-220	13.3	6.9	6.7	23.3	13.3	16.7	20.0	13.3	13.2
230-250	10.0	10.3	10.0	10.0	16.7	20.0	10.0	13.3	11.0
260-280	6.7	6.9	3.3	3.3	3.3	.0	3.3	10.0	5.2
290-310	6.7	13.8	13.3	10.0	13.3	13.3	13.3	13.3	10.5
320-340	36.7	31.0	40.0	26.7	23.3	16.7	30.0	33.3	31.7
350- 10	13.3	10.3	3.3	16.7	13.3	16.7	6.7	6.7	10.6
STILLE	.0	.0	.0	.0	.0	.0	.0	.0	.0
ANT.OBS.	30	29	30	30	30	30	30	30	717
MIDL.VIND	3.0	2.8	3.0	3.1	3.2	3.2	3.1	3.1	3.1

VINDANALYSE

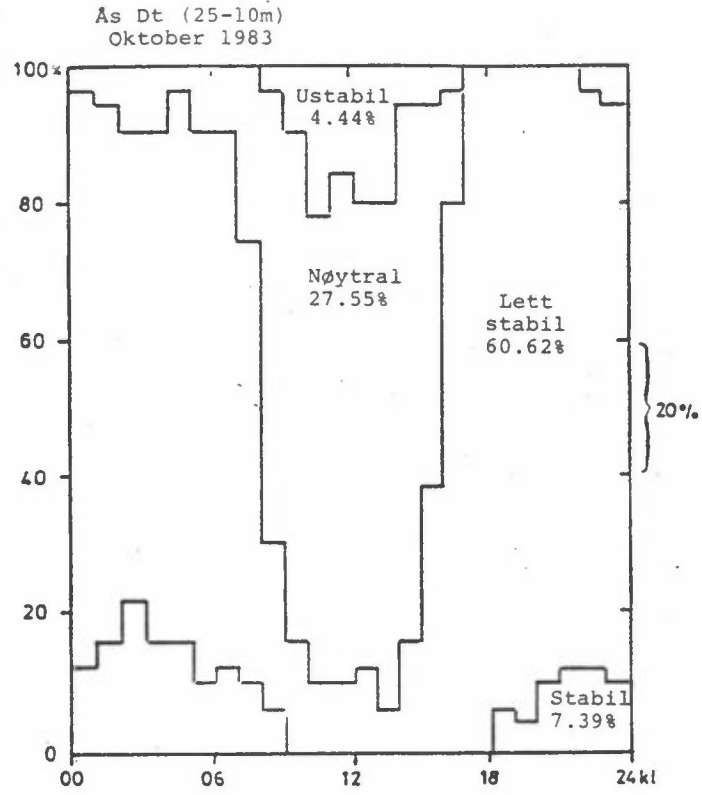
DØGNMIDDEL	30	60	90	120	150	180	210	240	270	300	330	360	TOTAL
STILLE													.0
.3- 2.0 M/S	1.7	1.5	1.3	.7	1.3	2.1	3.1	2.6	2.0	2.5	6.8	4.2	29.7
2.1- 4.0 M/S	4.0	.8	.4	.0	.3	.6	5.0	2.6	1.3	3.9	21.9	5.0	45.9
4.1- 6.0 M/S	1.7	.7	.0	.0	.0	.1	5.2	4.5	.8	1.4	2.1	1.3	17.7
OVER 6.0 M/S	.6	.1	.0	.0	.0	.0	.0	1.3	1.1	2.6	.8	.1	6.7
TOTAL	7.9	3.2	1.7	.7	1.5	2.8	13.2	11.0	5.2	10.5	31.7	10.6	100.0
MIDL.VIND M/S	3.5	2.6	1.4	1.0	1.4	1.9	3.4	3.9	3.4	4.0	2.8	2.6	3.1
ANT. OBS.	57	23	12	5	11	20	95	79	37	75	227	76	717

MIDLERE VINDSTYRKE FOR HELE DATASETET ER 3.1 M/S, BASERT PÅ 720 OBSERVASJONER
-1

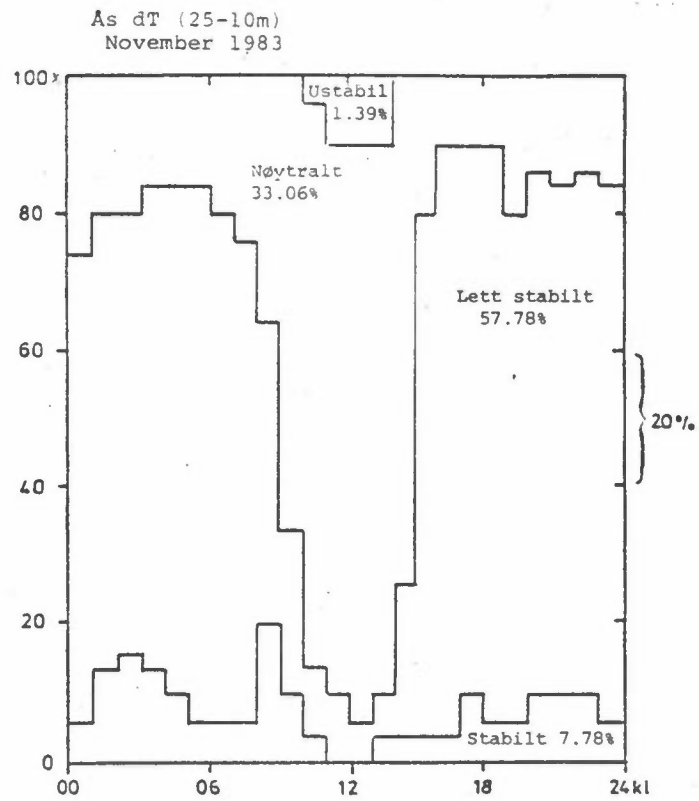
Tabell A.10: Månedsvise stabilitetsfrekvens (i fire klasser) fordelt over døgnet, basert på målinger av temperaturforskjellen mellom 25 m og 10 m i masta på Ås: a) sep. 1983, b) okt. 1983, c) nov. 1983.



b)



c)



Tabell A.11: Frekvens (i %) av vind og stabilitet fra Ås
(klassifisering som tabell 4) i
a) sep. 1983, b) okt. 1983, c) nov. 1983.

a)

	.0- 2.0 M/S				2.0- 4.0 M/S				4.0- 6.0 M/S				OVER 6.0 M/S				ROSE
	1	2	3	4	1	2	3	4	1	2	3	4	1	2	3	4	
30	.1	.1	1.3	.3	.0	.3	.1	.1	.0	.0	.1	.0	.0	.0	.0	.0	2.6
60	.3	1.0	1.0	.0	.0	1.6	2.5	.0	.0	.1	.9	.0	.0	.0	.3	.0	7.6
90	.1	.7	1.2	.1	.0	1.9	.7	.0	.0	.9	1.2	.0	.0	.0	.3	.0	7.1
120	.1	.4	1.0	.3	.4	.7	1.0	.0	.0	.9	.3	.0	.0	.0	.1	.0	5.3
150	.6	1.2	1.4	.1	1.3	4.9	1.6	.0	.1	1.2	.6	.0	.0	.0	.0	.0	13.0
180	.3	.6	1.4	.1	.4	1.9	.7	.0	.0	.6	.0	.0	.0	.4	.0	.0	6.5
210	.0	.3	2.3	.1	.3	1.3	4.0	.0	.3	.7	1.3	.0	.1	.4	.0	.0	11.2
240	.7	.7	.6	.0	.3	1.7	2.2	.0	.4	2.5	1.0	.0	.0	.0	.0	.0	10.1
270	.0	.4	1.2	.0	.0	.4	.9	.0	.0	1.2	.0	.0	.0	.4	.0	.0	4.5
300	1.0	.4	.1	.7	1.4	1.0	2.2	.3	.1	1.2	2.0	.0	.1	.4	.6	.0	11.7
330	1.4	1.3	.9	.9	1.0	1.3	2.9	2.0	.7	1.0	.1	.0	.1	.1	.1	.0	14.0
360	.0	.4	.1	.7	.1	1.0	1.7	1.2	.0	.0	.4	.0	.0	.3	.4	.0	6.5
STILLE	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
TOTAL	4.8	7.6	12.5	3.5	5.3	18.0	20.5	3.6	1.7	10.1	7.9	.0	.4	2.2	1.9	.0	100.0
FORDELING PÅ VINDHASTIGHET																	
.0- 2.0 M/S				2.0- 4.0 M/S				4.0- 6.0 M/S				OVER 6.0 M/S					
28.4				47.4				19.7				4.5					
FORDELING AV STABILITETSKLASSENE																	
12.2				37.9				42.8				7.1					
ANTALL TIMER = 720, ANTALL OBSERVASJONER = 694																	

b)

	.0- 2.0 M/S				2.0- 4.0 M/S				4.0- 6.0 M/S				OVER 6.0 M/S				ROSE
	1	2	3	4	1	2	3	4	1	2	3	4	1	2	3	4	
30	.0	.3	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.7
60	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
90	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.3
120	.0	.8	.6	.3	.0	.4	.8	.0	.0	.0	.0	.0	.0	.0	.0	.0	2.9
150	.0	.6	.4	.4	.1	.1	.6	.0	.0	.3	.3	.0	.0	.3	1.0	.0	4.0
180	.0	.4	.4	.0	.0	1.0	1.2	.0	.0	.4	1.8	.0	.0	.4	1.0	.0	6.6
210	.3	.3	.6	.1	.4	1.2	3.6	.0	.0	.3	5.0	.0	.0	.1	1.8	.0	13.6
240	.0	.3	2.9	.4	.0	.8	3.9	.0	.0	2.9	6.3	.0	.0	2.1	1.8	.0	21.4
270	.0	.0	2.1	.3	.0	.4	3.0	.3	.0	.7	1.5	.0	.0	.8	.1	.0	9.2
300	.4	1.8	1.4	.3	.8	2.1	4.7	1.2	.0	1.5	2.2	.0	.0	1.0	1.7	.0	19.0
330	1.4	1.9	2.5	.8	.3	1.2	5.2	2.9	.3	1.0	1.1	.0	.0	1.1	.0	.0	19.7
360	.4	.6	.3	.1	.0	.1	.6	.0	.0	.0	.4	.0	.0	.0	.0	.0	2.5
STILLE	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
TOTAL	2.5	7.0	11.7	2.8	1.7	7.4	23.6	4.4	.3	7.0	18.6	.0	.0	5.8	7.3	.0	100.0
FORDELING PÅ VINDHASTIGHET																	
.0- 2.0 M/S				2.0- 4.0 M/S				4.0- 6.0 M/S				OVER 6.0 M/S					
24.0				37.1				25.9				13.1					
FORDELING AV STABILITETSKLASSENE																	
4.4				27.3				61.2				7.2					
ANTALL TIMER = 744, ANTALL OBSERVASJONER = 726																	

c)

	.0- 2.0 M/S				2.0- 4.0 M/S				4.0- 6.0 M/S				OVER 6.0 M/S				ROSE
	1	2	3	4	1	2	3	4	1	2	3	4	1	2	3	4	
30	.3	.6	.1	.0	.0	2.9	1.6	.0	.0	1.4	.0	.0	.0	.7	.0	.0	7.6
60	.0	1.1	.3	.0	.0	.6	.4	.0	.0	.9	.0	.0	.0	.1	.0	.0	3.4
90	.0	.3	.7	.0	.0	.1	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	1.6
120	.0	.0	.7	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.7
150	.0	.3	.3	.3	.0	.4	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	1.4
180	.0	.4	1.6	.1	.0	.3	.3	.0	.0	.1	.0	.0	.0	.0	.0	.0	2.9
210	.0	1.1	1.0	.3	.0	2.9	1.9	.0	.0	1.1	4.3	.0	.0	.0	.1	.0	12.7
240	.0	.7	1.6	.3	.0	.9	1.4	.1	.0	1.1	3.7	.0	.0	.0	1.4	.0	11.3
270	.0	1.0	.9	.0	.0	.1	1.3	.0	.0	.1	.7	.0	.0	.3	.9	.0	5.3
300	.0	.4	1.1	.4	.0	.7	2.7	.4	.0	.0	1.4	.0	.0	1.3	1.4	.0	10.0
330	.9	1.0	3.4	.9	.0	3.6	15.3	4.3	.0	.6	1.6	.0	.0	.9	.0	.0	32.2
360	.3	1.7	1.4	.3	.0	2.6	2.9	.3	.0	.9	.6	.0	.0	.1	.0	.0	11.0
STILLE	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
TOTAL	1.4	8.7	13.1	2.6	.0	15.0	28.2	5.1	.0	6.3	12.3	.0	.0	3.4	3.9	.0	100.0
FORDELING PÅ VINDHASTIGHET																	
.0- 2.0 M/S				2.0- 4.0 M/S				4.0- 6.0 M/S				OVER 6.0 M/S					
25.8				48.4				18.5				7.3					
FORDELING AV STABILITETSKLASSENE																	
1.4				33.4				57.5				7.7					
ANTALL TIMER = 720, ANTALL OBSERVASJONER = 701																	

VEDLEGG B

GRAFISK FREMSTILLING AV TIDSFORLØPET AV:

Temperatur (°C)

Temperaturdifferens (25-10 m)

Vindhastighet (m/s)

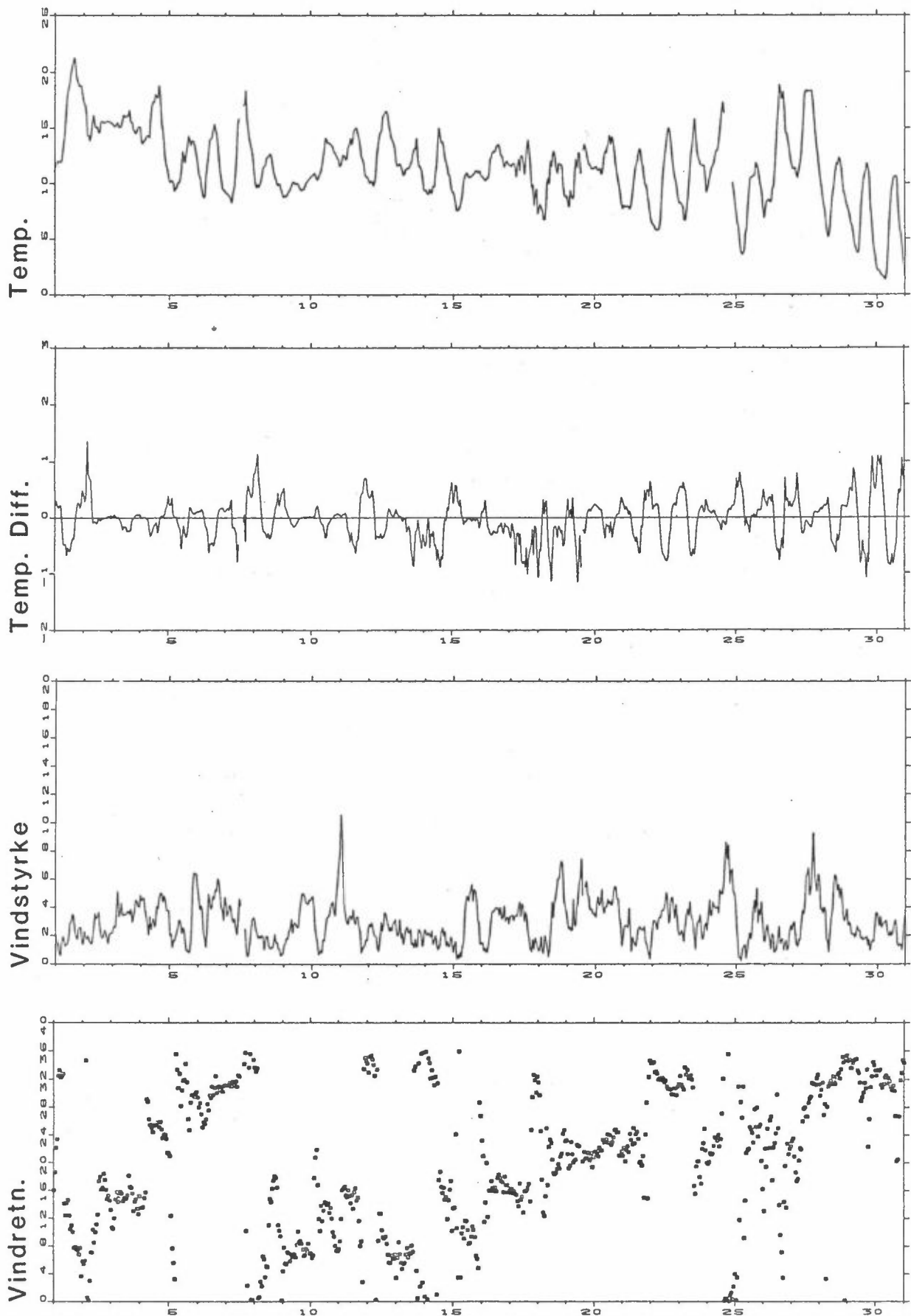
Vindretning (dekagrader)

For månedene september, oktober og november 1983
ved Ås.

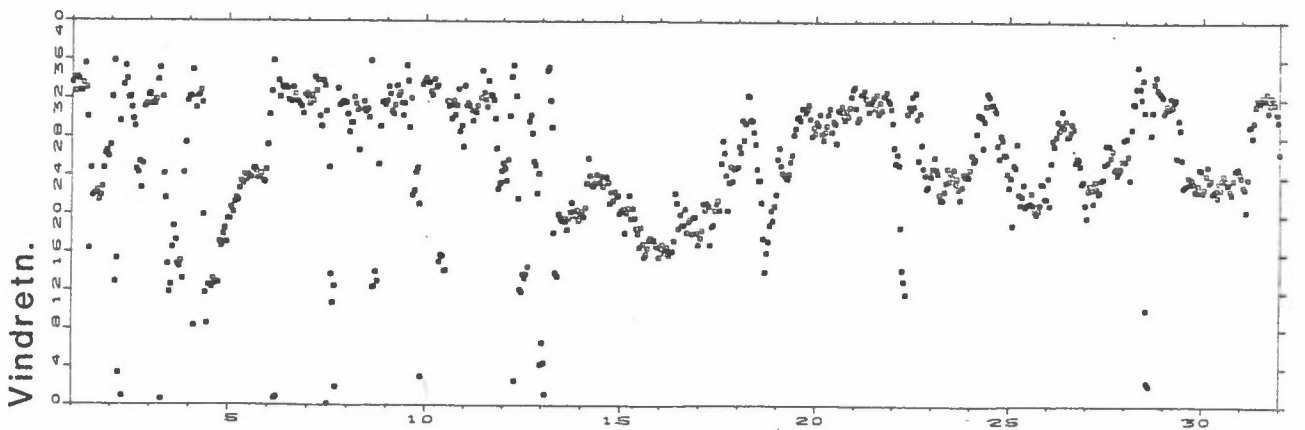
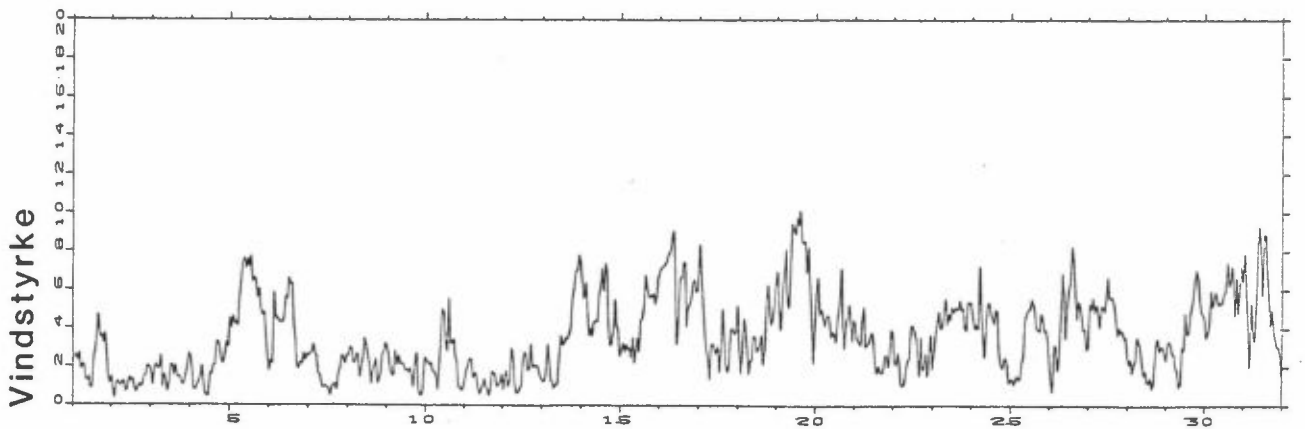
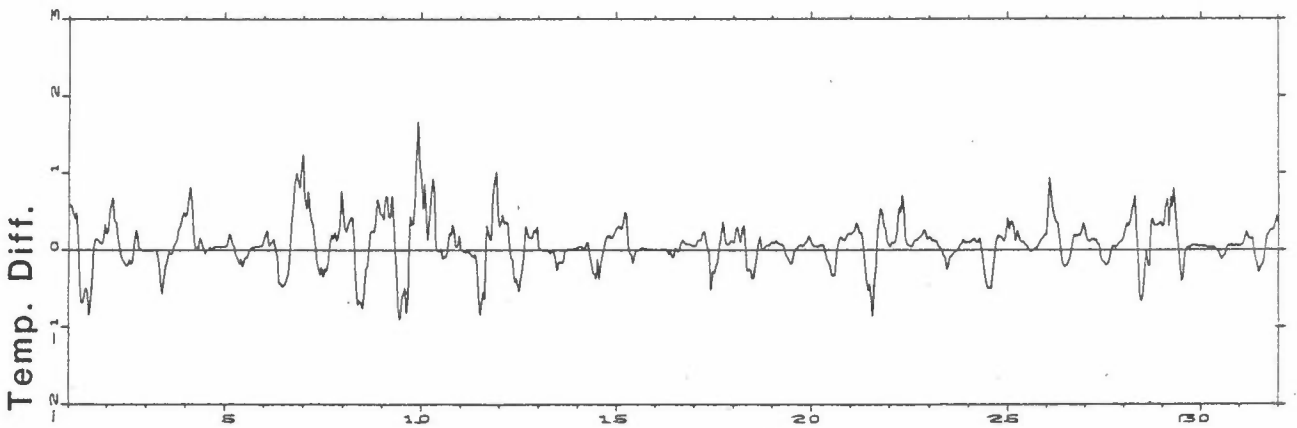
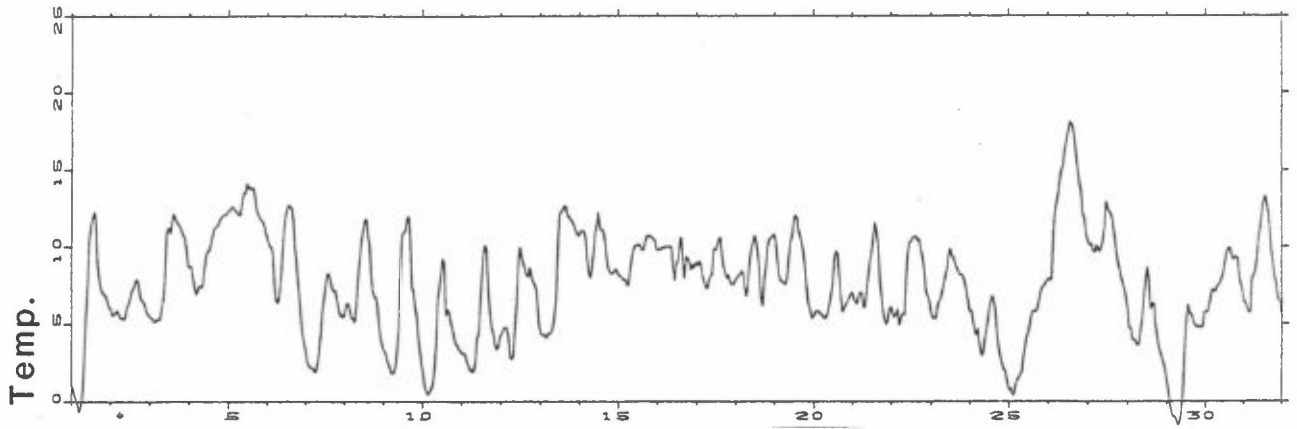
Temperatur (°C)

For månedene september, oktober og november 1983
ved Tangen, Brevik.

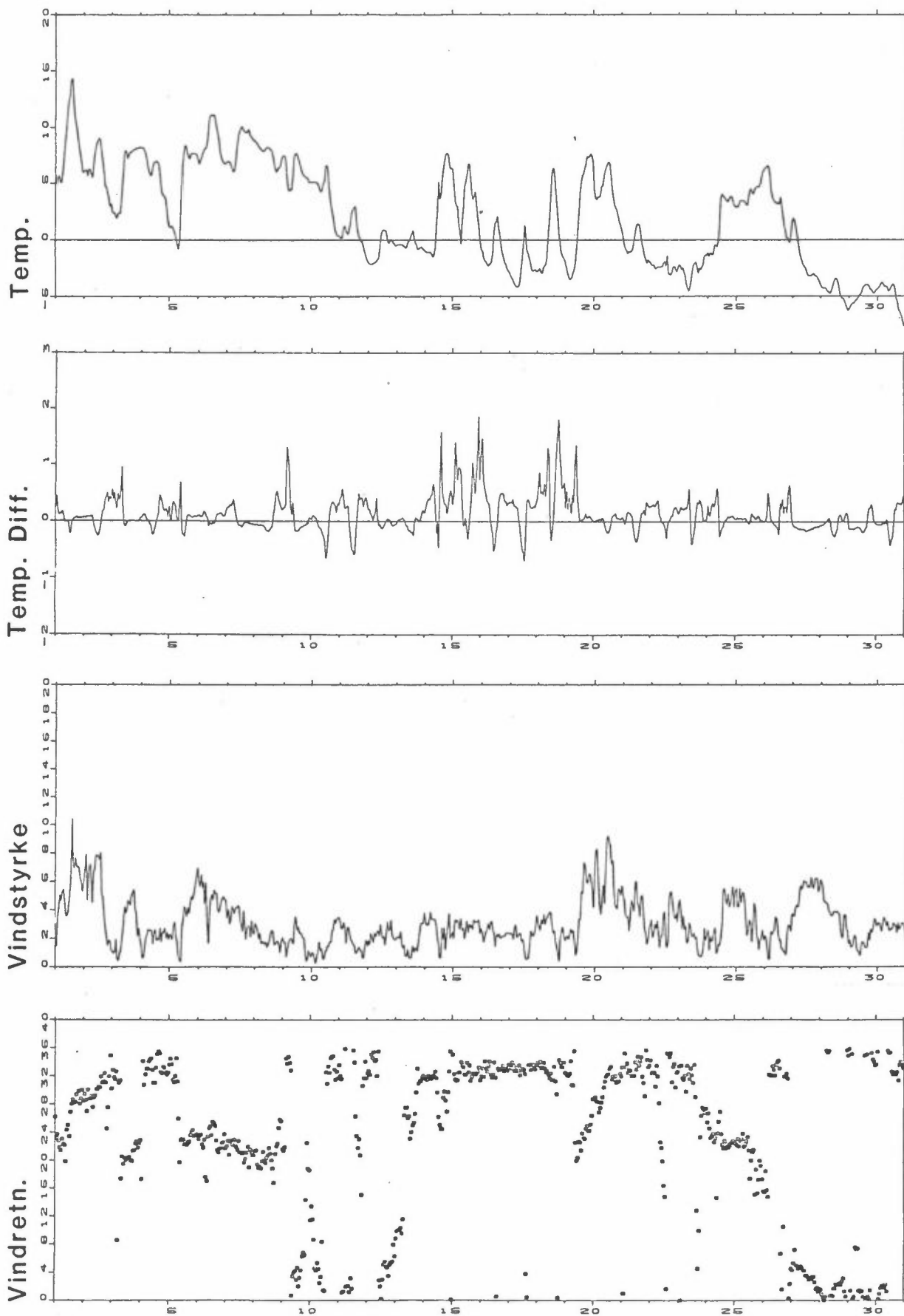
a) 338 Ås, september 1983



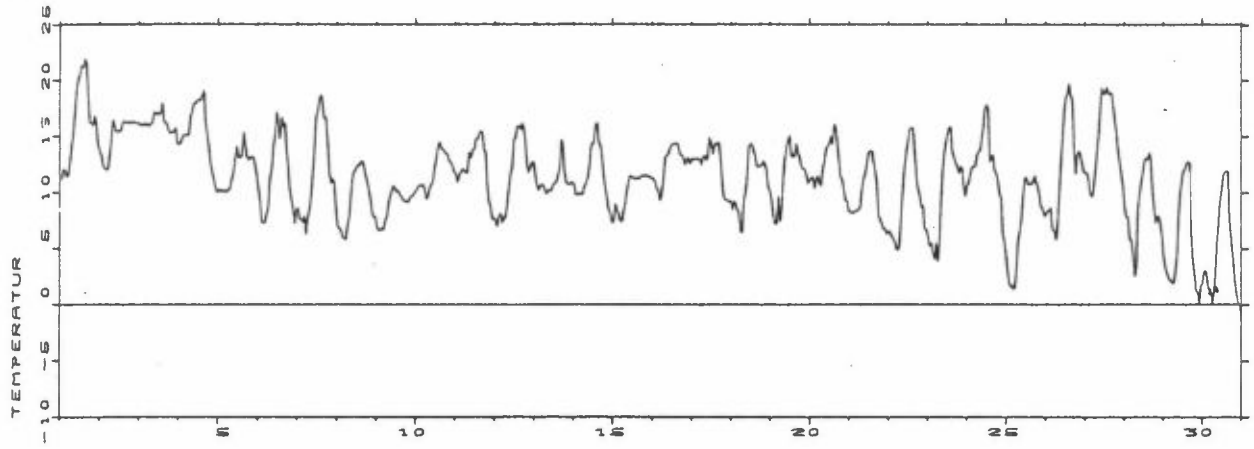
b) 338 Ås, oktober 1983



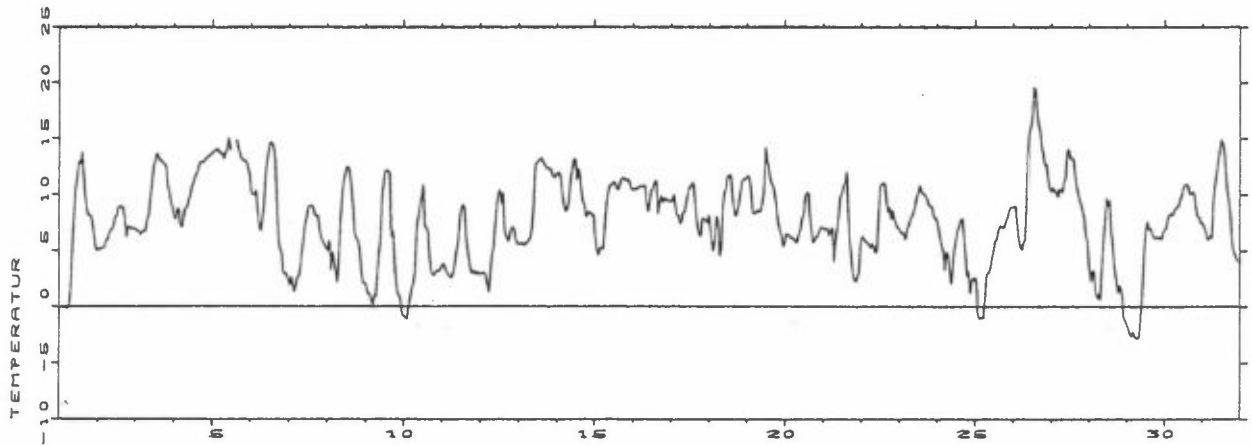
c) 338 ÅS, November 1983



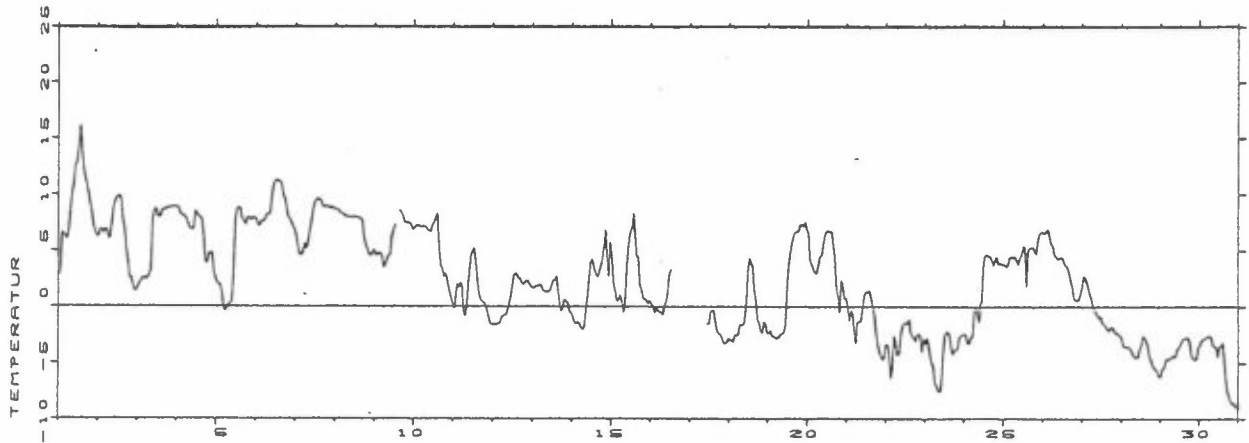
Tangen, September 1983



Oktober 1983



November 1983



VEDLEGG C

LISTE AV TIMEVISE DATA FRA NEDRE TELEMAR
1.9.83-30.11.83

FØLGENDE PARAMETERER ER GITT I DEN SYNOPTISKE LISTEN AV DATA:

T-ÅS = lufttemperatur ($^{\circ}$ C) 3 m over bakken ved Ås
dT-ÅS = temperaturforskjell ($^{\circ}$ C) 25-10 m ved Ås
RH-ÅS = relativ fuktighet (%) 3 m over bakken ved Ås
F-ÅS = vindstyrke (m/s) 25 m over bakken ved Ås
D-ÅS = vindreting (dekagrader; 9=vind fra øst,
18=vind fra sør, osv.)
T-BR = lufttemperatur ($^{\circ}$ C) 2 m over bakken ved Tangen,
Brevik
RH-BR = relativ fuktighet (%) 2 m over bakken ved Tangen,
Brevik
P-TA = nedbørmåling ved Tangen, Brevik (pluviograf)

			T-AS	DT-AS	RH-AS	F-AS	D-AS	T-BR	RH-BR	P-BR	
1	9	83	1	11.6	.23	.98	2.0	16.	11.4	.97	.0
1	9	83	2	10.9	.31	.98	1.4	19.	11.2	.98	.0
1	9	83	3	11.7	.21	.98	1.5	22.	12.1	.94	.0
1	9	83	4	11.8	.17	.98	.8	1023.	12.1	.94	.0
1	9	83	5	11.1	.22	.98	.6	32.	11.4	.96	.0
1	9	83	6	11.4	.22	.98	1.4	33.	11.5	.95	.0
1	9	83	7	12.5	-.14	.98	2.0	32.	12.8	.92	.0
1	9	83	8	14.2	-.49	.94	1.6	32.	14.2	.83	.0
1	9	83	9	15.2	-.49	.89	1.3	33.	15.2	.76	.0
1	9	83	10	16.9	-.48	.80	1.5	14.	17.1	.69	.0
1	9	83	11	18.7	-.69	.75	1.4	12.	19.1	.64	.0
1	9	83	12	19.3	-.54	.72	1.8	14.	20.1	.57	.0
1	9	83	13	20.0	-.61	.60	3.0	15.	20.7	.48	.0
1	9	83	14	21.0	-.59	.55	3.0	12.	21.4	.48	.0
1	9	83	15	21.5	-.44	.51	3.5	10.	21.2	.46	.0
1	9	83	16	21.7	-.37	.47	3.4	11.	22.0	.43	.0
1	9	83	17	21.9	-.38	.45	2.4	10.	21.4	.42	.0
1	9	83	18	21.0	-.08	.47	2.0	8.	18.7	.54	.0
1	9	83	19	19.0	.14	.53	1.7	8.	16.1	.66	.0
1	9	83	20	18.8	.28	.56	2.5	7.	16.2	.68	.0
1	9	83	21	18.5	.26	.60	2.6	7.	15.9	.74	.0
1	9	83	22	18.9	.17	.61	2.6	7.	16.9	.70	.0
1	9	83	23	18.2	.27	.61	1.5	8.	16.0	.74	.0
1	9	83	24	16.0	.50	.69	1.4	4.	14.2	.78	.0
2	9	83	1	16.6	.40	.67	2.3	6.	13.6	.82	.0
2	9	83	2	16.6	.28	.68	1.8	5.	13.3	.85	.0
2	9	83	3	15.6	.37	.71	1.8	6.	12.4	.86	.0
2	9	83	4	13.4	1.37	.91	2.0	35.	12.1	.94	.0
2	9	83	5	13.2	.79	.91	1.6	1.	12.0	.94	.0
2	9	83	6	13.3	.70	.93	1.5	0.	12.2	.90	.0
2	9	83	7	14.1	.67	.89	1.4	3.	13.5	.85	.0
2	9	83	8	15.4	.18	.78	1.9	7.	14.7	.74	.0
2	9	83	9	16.7	-.11	.72	2.5	7.	16.5	.65	.0
2	9	83	10	15.7	-.07	.81	3.6	10.	16.0	.76	.0
2	9	83	11	15.3	-.07	.91	3.2	8.	15.4	.83	.0
2	9	83	12	15.6	-.12	.97	3.4	10.	15.5	.88	.0
2	9	83	13	14.9	-.06	.98	3.7	11.	15.4	.98	.0
2	9	83	14	14.9	.01	.98	2.6	13.	15.6	.98	2.2
2	9	83	15	16.0	-.06	.98	2.0	17.	16.3	.96	.1
2	9	83	16	16.0	-.04	.98	1.8	18.	16.4	.97	.1
2	9	83	17	15.8	-.02	.98	2.0	16.	16.2	.98	.0
2	9	83	18	15.9	.00	.98	2.4	16.	16.3	.98	.2
2	9	83	19	15.8	-.01	.98	2.1	18.	16.2	.98	.2
2	9	83	20	15.9	.00	.98	1.8	17.	16.3	.98	.1
2	9	83	21	16.0	.01	.98	1.5	16.	16.3	.98	.1
2	9	83	22	15.8	.03	.98	2.1	15.	16.3	.98	.0
2	9	83	23	15.8	.01	.98	2.2	15.	16.2	.98	.0
2	9	83	24	15.7	.05	.98	2.2	15.	16.2	.98	.0
3	9	83	1	15.7	.00	.98	2.4	13.	16.1	.98	.1
3	9	83	2	15.5	.01	.98	2.7	11.	16.1	.98	.1
3	9	83	3	15.4	.06	.98	2.6	10.	16.0	.98	.0
3	9	83	4	15.6	.02	.98	3.7	12.	16.1	.98	.9
3	9	83	5	15.8	.00	.98	5.2	15.	16.2	.98	2.7
3	9	83	6	15.3	.01	.98	3.3	16.	16.0	.98	1.8
3	9	83	7	15.4	-.01	.98	3.7	14.	16.0	.98	1.7
3	9	83	8	15.5	-.05	.98	4.4	15.	16.2	.98	.3
3	9	83	9	16.0	-.11	.98	3.4	16.	16.3	.98	.0
3	9	83	10	16.7	-.23	.98	3.5	16.	17.3	.94	.0
3	9	83	11	16.4	-.15	.98	3.5	14.	17.0	.95	.0
3	9	83	12	16.5	-.18	.98	3.6	15.	17.1	.93	.0
3	9	83	13	16.5	-.17	.98	3.7	15.	17.0	.91	.0
3	9	83	14	16.8	-.25	.98	3.7	15.	17.2	.87	.0
3	9	83	15	17.2	-.24	.94	3.5	15.	18.1	.84	.0
3	9	83	16	15.9	-.24	.97	3.9	18.	16.3	.84	.0
3	9	83	17	16.1	-.22	.95	3.0	16.	16.2	.90	.0
3	9	83	18	15.2	-.05	.98	3.4	16.	15.9	.92	.0
3	9	83	19	14.9	-.02	.98	3.8	16.	15.4	.94	.0
3	9	83	20	14.7	.00	.98	4.6	13.	15.3	.93	.0
3	9	83	21	14.9	.05	.98	4.4	14.	15.4	.94	.0
3	9	83	22	15.2	.05	.98	4.1	15.	15.5	.91	.0
3	9	83	23	15.4	.06	.97	4.0	13.	15.8	.85	.0
3	9	83	24	15.2	.04	.95	4.9	13.	14.3	.98	.0

	T-AS	DT-AS	RH-AS	F-AS	D-AS	T-BR	RH-BR	P-BR
4 9 83 1	14.0	.06	.98	4.5	15.	14.3	.98	.0
4 9 83 2	13.7	-.01	.98	4.6	13.	14.4	.98	.0
4 9 83 3	14.1	.00	.98	4.7	13.	14.9	.98	.0
4 9 83 4	14.1	.00	.98	3.8	14.	15.2	.98	.0
4 9 83 5	14.5	.01	.98	3.2	15.	15.2	.98	.0
4 9 83 6	14.6	.00	.98	2.7	16.	15.2	.98	.0
4 9 83 7	14.7	-.03	.98	2.0	1029.	15.2	.94	.0
4 9 83 8	14.4	-.05	.98	3.4	29.	16.9	.87	.0
4 9 83 9	16.4	-.21	.97	2.4	26.	17.2	.83	.0
4 9 83 10	17.6	-.34	.93	2.8	25.	18.1	.76	.0
4 9 83 11	18.1	-.29	.86	3.2	25.	18.0	.73	.0
4 9 83 12	17.8	-.22	.85	2.7	24.	18.3	.61	.0
4 9 83 13	18.6	-.15	.73	2.8	25.	18.4	.60	.0
4 9 83 14	18.3	-.12	.68	4.1	25.	18.2	.58	.0
4 9 83 15	18.1	-.08	.66	3.9	25.	18.8	.49	.0
4 9 83 16	19.5	-.28	.56	4.8	26.	19.2	.49	.0
4 9 83 17	18.2	-.16	.56	5.1	25.	16.2	.58	.0
4 9 83 18	15.9	.00	.65	5.0	26.	15.3	.65	.0
4 9 83 19	15.0	.03	.66	4.4	25.	14.2	.76	.0
4 9 83 20	13.9	.03	.72	4.8	24.	12.7	.77	.0
4 9 83 21	12.4	.03	.83	4.5	24.	12.0	.76	.0
4 9 83 22	11.4	.08	.89	3.7	24.	11.2	.78	.0
4 9 83 23	11.0	.17	.87	3.8	23.	10.5	.81	.0
4 9 83 24	10.3	.22	.88	3.7	21.	10.0	.81	.0
5 9 83 1	9.5	.40	.92	2.0	21.	10.2	.82	.0
5 9 83 2	9.8	.22	.92	2.2	21.	10.3	.93	.0
5 9 83 3	10.0	.22	.95	1.2	12.	10.1	.97	.0
5 9 83 4	9.6	.35	.98	1.7	8.	10.2	.98	.0
5 9 83 5	9.2	.05	.98	1.7	6.	10.1	.98	.0
5 9 83 6	9.5	.01	.98	2.0	3.	10.2	.98	.0
5 9 83 7	9.6	.00	.98	2.4	36.	10.3	.98	.0
5 9 83 8	10.0	.02	.98	2.7	33.	10.5	.98	.0
5 9 83 9	10.0	-.08	.98	3.1	31.	11.2	.96	.0
5 9 83 10	10.6	-.18	.98	2.8	33.	12.0	.90	.0
5 9 83 11	11.4	-.22	.97	2.1	28.	13.3	.79	.0
5 9 83 12	13.8	-.57	.89	2.6	30.	14.2	.81	.0
5 9 83 13	13.3	-.34	.92	2.4	32.	13.1	.94	.0
5 9 83 14	12.4	-.14	.98	1.5	32.	13.2	.94	.0
5 9 83 15	13.4	-.30	.98	.9	34.	13.3	.90	.0
5 9 83 16	14.1	-.36	.95	1.0	1032.	15.4	.84	.0
5 9 83 17	14.8	-.28	.96	.8	26.	14.2	.94	.0
5 9 83 18	14.2	-.08	.97	1.1	25.	13.1	.98	.0
5 9 83 19	13.4	.20	.98	2.2	29.	12.9	.71	.0
5 9 83 20	13.9	.17	.76	5.3	30.	13.2	.59	.0
5 9 83 21	13.9	.09	.64	6.5	30.	13.3	.56	.0
5 9 83 22	13.5	.07	.62	6.4	29.	13.0	.53	.0
5 9 83 23	12.9	.06	.59	6.4	30.	12.2	.56	.0
5 9 83 24	12.2	.10	.60	5.5	30.	11.4	.55	.0
6 9 83 1	11.3	.10	.61	4.8	29.	10.2	.60	99.0
6 9 83 2	10.5	.12	.63	3.8	28.	9.2	.61	99.0
6 9 83 3	10.0	.11	.61	4.1	29.	7.3	.74	99.0
6 9 83 4	9.3	.13	.65	3.6	27.	7.3	.84	99.0
6 9 83 5	8.6	.16	.70	2.2	25.	7.4	.75	99.0
6 9 83 6	8.4	.11	.75	1.9	26.	8.2	.80	99.0
6 9 83 7	8.8	.01	.79	1.2	26.	8.7	.69	99.0
6 9 83 8	10.9	-.15	.71	2.2	26.	11.3	.59	99.0
6 9 83 9	12.1	-.20	.62	5.0	28.	12.4	.53	99.0
6 9 83 10	13.3	-.32	.59	4.6	28.	14.2	.48	99.0
6 9 83 11	15.1	-.64	.54	3.9	30.	15.2	.46	99.0
6 9 83 12	14.7	-.47	.52	4.0	29.	17.3	.38	99.0
6 9 83 13	15.1	-.47	.49	4.8	31.	16.3	.39	99.0
6 9 83 14	15.6	-.45	.44	4.6	30.	14.8	.35	99.0
6 9 83 15	16.3	-.51	.40	5.3	31.	16.8	.33	99.0
6 9 83 16	15.7	-.41	.40	5.2	32.	15.8	.34	99.0
6 9 83 17	15.1	-.35	.39	6.1	30.	16.3	.34	99.0
6 9 83 18	13.8	-.10	.42	5.8	31.	13.8	.37	99.0
6 9 83 19	12.2	.06	.47	5.1	31.	12.3	.44	99.0
6 9 83 20	10.8	.15	.54	4.1	30.	10.4	.53	99.0
6 9 83 21	9.8	.17	.58	3.8	31.	9.3	.56	99.0
6 9 83 22	9.0	.18	.64	3.1	30.	8.6	.64	99.0
6 9 83 23	9.0	.18	.67	4.8	31.	7.2	.59	99.0
6 9 83 24	9.0	.11	.68	4.3	31.	8.6	.59	99.0

	T-AS	DT-AS	RH-AS	F-AS	D-AS	T-BR	RH-BR	P-BR
7 9 83 1	8.0	.10	.68	3.4	31.	8.7	.59	99.0
7 9 83 2	8.7	.16	.68	3.8	31.	7.6	.67	99.0
7 9 83 3	8.5	.18	.69	4.2	31.	7.7	.65	99.0
7 9 83 4	8.5	.13	.68	3.9	31.	7.3	.81	99.0
7 9 83 5	8.0	.23	.72	3.2	31.	8.0	.63	99.0
7 9 83 6	7.6	.33	.76	2.9	32.	6.3	.71	99.0
7 9 83 7	9.6	-.19	.75	3.3	32.	7.8	.83	99.0
7 9 83 8	9.9	-.17	.74	2.5	31.	8.6	.67	99.0
7 9 83 9	11.1	-.23	.72	2.1	32.	9.8	.63	99.0
7 9 83 10	12.8	-.29	.68	2.9	31.	11.8	.57	99.0
7 9 83 11	99.0	-.00	.53	4.7	33.	13.8	.54	99.0
7 9 83 12	99.0	-.48	.51	4.2	32.	16.9	.42	99.0
7 9 83 13	99.0	99.00	99.00	99.0	99.	17.3	.42	99.0
7 9 83 14	99.0	99.00	99.00	99.0	99.	18.6	.40	99.0
7 9 83 15	99.0	99.00	99.00	99.0	99.	18.8	.40	99.0
7 9 83 16	99.0	-.08	.54	2.5	34.	17.8	.39	99.0
7 9 83 17	17.3	.06	.58	1.0	1036.	16.6	.49	99.0
7 9 83 18	19.0	-.44	.53	.5	10.	16.7	.64	99.0
7 9 83 19	15.0	.38	.66	.7	2.	14.8	.74	99.0
7 9 83 20	13.4	.59	.72	1.6	34.	11.8	.81	99.0
7 9 83 21	12.9	.49	.69	2.4	36.	10.8	.89	99.0
7 9 83 22	12.5	.41	.70	3.2	0.	11.3	.79	99.0
7 9 83 23	12.3	.36	.70	3.3	0.	10.9	.67	99.0
7 9 83 24	11.7	.42	.71	3.0	35.	8.7	.84	99.0
8 9 83 1	9.9	.78	.79	2.5	34.	7.0	.92	99.0
8 9 83 2	8.9	.82	.94	2.1	33.	6.8	.95	99.0
8 9 83 3	8.3	.94	.94	1.8	34.	6.6	.95	99.0
8 9 83 4	8.0	1.14	.91	2.0	1.	6.0	.89	99.0
8 9 83 5	8.3	.69	.89	1.8	1.	5.9	.87	99.0
8 9 83 6	8.6	.52	.84	2.1	3.	5.8	.74	99.0
8 9 83 7	9.9	.14	.71	1.9	2.	7.3	.84	99.0
8 9 83 8	11.0	-.14	.67	1.0	6.	7.9	.59	99.0
8 9 83 9	11.9	-.26	.63	1.7	6.	9.8	.53	99.0
8 9 83 10	12.2	-.26	.62	2.0	3.	11.3	.54	99.0
8 9 83 11	12.4	-.30	.62	1.9	5.	12.0	.52	99.0
8 9 83 12	13.2	-.37	.61	1.3	5.	12.1	.51	99.0
8 9 83 13	12.8	-.28	.62	1.1	11.	12.6	.51	99.0
8 9 83 14	13.0	-.39	.63	1.2	15.	12.4	.51	99.0
8 9 83 15	13.0	-.35	.63	1.2	14.	12.9	.51	99.0
8 9 83 16	12.6	-.27	.67	1.5	16.	12.8	.53	99.0
8 9 83 17	11.6	-.11	.75	2.1	17.	12.3	.59	99.0
8 9 83 18	10.8	.02	.82	1.5	18.	11.5	.64	99.0
8 9 83 19	10.1	.19	.88	1.6	18.	10.8	.72	99.0
8 9 83 20	9.6	.24	.92	1.0	16.	10.1	.79	99.0
8 9 83 21	8.7	.46	.98	1.1	11.	9.3	.91	99.0
8 9 83 22	8.5	.20	.98	.6	10.	8.1	.93	99.0
8 9 83 23	8.6	.30	.98	.8	9.	7.8	.92	99.0
8 9 83 24	8.0	.42	.98	.8	1000.	7.8	.95	99.0
9 9 83 1	7.8	.49	.98	1.5	4.	6.8	.95	99.0
9 9 83 2	7.8	.54	.98	1.5	8.	6.6	.94	99.0
9 9 83 3	8.6	.20	.98	1.9	5.	6.8	.94	99.0
9 9 83 4	8.5	.14	.97	1.8	5.	6.8	.94	99.0
9 9 83 5	8.8	.08	.95	2.3	7.	6.8	.89	99.0
9 9 83 6	9.1	.02	.94	2.5	7.	7.5	.84	99.0
9 9 83 7	9.3	-.02	.95	3.2	6.	8.0	.80	99.0
9 9 83 8	9.7	-.12	.94	2.2	7.	9.1	.79	99.0
9 9 83 9	10.0	-.13	.96	2.9	6.	9.8	.80	99.0
9 9 83 10	10.3	-.17	.98	2.9	7.	10.2	.81	99.0
9 9 83 11	10.2	-.15	.98	2.7	7.	10.7	.81	99.0
9 9 83 12	9.9	-.12	.98	2.6	6.	10.3	.91	99.0
9 9 83 13	10.1	-.07	.98	2.8	8.	10.0	.91	99.0
9 9 83 14	9.9	-.04	.98	3.8	10.	10.2	.89	99.0
9 9 83 15	9.6	.00	.98	4.4	9.	9.8	.91	99.0
9 9 83 16	9.4	.00	.98	5.1	9.	9.6	.93	99.0
9 9 83 17	9.2	.00	.98	5.0	8.	9.3	.94	99.0
9 9 83 18	9.3	.01	.98	4.8	8.	9.2	.94	99.0
9 9 83 19	9.4	.02	.98	4.4	7.	9.2	.94	99.0
9 9 83 20	9.6	.01	.98	4.3	7.	9.2	.95	99.0
9 9 83 21	9.9	.02	.98	4.2	8.	9.6	.95	99.0
9 9 83 22	10.1	.01	.98	4.6	7.	9.8	.94	99.0
9 9 83 23	10.3	.01	.98	4.5	8.	9.8	.95	99.0
9 9 83 24	10.4	.02	.98	4.8	7.	10.1	.95	99.0

			T-AS	DT-AS	RH-AS	F-AS	D-AS	T-BR	RH-BR	P-BR	
10	9	83	1	10.5	.01	.98	4.9	7.	10.3	.94	99.0
10	9	83	2	10.6	.01	.98	4.1	6.	10.6	.95	99.0
10	9	83	3	10.8	.03	.98	2.8	7.	10.7	.96	99.0
10	9	83	4	10.9	.03	.98	2.0	18.	10.7	.95	99.0
10	9	83	5	10.4	.15	.98	1.6	21.	10.8	.94	99.0
10	9	83	6	9.8	.22	.98	.7	22.	10.3	.96	99.0
10	9	83	7	10.2	.14	.98	.8	17.	9.4	.96	99.0
10	9	83	8	10.7	.02	.98	1.0	12.	9.8	.96	99.0
10	9	83	9	11.0	-.08	.98	.8	10.	10.4	.96	99.0
10	9	83	10	11.4	-.11	.98	1.8	14.	10.8	.96	99.0
10	9	83	11	12.4	-.13	.98	1.6	12.	11.0	.87	99.0
10	9	83	12	13.3	-.24	.98	2.6	13.	12.3	.86	99.0
10	9	83	13	14.6	-.37	.96	3.3	14.	13.2	.83	99.0
10	9	83	14	14.4	-.34	.96	3.3	14.	14.1	.83	99.0
10	9	83	15	13.9	-.14	.98	3.4	14.	14.6	.86	99.0
10	9	83	16	13.9	-.09	.98	3.9	14.	14.0	.86	99.0
10	9	83	17	13.8	-.06	.98	4.3	13.	13.8	.87	99.0
10	9	83	18	13.6	-.02	.98	4.4	13.	13.7	.89	99.0
10	9	83	19	13.4	.00	.98	3.7	12.	13.4	.90	99.0
10	9	83	20	12.9	.02	.98	3.4	10.	13.4	.92	99.0
10	9	83	21	12.7	.06	.98	4.8	9.	12.8	.92	99.0
10	9	83	22	12.5	.05	.98	5.7	8.	12.7	.92	99.0
10	9	83	23	12.2	.08	.98	7.0	7.	12.3	.92	99.0
10	9	83	24	11.9	.06	.98	7.9	7.	11.8	.92	99.0
11	9	83	1	11.4	.06	.98	10.6	8.	11.7	.92	99.0
11	9	83	2	11.6	.03	.98	9.2	9.	10.9	.92	99.0
11	9	83	3	12.1	.03	.98	6.2	12.	11.6	.94	99.0
11	9	83	4	12.6	.07	.98	3.9	16.	11.8	.92	99.0
11	9	83	5	12.4	.06	.98	3.2	16.	12.2	.92	99.0
11	9	83	6	12.0	.09	.98	2.9	17.	12.0	.91	99.0
11	9	83	7	12.3	.01	.98	2.8	15.	11.8	.91	99.0
11	9	83	8	13.6	-.22	.95	3.4	15.	11.8	.84	99.0
11	9	83	9	13.9	-.27	.94	3.5	16.	13.7	.79	99.0
11	9	83	10	14.7	-.45	.88	3.1	15.	13.1	.79	99.0
11	9	83	11	13.8	-.26	.93	3.9	14.	13.9	.75	99.0
11	9	83	12	14.7	-.45	.87	3.0	15.	14.0	.73	99.0
11	9	83	13	15.4	-.51	.86	2.8	13.	14.9	.73	99.0
11	9	83	14	15.9	-.54	.83	3.4	16.	14.8	.67	99.0
11	9	83	15	16.0	-.64	.79	3.3	16.	15.3	.65	99.0
11	9	83	16	15.3	-.43	.83	2.7	15.	15.6	.66	99.0
11	9	83	17	14.5	-.39	.86	2.3	15.	15.3	.73	99.0
11	9	83	18	13.3	-.08	.93	.8	1012.	13.8	.74	99.0
11	9	83	19	11.4	.37	.98	1.0	1008.	13.6	.94	99.0
11	9	83	20	10.4	.43	.98	1.3	9.	10.8	.96	99.0
11	9	83	21	9.9	.44	.98	1.3	3.	9.3	.96	99.0
11	9	83	22	10.3	.69	.98	1.7	33.	8.6	.96	99.0
11	9	83	23	9.7	.72	.98	1.7	35.	7.6	.96	99.0
11	9	83	24	9.6	.69	.98	2.5	35.	7.8	.96	99.0
12	9	83	1	9.6	.46	.98	2.8	34.	7.6	.96	99.0
12	9	83	2	9.4	.37	.98	2.6	33.	7.0	.96	99.0
12	9	83	3	9.6	.35	.98	3.0	35.	7.9	.96	99.0
12	9	83	4	9.4	.41	.98	2.5	35.	8.3	.96	99.0
12	9	83	5	9.2	.49	.98	2.0	35.	7.3	.96	99.0
12	9	83	6	9.6	.32	.98	2.0	34.	7.8	.96	99.0
12	9	83	7	10.5	.03	.98	1.9	32.	7.9	.95	99.0
12	9	83	8	12.8	-.40	.95	1.1	0.	8.8	.93	99.0
12	9	83	9	13.8	-.33	.95	.9	33.	10.3	.85	99.0
12	9	83	10	14.5	-.35	.88	1.7	9.	11.8	.81	99.0
12	9	83	11	15.2	-.37	.86	3.0	13.	12.3	.74	99.0
12	9	83	12	15.4	-.29	.85	2.3	13.	14.8	.69	99.0
12	9	83	13	16.7	-.38	.77	2.8	10.	14.9	.64	99.0
12	9	83	14	17.1	-.37	.74	3.7	9.	16.0	.63	99.0
12	9	83	15	17.0	-.32	.70	3.5	9.	16.1	.62	99.0
12	9	83	16	17.1	-.25	.67	3.0	9.	15.6	.57	99.0
12	9	83	17	16.5	-.16	.70	2.7	8.	16.3	.57	99.0
12	9	83	18	15.4	.07	.79	2.3	7.	15.8	.69	99.0
12	9	83	19	14.7	.17	.86	2.6	6.	14.8	.84	99.0
12	9	83	20	14.1	.13	.93	2.3	6.	12.0	.91	99.0
12	9	83	21	13.9	.05	.94	2.8	7.	11.8	.84	99.0
12	9	83	22	13.6	.03	.96	3.0	6.	12.3	.83	99.0
12	9	83	23	13.0	.02	.98	3.2	6.	12.3	.83	99.0
12	9	83	24	11.8	.08	.98	2.4	7.	12.8	.90	99.0

			T-AS	DT-AS	RH-AS	F-AS	D-AS	T-BR	RH-BR	P-BR	
13	9	83	1	11.3	.15	.98	2.0	3.	11.8	.92	99.0
13	9	83	2	11.5	.08	.98	2.2	6.	10.8	.95	99.0
13	9	83	3	11.7	.04	.98	3.2	9.	10.2	.96	99.0
13	9	83	4	11.5	.00	.98	1.8	7.	10.7	.94	99.0
13	9	83	5	11.0	.03	.98	2.2	6.	10.8	.93	99.0
13	9	83	6	10.5	-.06	.98	1.4	5.	10.7	.94	99.0
13	9	83	7	10.7	-.07	.98	1.8	5.	10.3	.95	99.0
13	9	83	8	11.2	.00	.98	2.4	6.	9.9	.96	99.0
13	9	83	9	11.3	-.01	.98	2.7	7.	10.3	.95	99.0
13	9	83	10	11.5	-.27	.98	2.3	8.	10.3	.94	99.0
13	9	83	11	11.6	-.21	.98	2.2	6.	10.3	.95	99.0
13	9	83	12	11.9	-.14	.98	2.5	7.	10.8	.92	99.0
13	9	83	13	12.4	-.27	.98	1.3	7.	10.9	.91	99.0
13	9	83	14	13.1	-.59	.95	1.5	8.	11.0	99.00	99.0
13	9	83	15	13.7	-.76	.90	1.2	7.	11.8	99.00	99.0
13	9	83	16	14.2	-.93	.86	1.8	1033.	12.3	99.00	99.0
13	9	83	17	15.1	-.56	.92	1.2	34.	14.8	99.00	99.0
13	9	83	18	12.4	-.23	.98	1.3	4.	14.0	.86	99.0
13	9	83	19	11.2	-.24	.98	2.5	0.	11.8	.89	99.0
13	9	83	20	11.0	-.04	.98	2.3	34.	10.9	.95	99.0
13	9	83	21	11.3	-.27	.98	2.1	2.	10.7	.95	99.0
13	9	83	22	10.7	-.44	.98	1.2	36.	10.8	.95	99.0
13	9	83	23	9.8	-.56	.98	1.7	3.	10.9	.95	99.0
13	9	83	24	9.2	-.29	.98	2.5	36.	10.9	.95	99.0
14	9	83	1	9.2	-.40	.98	2.2	1.	10.6	.95	99.0
14	9	83	2	9.0	-.53	.98	2.0	36.	9.8	.93	99.0
14	9	83	3	8.9	-.44	.98	2.3	0.	9.9	.94	99.0
14	9	83	4	9.3	-.08	.98	2.0	35.	10.0	.94	99.0
14	9	83	5	8.8	.01	.98	1.9	34.	9.9	.94	99.0
14	9	83	6	9.1	-.56	.98	2.4	32.	9.9	.94	99.0
14	9	83	7	9.7	-.28	.98	1.4	33.	10.6	.98	99.0
14	9	83	8	9.7	-.35	.98	1.8	32.	11.0	.98	2.7
14	9	83	9	11.1	-.24	.98	2.0	31.	11.4	.97	.0
14	9	83	10	12.3	-.52	.96	1.4	32.	12.5	.89	.0
14	9	83	11	14.6	-.49	.88	1.0	1.	14.2	.83	.0
14	9	83	12	15.9	-.78	.78	1.2	31.	14.5	.75	.0
14	9	83	13	15.0	-.57	.82	1.4	17.	14.5	.77	.0
14	9	83	14	14.0	-.78	.85	2.3	19.	16.2	.71	.0
14	9	83	15	14.1	-.90	.83	2.6	16.	16.3	.69	.0
14	9	83	16	13.4	-.69	.87	2.0	16.	14.4	.79	.0
14	9	83	17	12.7	-.75	.95	2.3	16.	14.2	.86	.0
14	9	83	18	11.7	-.27	.98	1.3	15.	13.1	.94	.0
14	9	83	19	10.8	-.02	.98	1.6	15.	11.5	.97	.0
14	9	83	20	8.9	-.06	.98	1.2	12.	10.2	.97	.0
14	9	83	21	8.8	.19	.98	1.3	15.	9.4	.97	.0
14	9	83	22	8.6	.13	.98	2.0	16.	8.4	.97	.0
14	9	83	23	8.3	.36	.98	1.6	17.	8.2	.97	.0
14	9	83	24	8.3	.50	.98	.8	10.	7.3	.97	.0
15	9	83	1	7.8	.64	.98	1.3	13.	7.5	.97	.0
15	9	83	2	8.1	.24	.98	1.6	14.	9.1	.97	.0
15	9	83	3	7.2	.38	.98	.3	24.	8.4	.97	.0
15	9	83	4	7.1	.59	.98	.7	11.	8.2	.97	.0
15	9	83	5	7.2	.56	.98	.4	1003.	7.5	.97	.1
15	9	83	6	7.5	.23	.98	.9	36.	7.4	.97	.0
15	9	83	7	8.3	.20	.98	.5	3.	8.3	.97	.0
15	9	83	8	8.9	.32	.98	1.2	10.	9.1	.97	.0
15	9	83	9	9.9	.05	.98	1.6	11.	10.3	.97	.0
15	9	83	10	10.4	.00	.98	3.5	9.	11.1	.95	.4
15	9	83	11	10.8	-.13	.98	4.5	12.	11.6	.95	.5
15	9	83	12	11.0	-.06	.98	4.8	12.	11.4	.88	.9
15	9	83	13	10.6	-.08	.98	4.4	10.	11.3	.88	.4
15	9	83	14	10.4	-.01	.98	5.0	8.	11.3	.93	.4
15	9	83	15	10.5	-.01	.98	5.2	8.	11.3	.93	1.0
15	9	83	16	10.5	-.03	.98	5.7	9.	11.3	.94	2.9
15	9	83	17	10.7	-.04	.98	4.4	11.	11.4	.95	99.0
15	9	83	18	10.8	-.07	.98	5.3	10.	11.6	.94	99.0
15	9	83	19	11.0	-.03	.98	5.1	9.	11.5	.95	99.0
15	9	83	20	11.0	-.04	.98	4.4	7.	11.6	.95	99.0
15	9	83	21	10.9	-.06	.98	3.0	6.	11.5	.96	99.0
15	9	83	22	10.9	.00	.98	2.9	5.	11.5	.96	99.0
15	9	83	23	10.9	-.06	.98	1.4	1029.	11.4	.97	99.0
15	9	83	24	10.7	-.19	.98	1.5	27.	11.3	.97	99.0

			T-AS	DT-AS	RH-AS	F-AS	D-AS	T-BR	RH-BR	P-BR	
16	9	83	1	10.5	-.06	.98	1.5	23.	11.2	.97	99.0
16	9	83	2	10.2	.12	.98	.9	21.	10.9	.97	99.0
16	9	83	3	9.9	.09	.98	1.2	11.	10.3	.97	99.0
16	9	83	4	9.6	.18	.98	.9	14.	10.2	.97	99.0
16	9	83	5	9.7	.31	.98	.9	20.	9.3	.97	99.0
16	9	83	6	9.8	.05	.98	1.3	12.	9.9	.97	99.0
16	9	83	7	10.7	-.19	.98	2.0	16.	11.2	.97	99.0
16	9	83	8	12.2	-.23	.98	3.0	16.	13.2	.97	99.0
16	9	83	9	12.6	-.30	.98	3.7	17.	13.4	.93	99.0
16	9	83	10	13.0	-.32	.98	3.8	16.	13.5	.93	99.0
16	9	83	11	13.2	-.30	.98	3.8	16.	14.0	.88	99.0
16	9	83	12	13.1	-.24	.98	4.0	16.	14.3	.88	99.0
16	9	83	13	13.7	-.27	.98	3.9	16.	14.4	.87	99.0
16	9	83	14	13.9	-.29	.95	4.0	18.	14.4	.81	99.0
16	9	83	15	14.1	-.28	.93	3.4	18.	14.5	.80	99.0
16	9	83	16	13.3	-.14	.97	4.1	18.	14.2	.84	99.0
16	9	83	17	12.7	-.17	.98	3.2	17.	13.4	.89	99.0
16	9	83	18	12.4	-.09	.98	3.3	17.	13.3	.88	99.0
16	9	83	19	11.7	-.24	.98	4.1	16.	13.2	.94	99.0
16	9	83	20	11.3	-.30	.98	3.0	18.	12.5	.94	99.0
16	9	83	21	11.8	-.09	.98	3.2	17.	13.0	.93	99.0
16	9	83	22	12.0	-.17	.98	3.4	17.	13.2	.94	99.0
16	9	83	23	11.7	-.16	.98	2.8	16.	12.6	.94	99.0
16	9	83	24	11.5	-.20	.98	3.4	16.	13.0	.94	99.0
17	9	83	1	11.5	-.32	.98	3.4	16.	13.1	.91	99.0
17	9	83	2	11.4	-.38	.96	3.5	16.	13.1	.88	99.0
17	9	83	3	11.7	-.10	.97	3.1	16.	13.1	.90	99.0
17	9	83	4	11.8	-.21	.98	3.4	16.	13.0	.90	99.0
17	9	83	5	11.6	-.30	.98	3.5	15.	13.1	.90	99.0
17	9	83	6	10.4	-.86	.95	3.4	15.	12.5	.89	99.0
17	9	83	7	11.5	-.29	.98	4.0	14.	13.3	.91	99.0
17	9	83	8	12.2	-.27	.97	4.4	14.	13.4	.90	99.0
17	9	83	9	11.1	-.51	.98	3.3	17.	12.9	.96	99.0
17	9	83	10	12.6	-.29	.98	4.3	15.	13.4	.88	99.0
17	9	83	11	12.8	-.78	.89	4.1	15.	15.0	.77	99.0
17	9	83	12	12.0	-.84	.90	3.0	13.	14.3	.91	99.0
17	9	83	13	10.9	-.78	.97	3.7	16.	13.4	.90	99.0
17	9	83	14	12.3	-.90	.91	3.2	16.	14.4	.82	99.0
17	9	83	15	13.5	-.54	.83	2.2	18.	14.3	.72	99.0
17	9	83	16	14.9	-1.02	.79	1.8	16.	14.6	.76	99.0
17	9	83	17	13.6	-.75	.89	1.1	17.	14.3	.81	99.0
17	9	83	18	11.3	-.58	.97	.9	1014.	12.6	.97	99.0
17	9	83	19	9.3	-.51	.98	1.7	25.	10.5	.98	99.0
17	9	83	20	9.0	-.20	.98	1.1	29.	9.4	.98	99.0
17	9	83	21	7.7	-.63	.98	1.8	33.	9.4	.98	99.0
17	9	83	22	8.6	-.14	.98	1.5	32.	9.3	.98	99.0
17	9	83	23	9.3	-.20	.98	1.2	30.	9.2	.98	99.0
17	9	83	24	7.2	-.80	.98	.9	32.	9.3	.98	99.0
18	9	83	1	7.6	-1.08	.98	1.2	32.	8.5	.98	99.0
18	9	83	2	8.2	-.57	.98	2.0	30.	9.3	.98	99.0
18	9	83	3	7.7	-.61	.98	.9	25.	9.2	.98	99.0
18	9	83	4	7.5	-.19	.98	.7	18.	8.5	.98	99.0
18	9	83	5	6.8	.33	.96	2.1	13.	8.2	.98	99.0
18	9	83	6	6.5	.06	.98	1.6	12.	6.5	.98	99.0
18	9	83	7	7.1	.28	.98	1.2	15.	6.5	.98	99.0
18	9	83	8	10.5	.31	.98	.5	1025.	9.3	.98	99.0
18	9	83	9	10.9	-.29	.98	1.0	17.	10.0	.98	99.0
18	9	83	10	10.4	-.69	.95	2.1	22.	11.2	.82	99.0
18	9	83	11	12.4	-.85	.83	4.4	23.	14.2	.73	99.0
18	9	83	12	11.7	-1.15	.78	3.3	23.	14.4	.81	99.0
18	9	83	13	13.0	-.65	.85	4.4	20.	14.3	.78	99.0
18	9	83	14	13.1	-.19	.92	4.7	18.	13.8	.84	99.0
18	9	83	15	12.3	-.14	.98	5.3	18.	13.3	.92	99.0
18	9	83	16	11.3	-.16	.98	6.1	19.	12.3	.96	99.0
18	9	83	17	10.9	-.37	.98	6.1	19.	12.3	.96	99.0
18	9	83	18	11.8	-.14	.98	6.9	20.	12.5	.96	99.0
18	9	83	19	11.8	-.19	.98	7.3	19.	12.5	.96	99.0
18	9	83	20	11.6	-.29	.98	6.9	21.	12.9	.96	99.0
18	9	83	21	11.3	-.23	.98	4.5	21.	12.5	.95	99.0
18	9	83	22	9.5	-.52	.93	4.1	24.	12.0	.88	99.0
18	9	83	23	8.6	-.46	.92	3.6	25.	10.4	.89	99.0
18	9	83	24	8.6	-.10	.97	3.0	23.	10.1	.94	99.0

			T-AS	DT-AS	RH-AS	F-AS	D-AS	T-BR	RH-BR	P-BR	
19	9	83	1	8.5	.10	.97	2.5	23.	9.4	.95	99.0
19	9	83	2	7.4	.34	.98	2.6	21.	8.2	.98	99.0
19	9	83	3	7.3	.00	.98	2.4	19.	7.2	.98	99.0
19	9	83	4	8.8	.16	.97	2.4	20.	7.3	.98	99.0
19	9	83	5	8.6	-.02	.98	4.6	23.	9.8	.96	99.0
19	9	83	6	7.9	.36	.98	2.8	21.	7.5	.97	99.0
19	9	83	7	8.4	-.10	.97	2.7	20.	8.5	.97	99.0
19	9	83	8	11.1	-.35	.87	4.0	20.	11.0	.85	99.0
19	9	83	9	12.4	-.60	.83	4.2	20.	13.0	.79	99.0
19	9	83	10	12.6	-1.16	.76	5.7	23.	14.1	.74	99.0
19	9	83	11	12.7	-.76	.74	6.1	22.	14.0	.63	99.0
19	9	83	12	13.0	-.32	.81	7.5	22.	15.2	.71	99.0
19	9	83	13	10.3	-.90	.92	4.8	2022.	13.2	.81	99.0
19	9	83	14	90.0	99.00	99.00	99.0	99.	13.5	.77	99.0
19	9	83	15	13.4	-.23	.92	5.5	20.	13.2	.86	99.0
19	9	83	16	14.1	-.29	.82	5.9	22.	14.4	.75	99.0
19	9	83	17	13.4	-.15	.85	4.9	21.	13.5	.76	99.0
19	9	83	18	12.6	.06	.87	4.8	21.	13.2	.76	99.0
19	9	83	19	11.9	.13	.90	3.8	21.	12.3	.77	99.0
19	9	83	20	11.5	.16	.89	3.9	21.	12.1	.78	99.0
19	9	83	21	11.5	.11	.90	3.7	20.	12.1	.79	99.0
19	9	83	22	11.0	.17	.91	3.5	21.	11.6	.84	99.0
19	9	83	23	11.1	.20	.91	3.6	19.	10.8	.83	99.0
19	9	83	24	11.0	.24	.92	3.3	21.	11.2	.85	99.0
20	9	83	1	11.2	.24	.93	4.3	22.	11.3	.85	99.0
20	9	83	2	11.3	.21	.87	4.8	22.	11.5	.75	99.0
20	9	83	3	10.9	.19	.92	4.1	21.	10.4	.87	99.0
20	9	83	4	11.0	.16	.94	4.4	21.	11.3	.85	99.0
20	9	83	5	11.2	.14	.92	5.3	22.	11.6	.81	99.0
20	9	83	6	10.6	.14	.97	4.0	22.	10.9	.86	99.0
20	9	83	7	11.0	-.03	.93	3.6	22.	10.6	.85	99.0
20	9	83	8	12.3	-.22	.86	4.0	23.	12.1	.79	99.0
20	9	83	9	13.4	-.39	.78	4.1	23.	12.9	.73	99.0
20	9	83	10	12.9	-.11	.79	4.6	23.	14.0	.68	99.0
20	9	83	11	13.5	-.17	.76	4.3	23.	14.2	.65	99.0
20	9	83	12	14.0	-.13	.70	4.5	24.	14.4	.60	99.0
20	9	83	13	14.8	-.29	.69	4.1	23.	15.1	.60	99.0
20	9	83	14	13.7	-.07	.74	4.3	24.	14.3	.71	99.0
20	9	83	15	14.8	-.37	.69	5.1	23.	16.2	.56	99.0
20	9	83	16	14.1	-.22	.69	5.5	23.	15.7	.57	99.0
20	9	83	17	13.1	-.13	.71	5.4	24.	14.3	.60	99.0
20	9	83	18	11.8	-.01	.75	4.6	25.	12.7	.64	99.0
20	9	83	19	10.9	.05	.80	4.6	25.	11.4	.69	99.0
20	9	83	20	10.2	.07	.85	3.4	24.	11.2	.73	99.0
20	9	83	21	9.4	.07	.88	2.7	24.	10.1	.77	99.0
20	9	83	22	8.5	.22	.93	1.3	21.	9.3	.81	99.0
20	9	83	23	7.7	.37	.96	1.9	21.	9.2	.94	99.0
20	9	83	24	7.4	.30	.95	2.5	22.	8.3	.87	99.0
21	9	83	1	7.8	.24	.98	2.8	21.	8.3	.89	99.0
21	9	83	2	7.8	.14	.97	2.7	22.	8.2	.91	99.0
21	9	83	3	7.8	.20	.98	2.5	20.	8.3	.94	99.0
21	9	83	4	7.9	.13	.98	4.0	22.	8.4	.93	99.0
21	9	83	5	7.9	.05	.98	2.5	22.	8.5	.92	99.0
21	9	83	6	7.6	.12	.98	.9	1021.	8.6	.92	99.0
21	9	83	7	7.9	.04	.98	1.9	24.	8.7	.93	99.0
21	9	83	8	8.8	-.14	.96	1.6	23.	10.3	.80	.0
21	9	83	9	10.0	-.32	.90	1.4	23.	11.4	.75	.0
21	9	83	10	11.0	-.37	.83	1.3	25.	11.8	.69	.0
21	9	83	11	11.9	-.45	.79	2.0	23.	12.7	.65	.0
21	9	83	12	12.1	-.35	.75	2.5	24.	13.7	.60	.0
21	9	83	13	12.9	-.49	.71	2.7	24.	13.8	.59	.0
21	9	83	14	13.9	-.65	.65	2.4	23.	13.7	.65	.0
21	9	83	15	13.7	-.64	.67	2.4	20.	12.7	.61	.0
21	9	83	16	12.1	-.14	.76	2.4	20.	11.9	.86	.0
21	9	83	17	11.7	-.17	.74	2.7	20.	10.8	.76	.0
21	9	83	18	10.3	.14	.82	1.6	21.	8.0	.96	.0
21	9	83	19	8.7	.50	.92	1.4	15.	7.6	.97	.0
21	9	83	20	8.8	.30	.92	1.0	24.	7.2	.97	.0
21	9	83	21	8.0	.51	.97	.8	29.	6.7	.97	.0
21	9	83	22	7.2	.49	.98	.3	1015.	6.7	.97	.0
21	9	83	23	7.0	.37	.98	1.3	32.	6.3	.97	.0
21	9	83	24	6.1	.65	.97	2.3	35.	6.6	.93	.0

			T-AS	DT-AS	RH-AS	F-AS	D-AS	T-BR	RH-BR	P-BR	
22	9	83	1	6.0	.51	.98	3.1	34.	6.6	.93	.0
22	9	83	2	6.2	.14	.98	3.0	34.	6.1	.95	.0
22	9	83	3	6.0	.22	.98	2.8	34.	5.9	.95	.0
22	9	83	4	5.7	.20	.98	2.4	33.	5.6	.96	.0
22	9	83	5	5.7	.25	.98	3.1	33.	4.9	.96	.0
22	9	83	6	5.7	.24	.98	3.3	33.	4.9	.96	.0
22	9	83	7	5.8	.20	.95	3.3	32.	5.7	.91	.0
22	9	83	8	7.1	-.11	.86	3.8	32.	8.7	.65	.0
22	9	83	9	9.5	-.45	.74	3.8	32.	10.8	.54	.0
22	9	83	10	11.6	-.63	.64	4.0	32.	12.6	.46	.0
22	9	83	11	12.6	-.69	.57	4.3	32.	13.7	.39	.0
22	9	83	12	13.5	-.72	.52	5.1	32.	14.7	.37	.0
22	9	83	13	14.9	-.78	.48	4.5	32.	15.7	.35	.0
22	9	83	14	16.0	-.78	.43	2.9	31.	15.9	.32	.0
22	9	83	15	16.4	-.70	.40	3.3	31.	15.6	.33	.0
22	9	83	16	15.4	-.39	.40	4.6	31.	13.5	.38	.0
22	9	83	17	14.2	-.23	.43	4.8	31.	11.5	.48	.0
22	9	83	18	12.4	.07	.50	4.2	30.	10.4	.52	.0
22	9	83	19	10.9	.21	.56	3.2	30.	9.7	.61	.0
22	9	83	20	10.0	.26	.65	4.3	31.	8.7	.63	.0
22	9	83	21	9.5	.23	.68	3.2	31.	8.9	.64	.0
22	9	83	22	8.9	.22	.69	2.3	30.	6.8	.78	.0
22	9	83	23	7.5	.43	.83	2.0	31.	6.7	.91	.0
22	9	83	24	7.1	.46	.86	2.2	31.	6.3	.93	.0
23	9	83	1	6.8	.56	.86	2.4	33.	5.2	.92	.0
23	9	83	2	7.1	.56	.87	2.0	31.	5.6	.96	.0
23	9	83	3	6.4	.52	.91	1.6	31.	4.6	.96	.0
23	9	83	4	6.0	.64	.97	2.5	31.	4.1	.93	.0
23	9	83	5	6.1	.50	.95	3.4	34.	5.6	.96	.0
23	9	83	6	6.8	.47	.85	3.9	33.	3.9	.85	.0
23	9	83	7	8.5	.15	.76	3.4	33.	5.7	.64	.0
23	9	83	8	10.3	-.19	.69	4.5	32.	9.4	.51	.0
23	9	83	9	12.7	-.55	.63	3.4	32.	11.8	.48	.0
23	9	83	10	14.1	-.69	.55	3.2	33.	13.5	.43	.0
23	9	83	11	14.6	-.71	.53	2.8	32.	14.5	.38	.0
23	9	83	12	15.1	-.57	.47	1.9	31.	15.2	.37	.0
23	9	83	13	16.7	-.67	.39	1.0	10 17.	15.9	.44	.0
23	9	83	14	15.0	-.53	.48	2.5	16.	15.9	.49	.0
23	9	83	15	13.3	-.19	.59	3.0	19.	13.7	.56	.0
23	9	83	16	12.4	-.05	.66	2.9	20.	13.2	.56	.0
23	9	83	17	12.0	.07	.68	3.5	20.	12.7	.66	.0
23	9	83	18	11.5	.14	.76	2.6	18.	12.3	.90	.0
23	9	83	19	11.4	.19	.94	1.7	17.	11.7	.64	.0
23	9	83	20	11.3	.22	.86	2.0	22.	12.4	.64	.0
23	9	83	21	11.5	.09	.78	2.7	23.	12.2	.86	.0
23	9	83	22	10.2	.10	.85	2.9	25.	10.7	.91	.9
23	9	83	23	8.9	.32	.98	2.3	22.	9.7	.87	.0
23	9	83	24	9.3	.24	.98	3.5	20.	10.7	.86	.0
24	9	83	1	9.9	.14	.98	4.6	20.	11.0	.86	.0
24	9	83	2	10.4	.11	.98	3.4	20.	11.7	.84	.0
24	9	83	3	11.1	.08	.97	3.5	21.	12.4	.82	.0
24	9	83	4	11.4	.06	.96	4.4	21.	12.3	.85	.0
24	9	83	5	11.6	.12	.97	4.1	21.	12.5	.90	.1
24	9	83	6	12.1	.13	.98	3.9	22.	13.5	.84	.1
24	9	83	7	12.9	.05	.96	4.1	24.	13.7	.84	.0
24	9	83	8	13.0	.02	.97	4.0	24.	13.9	.83	.0
24	9	83	9	13.4	-.07	.97	3.6	23.	14.9	.79	.0
24	9	83	10	14.3	-.08	.92	5.3	24.	15.9	.74	.0
24	9	83	11	15.5	-.13	.87	5.0	22.	17.6	.69	.0
24	9	83	12	17.0	-.24	.77	5.0	23.	17.9	.59	.0
24	9	83	13	17.7	-.06	.67	5.6	27.	17.3	.51	.0
24	9	83	14	16.7	-.07	.60	7.4	32.	12.7	.55	.0
24	9	83	15	12.1	-.13	.65	8.7	0.	13.3	.45	.0
24	9	83	16	13.0	-.15	.55	7.4	0.	13.4	.43	.0
24	9	83	17	12.5	.01	.52	8.5	0.	12.0	.45	.0
24	9	83	18	11.7	.15	.52	5.7	36.	11.6	.43	.0
24	9	83	19	10.9	.16	.49	6.6	0.	10.9	.40	.0
24	9	83	20	10.3	.13	.46	6.8	1.	9.8	.42	.0
24	9	83	21	9.3	.21	.50	5.1	1.	9.5	.44	.0
24	9	83	22	8.6	.22	.48	5.0	0.	6.2	.59	.0
24	9	83	23	7.8	.22	.48	4.5	2.	5.7	.59	.0
24	9	83	24	6.6	.37	.52	2.5	4.	4.2	.73	.0

			T-AS	DT-AS	RH-AS	F-AS	D-AS	T-BR	RH-BR	P-BR
25	9 83	1	5.1	.71	.61	1.6	0.	2.7	.85	.0
25	9 83	2	4.0	.52	.62	.5	3.	1.7	.94	.0
25	9 83	3	3.8	.65	.87	.5	1031.	1.7	.96	.0
25	9 83	4	2.8	.81	.97	.3	1012.	1.4	.98	.0
25	9 83	5	3.1	.56	.95	1.1	29.	1.6	.98	.0
25	9 83	6	3.3	.50	.98	1.3	26.	3.1	.93	.0
25	9 83	7	4.2	.25	.98	1.4	31.	5.7	.81	.0
25	9 83	8	5.9	-.17	.87	.4	1009.	6.5	.76	.0
25	9 83	9	6.2	.02	.87	.9	15.	7.5	.75	.0
25	9 83	10	7.8	-.11	.86	1.7	21.	9.4	.75	.0
25	9 83	11	9.3	-.17	.80	2.2	22.	11.4	.69	.0
25	9 83	12	10.6	-.29	.80	1.7	22.	11.4	.55	.0
25	9 83	13	10.5	-.05	.62	2.4	25.	10.7	.51	.0
25	9 83	14	10.4	.04	.52	3.8	25.	10.8	.46	.0
25	9 83	15	10.6	.00	.51	4.5	24.	10.8	.49	.0
25	9 83	16	10.5	.06	.56	3.6	23.	10.9	.49	.0
25	9 83	17	11.8	.00	.52	5.4	28.	11.6	.49	.0
25	9 83	18	11.4	.04	.56	2.9	25.	10.9	.51	.0
25	9 83	19	11.0	.14	.57	3.9	28.	10.5	.54	.0
25	9 83	20	10.2	.14	.60	3.4	24.	9.8	.56	.0
25	9 83	21	9.5	.12	.63	4.4	25.	8.7	.61	.0
25	9 83	22	9.0	.14	.65	3.0	25.	8.6	.61	.0
25	9 83	23	7.1	.35	.75	1.6	20.	7.9	.65	.0
25	9 83	24	6.0	.50	.84	1.6	16.	8.2	.65	.0
26	9 83	1	7.1	.32	.82	2.4	13.	8.5	.69	.0
26	9 83	2	7.9	.26	.80	2.8	22.	8.4	.70	.0
26	9 83	3	8.2	.19	.82	2.1	19.	8.8	.70	.0
26	9 83	4	8.0	.34	.85	1.8	25.	6.7	.88	.0
26	9 83	5	7.4	.37	.91	1.0	22.	6.6	.93	.0
26	9 83	6	8.0	.28	.90	2.1	26.	5.8	.96	.0
26	9 83	7	9.2	.42	.88	2.0	27.	7.3	.91	.0
26	9 83	8	9.4	.18	.92	.8	17.	9.8	.79	.0
26	9 83	9	11.4	-.28	.87	1.0	1022.	12.6	.69	.0
26	9 83	10	14.2	-.51	.76	1.2	23.	15.2	.56	.0
26	9 83	11	16.2	-.62	.69	1.9	24.	17.5	.51	.0
26	9 83	12	17.4	-.57	.63	2.7	30.	18.6	.46	.0
26	9 83	13	19.7	-.78	.56	1.4	25.	18.9	.54	.0
26	9 83	14	19.0	-.59	.62	1.7	14.	19.8	.50	.0
26	9 83	15	18.7	-.37	.60	1.8	10.	18.7	.52	.0
26	9 83	16	19.5	-.58	.66	.9	7.	18.2	.61	.0
26	9 83	17	17.4	-.03	.71	1.4	1003.	13.7	.92	.0
26	9 83	18	13.9	.72	.91	1.7	1014.	11.7	.95	.0
26	9 83	19	14.0	.29	.84	1.0	19.	13.5	.76	.0
26	9 83	20	13.5	.35	.89	1.2	13.	13.8	.73	.0
26	9 83	21	13.0	.19	.90	2.2	23.	13.4	.77	.0
26	9 83	22	11.9	.29	.96	2.7	21.	12.6	.80	.0
26	9 83	23	11.4	.18	.98	2.4	22.	11.8	.84	.0
26	9 83	24	11.0	.19	.98	2.8	22.	11.8	.89	.0
27	9 83	1	11.0	.27	.98	3.0	23.	11.8	.91	.0
27	9 83	2	11.0	.31	.98	2.0	23.	11.2	.95	.0
27	9 83	3	10.0	.41	.98	1.4	21.	9.9	.99	.0
27	9 83	4	9.5	.80	.98	1.2	19.	9.6	.98	.0
27	9 83	5	10.1	.44	.98	1.7	17.	10.5	.97	.0
27	9 83	6	11.2	.19	.95	1.8	18.	11.9	.93	.0
27	9 83	7	12.3	.01	.95	2.8	20.	13.6	.84	.0
27	9 83	8	14.4	-.29	.89	3.8	22.	15.0	.77	.0
27	9 83	9	15.9	-.30	.84	3.5	22.	17.2	.64	.0
27	9 83	10	18.5	-.25	.67	4.2	26.	19.4	.51	.0
27	9 83	11	18.8	-.06	.60	6.3	28.	18.8	.52	.0
27	9 83	12	18.5	-.05	.59	6.4	28.	18.9	.50	.0
27	9 83	13	18.8	-.10	.57	6.8	27.	19.5	.48	.0
27	9 83	14	18.7	-.14	.57	4.5	27.	18.8	.49	.0
27	9 83	15	18.8	-.17	.56	5.4	29.	18.0	.48	.0
27	9 83	16	19.0	-.10	.55	7.0	29.	18.8	.47	.0
27	9 83	17	17.6	-.05	.56	9.3	29.	17.5	.48	.0
27	9 83	18	18.1	.07	.57	6.5	31.	18.2	.50	.0
27	9 83	19	14.7	.11	.55	5.8	31.	15.3	.48	.0
27	9 83	20	13.4	.09	.55	5.1	31.	13.7	.47	.0
27	9 83	21	12.2	.09	.51	6.4	31.	12.5	.44	.0
27	9 83	22	11.1	.09	.50	5.9	32.	11.5	.44	.0
27	9 83	23	10.0	.14	.50	3.8	33.	10.5	.46	.0
27	9 83	24	9.2	.18	.53	3.9	31.	8.6	.53	.0

	T-AS	DT-AS	RH-AS	F-AS	D-AS	T-BR	RH-BR	P-BR
28 9 83 1	8.6	.13	.55	3.6	30.	7.8	.53	.0
28 9 83 2	7.7	.19	.56	4.0	31.	7.8	.49	.0
28 9 83 3	7.0	.23	.57	3.7	32.	5.7	.61	.0
28 9 83 4	6.0	.21	.59	1.8	27.	5.8	.57	.0
28 9 83 5	5.1	.23	.64	1.6	28.	4.5	.71	.0
28 9 83 6	3.8	.36	.74	.8	3.	2.5	.87	.0
28 9 83 7	5.6	.17	.72	2.1	28.	3.4	.71	.0
28 9 83 8	7.1	-.12	.65	3.2	31.	8.4	.48	.0
28 9 83 9	9.4	-.44	.54	3.8	31.	10.0	.40	.0
28 9 83 10	10.1	-.47	.46	5.8	32.	11.0	.35	.0
28 9 83 11	10.8	-.52	.42	6.3	31.	11.9	.34	.0
28 9 83 12	11.7	-.57	.41	6.1	32.	12.9	.32	.0
28 9 83 13	12.8	-.65	.38	5.2	32.	13.2	.32	.0
28 9 83 14	12.1	-.30	.38	5.7	31.	13.0	.30	.0
28 9 83 15	13.3	-.43	.33	4.6	32.	13.6	.27	.0
28 9 83 16	12.8	-.32	.28	5.4	33.	12.8	.28	.0
28 9 83 17	11.3	-.08	.32	4.8	33.	10.2	.35	.0
28 9 83 18	9.5	.22	.38	3.4	32.	8.0	.49	.0
28 9 83 19	8.7	.21	.45	3.0	33.	7.3	.50	.0
28 9 83 20	8.3	.20	.43	3.4	35.	8.0	.45	.0
28 9 83 21	7.8	.21	.45	3.9	34.	7.9	.51	.0
28 9 83 22	7.5	.17	.45	2.7	0.	7.0	.58	.0
28 9 83 23	7.1	.22	.47	3.0	35.	6.0	.61	.0
28 9 83 24	6.5	.34	.49	2.8	35.	4.2	.79	.0
29 9 83 1	5.2	.53	.55	2.1	35.	3.3	.81	.0
29 9 83 2	4.4	.52	.59	2.1	35.	2.7	.84	.0
29 9 83 3	4.4	.45	.63	2.1	34.	2.2	.86	.0
29 9 83 4	3.6	.80	.86	1.9	34.	2.2	.94	.0
29 9 83 5	3.1	.78	.83	2.2	34.	1.9	.96	.0
29 9 83 6	3.2	.61	.77	2.7	35.	2.0	.90	.0
29 9 83 7	3.5	.36	.79	2.4	35.	2.9	.81	.0
29 9 83 8	4.4	-.07	.82	2.4	35.	4.7	.69	.0
29 9 83 9	7.4	-.51	.75	1.8	33.	8.0	.55	.0
29 9 83 10	9.1	-.84	.68	1.9	33.	10.1	.46	.0
29 9 83 11	9.9	-.72	.54	1.7	32.	11.0	.35	.0
29 9 83 12	10.1	-.42	.48	1.8	29.	12.1	.30	.0
29 9 83 13	11.3	-.63	.42	1.9	29.	12.1	.29	.0
29 9 83 14	12.3	-.69	.34	2.0	30.	12.8	.28	.0
29 9 83 15	13.2	-1.09	.31	1.3	31.	12.8	.28	.0
29 9 83 16	12.1	-.66	.31	1.8	31.	12.6	.36	.0
29 9 83 17	11.4	-.83	.34	.9	33.	7.0	.69	.0
29 9 83 18	7.4	.24	.51	1.5	22.	4.3	.78	.0
29 9 83 19	6.1	.43	.59	1.7	26.	3.0	.87	.0
29 9 83 20	3.8	1.09	.91	1.6	31.	1.2	.93	.0
29 9 83 21	3.1	.83	.89	2.5	32.	1.0	.98	.0
29 9 83 22	3.0	.53	.75	3.6	34.	.0	.91	.0
29 9 83 23	2.3	.49	.78	3.7	34.	1.7	.81	.0
29 9 83 24	1.7	.64	.88	3.3	33.	1.9	.74	.0
30 9 83 1	1.5	1.10	.97	2.7	33.	3.1	.64	.0
30 9 83 2	1.5	1.00	.96	3.4	33.	3.0	.70	.0
30 9 83 3	1.3	.93	.93	2.5	33.	2.2	.75	.0
30 9 83 4	.9	1.09	.95	2.8	33.	.8	.86	.0
30 9 83 5	1.0	.69	.96	2.9	31.	1.5	.84	.0
30 9 83 6	1.0	.41	.96	3.0	31.	.0	.94	.0
30 9 83 7	1.5	.09	.98	3.1	31.	1.2	.90	.0
30 9 83 8	3.5	-.38	.93	2.3	32.	2.9	.79	.0
30 9 83 9	5.9	-.68	.81	2.0	33.	5.5	.66	.0
30 9 83 10	7.5	-.86	.70	2.0	31.	7.0	.52	.0
30 9 83 11	8.9	-.84	.56	2.4	32.	9.2	.40	.0
30 9 83 12	9.5	-.88	.47	2.0	32.	10.1	.36	.0
30 9 83 13	10.6	-.66	.39	2.3	31.	11.6	.31	.0
30 9 83 14	11.9	-.85	.34	2.8	30.	11.9	.30	.0
30 9 83 15	11.8	-.73	.32	3.1	31.	12.0	.29	.0
30 9 83 16	11.3	-.57	.33	2.6	30.	11.9	.31	.0
30 9 83 17	10.4	-.47	.36	1.4	27.	7.4	.59	.0
30 9 83 18	6.7	.17	.52	1.3	20.	5.9	.67	.0
30 9 83 19	5.0	.51	.67	1.4	20.	4.0	.79	.0
30 9 83 20	4.1	.42	.73	1.4	27.	2.2	.90	.0
30 9 83 21	3.2	.53	.88	1.0	32.	1.0	.95	.0
30 9 83 22	2.5	1.07	.96	1.7	33.	.2	.99	.0
30 9 83 23	1.8	.72	.82	3.4	35.	-.1	.98	.0
30 9 83 24	1.0	.65	.88	2.9	34.	-.9	.98	.0
AMT. 99.	7	4	4	4	4	0	4	334
PERCENT 99.	1.0	.6	.6	.6	.6	.0	.6	40.4

	T-AS	DT-AS	RH-AS	F-AS	D-AS	T-BR	RH-BR	P-BR
1 10 83 1	.5	.56	.98	2.3	34.	-.1	.98	.0
1 10 83 2	.2	.59	.98	2.6	34.	.0	.98	.0
1 10 83 3	.0	.56	.98	2.6	33.	.0	.98	.0
1 10 83 4	-.4	.47	.98	2.3	34.	-.2	.98	.0
1 10 83 5	-.5	.39	.98	2.7	34.	.0	.95	.0
1 10 83 6	-1.2	.49	.98	1.9	33.	-.2	.95	.0
1 10 83 7	-.3	.15	.98	2.2	33.	.1	.95	.0
1 10 83 8	1.8	-.34	.96	2.1	33.	1.8	.86	.0
1 10 83 9	5.1	-.69	.82	1.4	35.	5.3	.69	.0
1 10 83 10	7.1	-.70	.77	1.2	33.	8.2	.61	.0
1 10 83 11	8.1	-.61	.70	1.5	30.	10.6	.53	.0
1 10 83 12	10.3	-.49	.63	.8	1016.	11.7	.53	.0
1 10 83 13	12.1	-.55	.60	1.0	1025.	13.1	.49	.0
1 10 83 14	12.8	-.86	.54	2.5	22.	12.7	.49	.0
1 10 83 15	13.1	-.69	.44	2.9	22.	13.9	.46	.0
1 10 83 16	11.6	-.44	.53	3.8	22.	12.0	.53	.0
1 10 83 17	8.8	.02	.69	4.7	22.	9.9	.57	.0
1 10 83 18	7.8	.14	.71	3.5	21.	8.8	.62	.0
1 10 83 19	7.2	.14	.76	3.6	22.	8.2	.64	.0
1 10 83 20	6.9	.12	.76	3.2	23.	8.1	.61	.0
1 10 83 21	6.9	.09	.75	3.8	25.	8.0	.64	.0
1 10 83 22	6.8	.07	.79	2.8	26.	7.2	.74	.0
1 10 83 23	6.4	.11	.83	1.5	26.	6.0	.89	.0
1 10 83 24	5.1	.34	.90	1.1	26.	5.0	.93	.0
2 10 83 1	5.7	.20	.89	1.5	27.	5.1	.93	.0
2 10 83 2	5.1	.25	.95	.9	32.	5.2	.93	.0
2 10 83 3	4.9	.50	.98	.3	36.	5.2	.94	.0
2 10 83 4	5.1	.62	.97	1.1	13.	5.3	.96	.0
2 10 83 5	5.6	.69	.95	1.3	15.	5.4	.95	.0
2 10 83 6	5.4	.38	.98	1.1	1003.	6.0	.94	.0
2 10 83 7	5.2	.35	.98	1.1	1030.	6.0	.97	.1
2 10 83 8	5.6	.16	.98	1.3	1.	6.6	.97	1.0
2 10 83 9	5.7	.05	.98	1.2	33.	6.9	.97	1.0
2 10 83 10	6.0	-.08	.98	.7	35.	7.0	.97	.9
2 10 83 11	6.6	-.13	.98	.8	34.	7.3	.97	.6
2 10 83 12	6.9	-.17	.98	1.4	32.	8.2	.97	.9
2 10 83 13	7.3	-.21	.98	1.3	32.	8.2	.97	1.0
2 10 83 14	7.7	-.21	.98	1.4	31.	9.0	.97	.2
2 10 83 15	7.6	-.12	.98	1.0	30.	9.0	.93	.0
2 10 83 16	8.0	-.19	.97	.7	29.	9.0	.94	.0
2 10 83 17	8.0	-.14	.97	.9	25.	8.9	.96	.0
2 10 83 18	7.3	.11	.98	1.1	24.	7.9	.98	.0
2 10 83 19	6.2	.26	.98	1.0	25.	6.2	.98	.0
2 10 83 20	6.5	.15	.98	1.1	23.	7.3	.98	.0
2 10 83 21	6.6	.01	.98	1.5	25.	7.1	.98	.0
2 10 83 22	6.3	.00	.98	1.6	31.	7.0	.98	.0
2 10 83 23	6.0	-.01	.98	2.1	31.	7.0	.98	.0
2 10 83 24	5.8	-.02	.98	2.0	32.	7.0	.98	.0
3 10 83 1	5.6	.00	.98	1.8	32.	6.9	.98	.0
3 10 83 2	5.6	-.01	.98	1.0	31.	6.8	.93	.0
3 10 83 3	5.4	-.01	.98	1.9	32.	6.7	.98	.0
3 10 83 4	5.4	-.01	.98	2.2	31.	6.4	.98	.0
3 10 83 5	5.6	.00	.98	1.9	32.	6.8	.98	.0
3 10 83 6	5.5	.00	.98	2.0	34.	6.8	.98	.0
3 10 83 7	5.6	.01	.98	2.6	35.	6.9	.98	.0
3 10 83 8	6.3	-.06	.98	.9	1001.	7.3	.96	.0
3 10 83 9	7.0	-.17	.98	1.6	32.	8.2	.94	.0
3 10 83 10	8.6	-.41	.98	1.3	1024.	9.8	.95	.0
3 10 83 11	11.2	-.58	.94	.7	22.	11.1	.80	.0
3 10 83 12	11.5	-.37	.95	1.2	15.	12.6	.81	.0
3 10 83 13	11.1	-.21	.98	2.1	12.	11.1	.87	.0
3 10 83 14	11.8	-.15	.98	2.1	13.	13.8	.89	.0
3 10 83 15	12.3	-.02	.98	1.6	16.	13.3	.91	.0
3 10 83 16	12.0	-.06	.98	2.1	19.	13.0	.95	.0
3 10 83 17	11.8	-.04	.98	1.4	17.	13.0	.96	.0
3 10 83 18	11.4	.05	.98	1.5	15.	12.8	.96	.0
3 10 83 19	11.2	.09	.98	1.4	14.	12.7	.97	.0
3 10 83 20	11.0	.13	.98	1.1	15.	12.5	.97	.0
3 10 83 21	10.5	.27	.98	1.1	13.	10.8	.97	.0
3 10 83 22	10.3	.30	.98	1.4	24.	10.2	.97	.0
3 10 83 23	9.4	.42	.98	2.0	27.	9.3	.97	.0
3 10 83 24	8.7	.49	.98	2.7	32.	8.9	.97	.0

	T-AS	DT-AS	RH-AS	F-AS	D-AS	T-BR	RH-BR	P-BR
4 10 83 1	8.3	.43	.98	2.5	32.	8.0	.97	.0
4 10 83 2	8.1	.48	.98	1.9	32.	7.8	.97	.0
4 10 83 3	6.8	.66	.98	.8	35.	8.8	.97	.0
4 10 83 4	6.7	.82	.98	.8	1008.	8.9	.97	.0
4 10 83 5	6.6	.57	.98	1.0	31.	7.2	.97	.0
4 10 83 6	7.1	.15	.98	1.3	32.	7.1	.97	.0
4 10 83 7	7.6	-.01	.98	1.5	32.	8.1	.97	.0
4 10 83 8	7.5	.04	.98	2.1	33.	8.9	.97	.0
4 10 83 9	7.6	.02	.98	1.2	32.	9.0	.97	.1
4 10 83 10	8.5	.17	.98	.6	20.	9.7	.97	.1
4 10 83 11	9.6	.08	.98	.5	12.	10.0	.97	.4
4 10 83 12	9.0	.02	.98	.5	9.	10.9	.97	.2
4 10 83 13	9.8	-.06	.98	1.7	13.	11.1	.96	1.1
4 10 83 14	10.2	-.01	.98	1.6	13.	11.7	.96	.5
4 10 83 15	10.7	.00	.98	2.1	12.	12.0	.96	.5
4 10 83 16	11.2	.04	.98	2.1	13.	12.3	.96	.2
4 10 83 17	11.3	.00	.98	3.4	13.	13.0	.96	.2
4 10 83 18	11.4	.02	.98	3.3	13.	12.9	.96	.0
4 10 83 19	11.7	.04	.98	2.9	13.	13.0	.96	.0
4 10 83 20	12.0	.04	.98	2.3	17.	13.1	.96	.0
4 10 83 21	12.1	.04	.98	2.2	17.	13.3	.96	.0
4 10 83 22	12.2	.04	.98	2.6	18.	13.5	.96	.1
4 10 83 23	12.2	.03	.98	3.3	18.	13.5	.96	.1
4 10 83 24	12.3	.05	.98	3.0	17.	13.7	.96	.5
5 10 83 1	12.5	.05	.98	4.6	19.	13.8	.96	1.4
5 10 83 2	12.6	.04	.98	4.0	19.	14.0	.96	.0
5 10 83 3	12.7	.08	.98	4.7	21.	14.0	.96	.0
5 10 83 4	12.4	.21	.98	4.2	20.	14.2	.96	.0
5 10 83 5	12.1	.16	.98	4.4	21.	13.8	.96	.0
5 10 83 6	12.2	.07	.96	4.1	22.	13.6	.94	.0
5 10 83 7	12.0	.04	.96	5.6	21.	13.8	.90	.0
5 10 83 8	12.2	-.06	.91	6.4	23.	13.2	.88	.0
5 10 83 9	12.9	-.11	.86	7.4	23.	13.8	.82	.0
5 10 83 10	13.9	-.19	.76	7.7	23.	14.1	.76	.0
5 10 83 11	13.7	-.12	.73	7.1	24.	15.2	.66	.0
5 10 83 12	14.5	-.22	.69	7.6	24.	14.0	99.00	.0
5 10 83 13	14.1	-.16	.70	7.2	24.	99.0	99.00	.0
5 10 83 14	14.2	-.09	.67	7.8	24.	99.0	99.00	.0
5 10 83 15	14.1	-.11	.69	6.4	24.	99.0	99.00	.0
5 10 83 16	14.0	-.01	.65	6.7	25.	14.9	.58	.0
5 10 83 17	13.2	.02	.67	6.4	25.	14.1	.60	.0
5 10 83 18	12.4	.04	.73	5.6	24.	13.7	.64	.0
5 10 83 19	12.2	.03	.75	6.1	24.	13.2	.66	.0
5 10 83 20	11.9	.05	.77	5.0	24.	13.0	.68	.0
5 10 83 21	11.7	.05	.79	4.7	24.	13.0	.69	.0
5 10 83 22	11.6	.04	.81	4.9	23.	12.9	.71	.0
5 10 83 23	11.2	.06	.80	3.7	23.	12.4	.73	.0
5 10 83 24	10.7	.05	.86	2.6	25.	11.8	.79	.0
6 10 83 1	10.2	.12	.89	1.8	27.	10.1	.94	.0
6 10 83 2	9.8	.19	.95	2.4	30.	10.0	.94	.0
6 10 83 3	9.5	.26	.95	2.2	33.	10.0	.89	.1
6 10 83 4	9.3	.04	.93	5.9	36.	10.5	.81	.0
6 10 83 5	7.4	.08	.98	4.5	1.	8.6	.88	.0
6 10 83 6	6.3	.11	.96	4.6	1.	7.2	.89	1.0
6 10 83 7	6.2	.14	.90	4.4	34.	6.8	.93	1.2
6 10 83 8	6.8	.01	.89	4.3	32.	7.9	.80	.3
6 10 83 9	8.1	-.08	.82	4.3	33.	8.9	.71	.0
6 10 83 10	10.7	-.45	.68	4.7	33.	11.6	.54	.0
6 10 83 11	11.8	-.43	.53	5.7	33.	13.1	.43	.0
6 10 83 12	12.6	-.49	.43	5.6	33.	14.0	.36	.0
6 10 83 13	13.5	-.46	.37	6.6	32.	14.8	.31	.0
6 10 83 14	13.9	-.45	.33	6.3	32.	14.6	.29	.1
6 10 83 15	13.5	-.37	.32	6.3	32.	14.2	.29	.0
6 10 83 16	13.3	-.30	.31	4.2	33.	13.0	.30	.0
6 10 83 17	11.6	-.05	.38	3.5	32.	9.0	.56	.0
6 10 83 18	9.0	.34	.51	2.1	32.	6.1	.74	.0
6 10 83 19	7.6	.54	.60	1.9	32.	5.1	.81	.0
6 10 83 20	6.5	.86	.65	2.3	31.	4.9	.82	.0
6 10 83 21	5.5	1.00	.79	2.2	31.	3.1	.91	.0
6 10 83 22	4.3	.89	.95	2.8	30.	2.9	.96	.0
6 10 83 23	3.5	.80	.92	2.4	32.	3.0	.94	.0
6 10 83 24	2.9	1.07	.90	2.7	32.	2.5	.95	.0

	T-ÅS	DT-ÅS	RH-ÅS	F-ÅS	D-ÅS	T-BR	RH-BR	P-BR
7 10 83 1	2.3	1.25	.96	2.6	32.	1.9	.97	.0
7 10 83 2	2.1	.67	.98	2.8	31.	2.0	.97	.0
7 10 83 3	2.0	.52	.98	2.8	32.	2.0	.97	.0
7 10 83 4	1.9	.77	.97	3.2	32.	1.3	.98	.0
7 10 83 5	2.0	.53	.98	2.7	34.	2.0	.98	.0
7 10 83 6	1.9	.38	.97	2.5	33.	2.7	.93	.0
7 10 83 7	1.9	.33	.98	1.7	34.	2.8	.94	.0
7 10 83 8	2.7	.09	.98	1.6	1030.	3.7	.91	.0
7 10 83 9	3.7	-.13	.95	1.0	29.	5.0	.82	.0
7 10 83 10	5.2	-.24	.91	1.0	1034.	6.2	.78	.0
7 10 83 11	6.4	-.33	.80	1.1	33.	7.5	.73	.0
7 10 83 12	7.1	-.22	.77	1.0	31.	8.0	.67	.0
7 10 83 13	8.1	-.36	.71	.9	0.	9.0	.64	.0
7 10 83 14	8.5	-.25	.72	.5	25.	9.1	.56	.0
7 10 83 15	8.3	-.27	.68	.9	14.	9.1	.59	.0
7 10 83 16	7.9	-.16	.73	1.1	11.	9.0	.67	.0
7 10 83 17	7.3	.06	.83	1.1	12.	8.1	.81	.0
7 10 83 18	6.9	.21	.94	.9	2.	8.1	.85	.0
7 10 83 19	7.0	.14	.91	1.7	33.	8.1	.84	.0
7 10 83 20	6.2	.24	.90	2.0	31.	6.9	.87	.0
7 10 83 21	5.9	.11	.98	2.7	31.	6.2	.88	.0
7 10 83 22	5.3	.17	.97	2.5	32.	5.8	.94	.0
7 10 83 23	5.5	.31	.96	2.2	31.	5.6	.95	.0
7 10 83 24	4.9	.77	.96	2.7	32.	5.2	.93	.0
8 10 83 1	5.2	.53	.92	2.6	30.	5.0	.81	.0
8 10 83 2	6.2	.26	.75	3.1	28.	6.0	.68	.0
8 10 83 3	6.1	.22	.73	3.0	29.	3.3	.88	.0
8 10 83 4	5.4	.32	.75	2.2	29.	5.0	.73	.0
8 10 83 5	4.7	.38	.83	2.2	32.	3.9	.89	.0
8 10 83 6	4.8	.42	.79	2.7	31.	3.2	.86	.0
8 10 83 7	4.6	.42	.85	2.7	31.	2.2	.94	.0
8 10 83 8	6.5	.08	.78	1.5	27.	4.5	.91	.0
9 10 83 9	8.7	-.47	.68	2.0	31.	7.9	.62	.0
8 10 83 10	10.2	-.73	.64	2.4	31.	10.0	.52	.0
8 10 83 11	10.8	-.66	.53	3.5	32.	11.3	.44	.0
8 10 83 12	11.4	-.69	.47	3.2	31.	12.0	.40	.0
8 10 83 13	12.8	-.77	.41	2.6	31.	12.6	.36	.0
8 10 83 14	12.7	-.56	.40	2.1	30.	12.5	.35	.0
8 10 83 15	11.1	-.24	.46	1.1	36.	11.8	.41	.0
8 10 83 16	10.2	-.21	.56	1.9	12.	10.7	.56	.0
8 10 83 17	8.1	.01	.81	2.1	12.	9.0	.72	.0
8 10 83 18	7.0	.25	.89	2.4	14.	6.6	.89	.0
8 10 83 19	6.3	.24	.95	1.1	1013.	6.0	.94	.0
8 10 83 20	6.4	.23	.95	1.4	25.	5.9	.95	.0
8 10 83 21	5.7	.34	.96	1.7	29.	5.0	.96	.0
8 10 83 22	4.2	.67	.98	2.7	32.	3.1	.97	.0
8 10 83 23	3.6	.58	.90	2.8	32.	2.1	.98	.0
8 10 83 24	3.2	.46	.97	3.3	31.	2.1	.98	.0
9 10 83 1	2.9	.45	.98	3.0	32.	1.9	.98	.0
9 10 83 2	2.6	.39	.97	2.5	33.	1.1	.99	.0
9 10 83 3	1.9	.69	.96	1.8	32.	1.2	.99	.0
9 10 83 4	1.6	.70	.98	1.6	31.	.7	.99	.0
9 10 83 5	1.5	.43	.98	1.6	30.	.1	.99	.0
9 10 83 6	1.6	.41	.98	2.9	31.	1.0	.99	.0
9 10 83 7	1.7	.71	.98	2.1	33.	1.0	.99	.0
9 10 83 8	2.6	.38	.95	2.6	32.	2.9	.95	.0
9 10 83 9	3.9	-.03	.96	2.2	33.	4.7	.89	.0
9 10 83 10	5.7	-.29	.87	2.2	32.	6.0	.81	.0
9 10 83 11	8.9	-.84	.68	2.2	30.	9.6	.54	.0
9 10 83 12	11.1	-.91	.53	1.9	31.	11.1	.53	.0
9 10 83 13	11.7	-.64	.46	1.8	35.	12.2	.44	.0
9 10 83 14	12.1	-.56	.38	1.7	34.	12.2	.37	.0
9 10 83 15	12.7	-.49	.35	2.0	29.	12.2	.34	.0
9 10 83 16	13.3	-.83	.32	1.6	32.	11.8	.39	.0
9 10 83 17	10.5	-.61	.41	1.0	22.	6.2	.61	.0
9 10 83 18	6.9	.45	.69	2.2	22.	6.9	.64	.0
9 10 83 19	6.8	.32	.71	2.7	24.	4.0	.86	.0
9 10 83 20	5.1	.34	.79	.9	25.	2.2	.94	.0
9 10 83 21	4.1	.58	.87	.6	21.	1.2	.97	.0
9 10 83 22	3.2	1.24	.97	.6	1003.	.9	.97	.0
9 10 83 23	2.4	1.67	.98	.8	33.	.1	.98	.0
9 10 83 24	1.4	1.07	.90	2.6	34.	-.8	.98	.0

	T-AS	DT-AS	RH-AS	F-AS	D-AS	T-BR	RH-BR	D-BR
10 10 83 1	1.2	.97	.93	2.4	34.	-.9	.98	.0
10 10 83 2	.7	.52	.98	2.3	34.	-1.1	.98	.0
10 10 83 3	.2	.87	.98	2.1	34.	-1.2	.98	.0
10 10 83 4	.3	.46	.98	2.3	33.	.2	.98	.0
10 10 83 5	.8	.12	.98	1.8	32.	1.1	.98	.0
10 10 83 6	1.0	.41	.98	1.7	34.	1.9	.98	.0
10 10 83 7	1.4	.71	.98	1.6	33.	2.2	.98	.2
10 10 83 8	2.1	.93	.98	.8	1033.	3.6	.98	.8
10 10 83 9	3.5	.76	.98	1.9	15.	7.3	.97	1.3
10 10 83 10	6.7	.04	.98	3.6	16.	8.1	.97	1.6
10 10 83 11	7.4	-.03	.98	5.0	16.	9.2	.97	1.7
10 10 83 12	8.4	-.02	.98	4.8	14.	10.0	.97	.0
10 10 83 13	9.1	.02	.98	3.3	14.	11.0	.97	.0
10 10 83 14	9.0	-.13	.98	2.8	32.	7.2	.94	.0
10 10 83 15	5.8	-.08	.97	5.6	31.	7.0	.94	.0
10 10 83 16	6.2	-.10	.98	3.2	31.	6.8	.93	.0
10 10 83 17	5.9	-.02	.98	3.3	30.	4.5	.95	.0
10 10 83 18	4.9	.22	.97	3.5	32.	3.2	.97	.0
10 10 83 19	4.5	.19	.98	2.5	30.	2.8	.98	.0
10 10 83 20	3.9	.33	.98	2.3	31.	2.8	.98	.0
10 10 83 21	3.3	.25	.98	1.0	33.	3.2	.98	.0
10 10 83 22	3.8	.02	.98	.9	29.	3.3	.98	.0
10 10 83 23	3.5	.06	.98	.8	29.	3.2	.98	.0
10 10 83 24	3.3	.19	.98	1.1	27.	3.5	.98	.0
11 10 83 1	3.4	-.01	1.00	1.5	33.	3.9	.98	.0
11 10 83 2	3.4	-.01	1.00	1.9	31.	3.0	.98	.0
11 10 83 3	3.3	-.03	1.00	2.1	32.	3.3	.98	.0
11 10 83 4	2.9	-.04	1.00	2.5	31.	3.0	.98	.0
11 10 83 5	2.5	-.03	1.00	2.4	31.	2.8	.98	.0
11 10 83 6	2.3	-.03	1.00	1.5	30.	2.6	.98	.0
11 10 83 7	2.3	-.05	1.00	1.7	31.	2.7	.98	.0
11 10 83 8	2.4	-.09	1.00	1.7	31.	3.2	.98	.0
11 10 83 9	2.9	-.10	1.00	1.1	31.	4.1	.98	.0
11 10 83 10	4.5	-.05	.98	.6	2015.	5.2	.98	.0
11 10 83 11	5.2	-.21	.98	.9	32.	6.0	.98	.0
11 10 83 12	7.1	-.62	.95	1.1	35.	8.0	.87	.0
11 10 83 13	9.3	-.85	.80	1.4	33.	9.0	.82	.0
11 10 83 14	10.4	-.68	.76	1.0	32.	9.2	.80	.0
11 10 83 15	10.6	-.54	.74	.8	31.	8.6	.86	.0
11 10 83 16	10.4	-.65	.77	.5	34.	6.2	.96	.0
11 10 83 17	6.3	.33	.95	1.0	32.	4.9	.97	.0
11 10 83 18	5.3	.22	.97	1.9	32.	3.9	.98	.0
11 10 83 19	4.7	.14	.99	1.6	32.	3.0	.98	.0
11 10 83 20	4.6	.12	.99	1.7	30.	3.3	.98	.0
11 10 83 21	3.7	.70	.98	1.0	27.	2.9	.98	.0
11 10 83 22	3.2	.09	.98	1.1	23.	3.2	.98	.0
11 10 83 23	3.3	1.02	.98	1.2	23.	2.9	.98	.0
11 10 83 24	3.7	.49	.94	1.7	24.	3.0	.98	.0
12 10 83 1	3.7	.29	.92	.8	25.	3.0	.98	.0
12 10 83 2	4.4	.36	.88	1.5	25.	3.0	.98	.0
12 10 83 3	4.4	.46	.86	1.9	23.	3.1	.98	.0
12 10 83 4	4.3	.33	.88	1.0	26.	2.8	.98	.0
12 10 83 5	3.8	.37	.92	1.4	30.	2.0	.98	.0
12 10 83 6	2.7	.34	.96	3.0	34.	1.3	.98	.0
12 10 83 7	2.9	.05	.98	2.5	35.	3.0	.98	.0
12 10 83 8	3.4	-.11	.98	1.2	3.	4.8	.93	.0
12 10 83 9	5.1	-.13	.93	.7	32.	5.3	.95	.0
12 10 83 10	6.8	-.43	.83	.7	22.	7.3	.80	.0
12 10 83 11	8.9	-.37	.71	.9	1012.	9.0	.75	.0
12 10 83 12	9.4	-.47	.69	1.1	12.	10.2	.72	.0
12 10 83 13	9.5	-.55	.76	2.3	14.	10.5	.72	.0
12 10 83 14	9.2	-.38	.79	2.8	13.	9.2	.80	.0
12 10 83 15	8.7	-.27	.83	2.6	14.	10.2	.79	.0
12 10 83 16	8.1	-.05	.89	1.0	14.	6.8	.95	.0
12 10 83 17	7.5	.32	.81	2.0	1030.	6.3	.92	.0
12 10 83 18	8.3	.23	.56	3.2	30.	5.8	.87	.0
12 10 83 19	7.8	.16	.55	2.0	20.	6.3	.70	.0
12 10 83 20	7.5	.16	.58	2.1	25.	7.1	.75	.0
12 10 83 21	7.4	.14	.56	2.0	25.	7.2	.65	.0
12 10 83 22	6.8	.27	.63	2.1	22.	6.8	.80	.0
12 10 83 23	5.6	.23	.84	1.7	24.	6.0	.97	.0
12 10 83 24	4.7	.31	.98	1.4	4.	5.6	.97	.0

	T-AS	OT-AS	RH-AS	F-AS	D-AS	T-BR	RH-BR	P-BR
13 10 83 1	4.6	.02	.98	1.3	7.	5.6	.98	.0
13 10 83 2	4.6	.01	.97	1.3	4.	5.6	.98	.0
13 10 83 3	4.7	-.01	.98	1.6	1.	5.7	.98	.0
13 10 83 4	4.4	-.01	.98	3.2	35.	5.5	.98	.0
13 10 83 5	4.7	.01	.98	2.3	35.	5.7	.98	.0
13 10 83 6	4.7	-.01	.97	1.4	32.	5.8	.98	.0
13 10 83 7	4.8	-.01	.97	1.2	29.	6.0	.98	.0
13 10 83 8	5.1	-.06	.97	.9	18.	6.3	.97	.0
13 10 83 9	5.6	.00	.98	1.1	14.	7.2	.97	.0
13 10 83 10	6.9	-.03	.98	1.1	13.	9.2	.96	.0
13 10 83 11	9.9	-.11	.96	2.6	20.	12.7	.91	.0
13 10 83 12	12.4	-.27	.91	3.7	19.	12.9	.91	.0
13 10 83 13	12.6	-.17	.92	3.1	19.	13.1	.91	.0
13 10 83 14	12.7	-.14	.92	3.3	19.	13.2	.89	.0
13 10 83 15	13.0	-.17	.89	3.5	19.	13.4	.89	.0
13 10 83 16	12.8	-.14	.91	3.5	18.	12.9	.91	.0
13 10 83 17	12.0	.00	.91	3.7	20.	12.7	.91	.0
13 10 83 18	12.0	.00	.92	4.1	20.	12.4	.98	.0
13 10 83 19	11.8	.01	.99	5.5	21.	12.3	.98	.0
13 10 83 20	11.7	.00	.99	6.0	20.	12.3	.97	.0
13 10 83 21	11.4	.00	.98	7.0	20.	12.2	.97	.0
13 10 83 22	11.0	.01	.97	7.1	20.	11.7	.95	.0
13 10 83 23	10.8	.03	.97	7.9	19.	11.5	.95	.0
13 10 83 24	10.6	.01	.95	7.4	20.	11.8	.94	.0
14 10 83 1	10.9	.04	.96	6.4	20.	12.0	.95	.0
14 10 83 2	11.0	.04	.97	5.5	20.	12.0	.95	.0
14 10 83 3	11.0	.05	.96	6.4	21.	11.6	.95	.0
14 10 83 4	10.5	.01	.95	5.1	23.	10.3	.91	.0
14 10 83 5	9.1	.00	.92	3.7	26.	9.3	.92	.0
14 10 83 6	8.2	.09	.87	4.0	24.	8.5	.90	.0
14 10 83 7	7.9	.10	.88	3.6	23.	8.7	.85	.0
14 10 83 8	8.6	-.06	.85	4.4	23.	9.4	.85	.0
14 10 83 9	9.9	-.19	.81	4.4	23.	11.3	.75	.0
14 10 83 10	11.2	-.31	.74	4.4	24.	12.3	.66	.0
14 10 83 11	11.5	-.32	.68	5.7	23.	13.2	.60	.0
14 10 83 12	12.3	-.39	.60	6.3	23.	13.3	.56	.0
14 10 83 13	11.4	-.11	.61	7.2	24.	11.3	.74	.0
14 10 83 14	11.4	-.39	.66	5.9	23.	12.4	.62	.0
14 10 83 15	11.2	-.17	.64	7.4	24.	11.5	.61	.0
14 10 83 16	10.5	-.07	.65	6.9	24.	10.3	.69	.0
14 10 83 17	9.4	.02	.72	4.2	23.	9.3	.75	.0
14 10 83 18	8.5	.12	.79	3.1	21.	9.1	.81	.0
14 10 83 19	8.1	.18	.82	3.2	22.	8.0	.84	.0
14 10 83 20	7.9	.20	.82	4.0	21.	8.5	.83	.0
14 10 83 21	8.1	.14	.83	5.6	22.	8.5	.83	.0
14 10 83 22	8.2	.16	.83	4.1	22.	8.4	.80	.0
14 10 83 23	8.2	.19	.81	4.0	22.	8.2	.80	.0
14 10 83 24	8.0	.24	.83	2.6	20.	8.2	.81	.0
15 10 83 1	7.7	.29	.82	2.9	20.	6.1	.94	.0
15 10 83 2	7.6	.32	.83	3.3	21.	5.1	.97	.0
15 10 83 3	7.5	.28	.86	2.8	18.	4.6	.98	.0
15 10 83 4	7.4	.27	.89	3.2	20.	5.4	.98	.0
15 10 83 5	7.4	.35	.90	2.9	21.	5.3	.98	.0
15 10 83 6	6.9	.49	.91	3.0	22.	5.2	.97	.0
15 10 83 7	6.8	.47	.93	2.5	19.	7.3	.99	.0
15 10 83 8	8.5	.07	.93	3.6	21.	9.3	.90	.0
15 10 83 9	9.4	-.06	.91	2.2	20.	10.3	.93	.0
15 10 83 10	9.8	-.06	.94	2.3	18.	11.0	.90	.3
15 10 83 11	10.2	-.17	.95	3.5	18.	10.9	.89	.1
15 10 83 12	10.0	-.08	.96	2.8	16.	11.2	.96	.2
15 10 83 13	10.0	.00	.99	4.4	19.	11.2	.90	1.4
15 10 83 14	10.0	-.01	.93	4.6	17.	10.7	.80	.6
15 10 83 15	9.6	.01	.95	5.2	15.	10.4	.95	2.7
15 10 83 16	9.7	.02	.98	6.8	16.	10.8	.84	1.4
15 10 83 17	10.1	.03	.96	6.1	16.	11.4	.92	.1
15 10 83 18	10.6	.02	.95	5.8	17.	11.6	.92	.0
15 10 83 19	10.7	.02	.97	5.6	17.	11.4	.94	.1
15 10 83 20	10.7	.00	.97	5.8	17.	11.3	.95	.1
15 10 83 21	10.5	.00	.96	5.8	17.	11.3	.94	.1
15 10 83 22	10.5	.00	.95	5.3	17.	11.3	.91	.0
15 10 83 23	10.3	.00	.94	5.8	17.	10.7	.96	.0
15 10 83 24	9.7	.00	.98	6.7	15.	10.4	.97	.7

	T-AS	DT-AS	RH-AS	F-AS	D-AS	T-DR	RH-DR	P BR
16 10 83 1	9.6	.00	.98	7.1	16.	10.5	.98	2.3
16 10 83 2	9.7	.00	.99	7.2	17.	10.5	.98	.0
16 10 83 3	9.8	.00	.99	7.2	16.	10.6	.98	.0
16 10 83 4	9.8	.01	.98	7.4	16.	10.7	.97	.0
16 10 83 5	9.8	.01	.98	7.6	17.	10.8	.97	.0
16 10 83 6	9.9	.01	.97	7.9	16.	10.8	.95	.0
16 10 83 7	9.8	.01	.98	8.1	16.	10.8	.96	.0
16 10 83 8	9.9	-.01	.98	8.7	16.	10.9	.97	.0
16 10 83 9	9.8	-.08	.97	9.1	17.	9.4	.95	.0
16 10 83 10	8.5	-.01	.92	7.0	22.	8.5	.90	.1
16 10 83 11	7.8	-.09	.89	3.1	21.	9.3	.88	.0
16 10 83 12	8.9	-.11	.90	4.4	18.	10.4	.90	.0
16 10 83 13	9.1	.03	.91	6.6	20.	10.7	.87	.0
16 10 83 14	10.1	-.01	.90	6.7	19.	11.3	.81	.0
16 10 83 15	10.6	-.04	.85	7.5	19.	11.3	.82	.0
16 10 83 16	8.9	.04	.89	7.5	21.	8.3	.93	.0
16 10 83 17	7.9	.10	.94	4.1	18.	9.4	.85	.0
16 10 83 18	9.2	.13	.89	5.1	19.	10.0	.90	.0
16 10 83 19	9.0	.08	.92	5.3	19.	9.3	.88	.0
16 10 83 20	8.8	.07	.89	5.6	18.	9.8	.91	.0
16 10 83 21	8.3	.08	.95	6.5	20.	9.5	.91	.0
16 10 83 22	8.7	.07	.94	6.6	20.	9.6	.89	.0
16 10 83 23	8.5	.06	.90	5.9	18.	9.4	.87	.0
16 10 83 24	8.9	.05	.90	6.1	17.	9.4	.90	.0
17 10 83 1	8.7	.05	.93	8.4	18.	9.5	.95	.0
17 10 83 2	8.9	.06	.95	6.8	18.	10.1	.85	.0
17 10 83 3	8.6	.13	.89	5.5	21.	9.1	.85	.0
17 10 83 4	7.9	.13	.89	4.1	20.	8.2	.86	.0
17 10 83 5	7.6	.13	.89	2.9	21.	8.1	.90	.0
17 10 83 6	7.1	.24	.92	2.6	21.	7.4	.95	.0
17 10 83 7	7.1	.23	.92	1.3	17.	7.8	.91	.0
17 10 83 8	7.7	.09	.90	3.2	19.	8.6	.90	.0
17 10 83 9	8.0	.01	.90	3.3	19.	8.5	.90	.0
17 10 83 10	8.2	-.08	.87	3.0	20.	9.3	.85	.0
17 10 83 11	10.0	-.53	.78	2.7	21.	10.3	.79	.0
17 10 83 12	9.9	-.27	.75	3.1	21.	10.7	.75	.0
17 10 83 13	10.3	-.30	.75	1.7	20.	10.9	.74	.0
17 10 83 14	10.6	-.21	.74	3.2	25.	11.2	.70	.0
17 10 83 15	10.8	-.16	.64	5.1	28.	10.5	.84	.0
17 10 83 16	9.4	.04	.63	3.5	26.	8.3	.76	.0
17 10 83 17	8.5	.15	.68	2.3	24.	7.2	.85	.0
17 10 83 18	7.8	.37	.70	1.8	20.	6.3	.86	.0
17 10 83 19	7.7	.22	.72	2.2	23.	6.4	.80	.0
17 10 83 20	8.1	.08	.67	4.0	25.	8.0	.71	.0
17 10 83 21	7.6	.06	.70	4.0	23.	7.9	.71	.0
17 10 83 22	7.5	.07	.69	3.7	25.	7.7	.69	.0
17 10 83 23	7.4	.13	.69	3.9	25.	7.5	.70	.0
17 10 83 24	7.8	.10	.67	5.2	25.	8.3	.65	.0
18 10 83 1	7.9	.09	.65	3.1	27.	7.1	.80	.0
18 10 83 2	7.7	.27	.64	1.7	26.	5.7	.85	.0
18 10 83 3	7.7	.30	.64	2.8	30.	5.0	.89	.0
18 10 83 4	8.2	.17	.59	4.6	20.	6.3	.86	.0
18 10 83 5	8.1	.09	.58	4.0	29.	8.2	.59	.0
18 10 83 6	7.0	.27	.63	2.9	32.	7.4	.57	.0
18 10 83 7	6.1	.32	.64	1.7	32.	4.5	.80	.0
18 10 83 8	7.5	.08	.57	2.4	30.	5.3	.75	.0
18 10 83 9	9.4	-.28	.53	2.4	30.	9.0	.55	.0
18 10 83 10	9.9	-.25	.48	3.7	29.	10.2	.48	.0
18 10 83 11	10.1	-.26	.44	3.5	27.	10.7	.46	.0
18 10 83 12	10.7	-.38	.41	2.8	25.	11.3	.42	.0
18 10 83 13	10.6	-.37	.43	3.0	24.	11.6	.45	.0
18 10 83 14	9.7	-.23	.49	3.2	24.	11.9	.46	.0
18 10 83 15	8.5	-.10	.58	3.7	21.	10.3	.54	.0
18 10 83 16	6.9	.06	.78	2.2	17.	8.8	.65	.0
18 10 83 17	6.3	.18	.97	3.0	14.	8.1	.85	.0
18 10 83 18	7.9	.00	.98	5.6	16.	8.6	.96	.0
18 10 83 19	8.6	.00	.99	6.3	17.	9.2	.97	.0
18 10 83 20	9.8	.03	.99	5.1	19.	10.3	.97	.0
18 10 83 21	10.3	.06	.98	4.2	20.	11.2	.97	.0
18 10 83 22	10.4	.06	.96	4.5	19.	11.5	.95	.0
18 10 83 23	10.6	.06	.95	5.3	21.	11.4	.94	.0
18 10 83 24	10.7	.11	.91	6.4	22.	11.6	.92	.0

	T-AS	DT-AS	RH-AS	F-AS	D-AS	T-BR	RH-BR	P-BR
19 10 83 1	10.2	.10	.60	7.0	26.	11.8	.90	.0
19 10 83 2	9.0	.08	.60	5.1	27.	11.3	.61	.0
19 10 83 3	8.0	.13	.66	3.9	25.	10.2	.60	.0
19 10 83 4	7.6	.09	.71	5.6	24.	8.3	.73	.0
19 10 83 5	7.6	.07	.74	6.9	24.	8.4	.72	.0
19 10 83 6	7.5	.06	.78	8.2	24.	8.4	.72	.0
19 10 83 7	7.4	.07	.79	5.4	24.	8.7	.72	.0
19 10 83 8	7.8	.03	.72	5.1	24.	8.5	.77	.0
19 10 83 9	9.1	-.06	.65	6.5	26.	8.6	.71	.0
19 10 83 10	10.2	-.09	.57	9.5	26.	9.3	.66	.0
19 10 83 11	10.7	-.15	.55	9.1	28.	10.3	.50	.0
19 10 83 12	11.8	-.19	.51	8.9	29.	14.3	.54	.0
19 10 83 13	12.2	-.16	.49	9.0	30.	13.0	.49	.0
19 10 83 14	11.8	-.04	.46	9.4	30.	12.5	.46	.1
19 10 83 15	10.9	.02	.44	10.1	30.	11.5	.46	.0
19 10 83 16	10.4	.02	.44	8.5	31.	11.0	.45	.0
19 10 83 17	9.9	.07	.44	8.5	31.	10.7	.45	.0
19 10 83 18	9.2	.06	.44	8.5	31.	10.0	.45	.0
19 10 83 19	8.4	.05	.44	6.9	31.	9.0	.47	.0
19 10 83 20	7.3	.06	.43	8.3	31.	7.6	.47	.0
19 10 83 21	6.3	.09	.44	6.5	30.	6.8	.45	.0
19 10 83 22	5.8	.12	.45	4.3	28.	6.4	.47	.0
19 10 83 23	5.1	.19	.47	2.2	29.	5.4	.54	.0
19 10 83 24	5.4	.14	.48	4.2	28.	5.7	.52	.0
20 10 83 1	5.8	.08	.47	6.1	30.	6.6	.50	.0
20 10 83 2	5.9	.04	.45	6.7	29.	6.5	.47	.0
20 10 83 3	5.9	.05	.45	4.7	30.	6.4	.48	.0
20 10 83 4	5.8	.04	.45	5.1	28.	6.1	.48	.0
20 10 83 5	5.7	.04	.46	4.6	28.	6.2	.49	.0
20 10 83 6	5.5	.06	.46	4.1	29.	6.0	.50	.0
20 10 83 7	5.4	.07	.49	4.5	29.	5.7	.51	.0
20 10 83 8	5.5	.07	.49	4.7	30.	5.9	.50	.0
20 10 83 9	5.9	-.01	.48	4.6	31.	6.6	.49	.0
20 10 83 10	6.6	-.13	.45	3.6	29.	7.0	.48	.0
20 10 83 11	7.2	-.16	.42	3.9	30.	8.0	.43	.0
20 10 83 12	7.7	-.22	.42	3.7	29.	8.2	.44	.0
20 10 83 13	9.4	-.34	.39	3.3	27.	10.0	.42	.0
20 10 83 14	10.2	-.34	.38	4.5	31.	10.3	.42	.0
20 10 83 15	9.8	-.33	.39	5.3	31.	10.2	.41	.0
20 10 83 16	8.0	-.03	.37	7.2	31.	8.1	.40	.0
20 10 83 17	6.6	.08	.42	4.2	30.	6.0	.45	.0
20 10 83 18	5.5	.17	.46	3.0	30.	5.7	.50	.0
20 10 83 19	5.9	.16	.48	4.4	31.	6.0	.50	.0
20 10 83 20	6.1	.12	.47	4.6	30.	6.3	.48	.0
20 10 83 21	6.3	.13	.47	5.3	31.	6.4	.49	.0
20 10 83 22	6.4	.18	.47	4.2	32.	6.9	.49	.0
20 10 83 23	6.5	.22	.47	3.3	33.	7.2	.49	.0
20 10 83 24	6.7	.21	.47	4.5	33.	7.1	.49	.0
21 10 83 1	6.4	.21	.49	4.1	31.	6.9	.51	.0
21 10 83 2	6.1	.23	.50	3.4	30.	7.0	.50	.0
21 10 83 3	6.0	.26	.54	3.3	30.	7.0	.51	.0
21 10 83 4	6.3	.36	.50	3.2	33.	6.3	.55	.0
21 10 83 5	6.6	.30	.48	4.7	33.	7.0	.49	.0
21 10 83 6	6.6	.21	.46	5.1	33.	7.1	.49	.0
21 10 83 7	5.7	.22	.54	3.0	32.	4.0	.62	.0
21 10 83 8	6.2	.14	.52	3.2	32.	6.0	.53	.0
21 10 83 9	7.5	-.14	.49	3.3	31.	7.0	.52	.0
21 10 83 10	9.0	-.37	.44	3.7	32.	8.2	.48	.0
21 10 83 11	9.7	-.54	.42	3.8	32.	9.9	.44	.0
21 10 83 12	9.9	-.44	.39	3.4	32.	10.1	.43	.0
21 10 83 13	11.2	-.61	.34	2.3	31.	10.8	.41	.0
21 10 83 14	12.3	-.87	.26	1.7	33.	11.2	.37	.0
21 10 83 15	11.6	-.41	.26	2.1	30.	12.1	.33	.0
21 10 83 16	10.4	-.21	.26	1.8	32.	9.0	.47	.0
21 10 83 17	7.5	.23	.34	1.7	31.	6.0	.55	.0
21 10 83 18	5.8	.41	.39	1.8	32.	4.7	.56	.0
21 10 83 19	5.0	.54	.43	2.6	32.	3.0	.60	.0
21 10 83 20	4.6	.48	.49	2.7	33.	2.4	.68	.0
21 10 83 21	4.5	.30	.52	2.0	32.	2.2	.77	.0
21 10 83 22	4.8	.26	.53	2.8	32.	2.7	.77	.0
21 10 83 23	5.9	.11	.53	4.0	31.	3.1	.80	.0
21 10 83 24	6.2	.06	.50	3.7	30.	5.7	.58	.0

	T-AS	DT-AS	RH-AS	F-AS	D-AS	T-BR	RH-BR	P-BR
22 10 83 1	5.8	.03	.51	2.3	27.	6.4	.56	.0
22 10 83 2	5.5	.10	.53	2.1	25.	6.0	.58	.0
22 10 83 3	5.7	.08	.53	2.8	26.	5.8	.60	.0
22 10 83 4	6.0	.12	.56	2.2	25.	5.7	.61	.0
22 10 83 5	4.7	.25	.62	1.1	19.	5.6	.65	.0
22 10 83 6	4.9	.56	.63	1.0	14.	5.2	.70	.0
22 10 83 7	4.9	.48	.66	1.2	13.	5.7	.70	.0
22 10 83 8	5.1	.71	.70	1.9	12.	5.4	.75	.0
22 10 83 9	7.1	.51	.65	2.4	31.	4.8	.82	.0
22 10 83 10	9.2	.13	.59	2.5	31.	5.0	.83	.0
22 10 83 11	10.1	.06	.55	4.2	31.	8.0	.60	.0
22 10 83 12	10.2	.06	.56	4.2	32.	10.8	.56	.0
22 10 83 13	10.4	.04	.54	3.9	31.	11.0	.56	.0
22 10 83 14	10.5	.04	.56	3.5	33.	11.1	.55	.0
22 10 83 15	10.4	.11	.56	2.8	30.	11.0	.57	.0
22 10 83 16	10.0	.14	.54	1.5	26.	9.7	.70	.0
22 10 83 17	10.1	.12	.55	3.6	31.	8.4	.67	.0
22 10 83 18	9.4	.16	.57	1.9	27.	9.0	.61	.0
22 10 83 19	9.0	.17	.56	2.0	25.	7.8	.63	.0
22 10 83 20	8.1	.20	.62	2.0	24.	8.7	.63	.0
22 10 83 21	6.6	.27	.68	1.6	23.	7.8	.70	.0
22 10 83 22	6.5	.23	.71	2.5	23.	7.6	.71	.0
22 10 83 23	6.4	.13	.73	3.7	24.	7.0	.74	.0
22 10 83 24	5.7	.16	.76	1.9	24.	7.0	.73	.0
23 10 83 1	5.3	.17	.79	2.8	25.	6.7	.74	.0
23 10 83 2	5.4	.11	.69	3.8	26.	6.5	.73	.0
23 10 83 3	5.3	.13	.75	4.3	25.	6.6	.71	.0
23 10 83 4	6.1	.11	.74	5.0	24.	6.0	.72	.0
23 10 83 5	6.4	.11	.77	4.0	22.	7.0	.73	.0
23 10 83 6	6.7	.04	.82	4.1	22.	7.3	.74	.0
23 10 83 7	7.1	.03	.89	4.8	21.	7.9	.82	.0
23 10 83 8	7.6	.00	.87	5.6	22.	8.1	.84	.0
23 10 83 9	8.1	-.08	.75	4.2	23.	8.5	.82	.0
23 10 83 10	8.6	-.09	.68	4.8	25.	9.0	.70	.0
23 10 83 11	9.4	-.26	.65	4.5	23.	9.8	.65	.0
23 10 83 12	9.8	-.21	.64	5.2	24.	10.3	.62	.0
23 10 83 13	9.3	-.08	.67	4.8	24.	10.9	.62	.0
23 10 83 14	9.3	-.08	.71	5.2	25.	10.2	.66	.0
23 10 83 15	8.9	-.04	.76	5.1	23.	10.1	.69	.0
23 10 83 16	8.6	-.03	.81	5.0	24.	10.0	.71	.0
23 10 83 17	8.3	-.01	.88	5.5	23.	9.8	.76	.0
23 10 83 18	8.1	.01	.92	4.9	22.	9.5	.82	.0
23 10 83 19	8.0	.06	.93	5.1	23.	9.0	.83	.0
23 10 83 20	7.9	.08	.93	4.0	24.	9.0	.90	.0
23 10 83 21	7.5	.14	.85	3.9	24.	8.8	.93	.0
23 10 83 22	7.0	.09	.69	5.4	24.	8.0	.89	.0
23 10 83 23	6.4	.09	.68	5.3	24.	7.9	.68	.0
23 10 83 24	5.7	.11	.70	5.4	25.	7.7	.68	.0
24 10 83 1	5.9	.09	.64	4.5	26.	7.0	.69	.0
24 10 83 2	5.3	.12	.62	4.0	26.	6.2	.65	.0
24 10 83 3	4.6	.14	.62	4.2	26.	5.5	.69	.0
24 10 83 4	4.2	.15	.62	4.0	28.	5.0	.66	.0
24 10 83 5	4.8	.09	.43	7.3	30.	3.2	.73	.0
24 10 83 6	3.8	.09	.41	5.0	30.	5.0	.54	.0
24 10 83 7	3.0	.16	.44	3.5	30.	4.5	.47	.0
24 10 83 8	3.1	.01	.46	2.5	27.	3.2	.50	.0
24 10 83 9	4.1	-.11	.46	4.3	30.	2.0	.57	.0
24 10 83 10	5.1	-.31	.39	5.3	31.	3.8	.52	.0
24 10 83 11	5.6	-.43	.36	5.4	33.	5.2	.42	.0
24 10 83 12	6.2	-.51	.33	4.9	32.	6.1	.39	.0
24 10 83 13	7.3	-.50	.30	4.5	31.	6.9	.38	.0
24 10 83 14	7.8	-.51	.29	4.3	32.	7.2	.36	.0
24 10 83 15	7.1	-.28	.29	5.0	31.	7.9	.35	.0
24 10 83 16	6.0	-.09	.32	4.8	31.	7.9	.35	.0
24 10 83 17	4.4	.09	.37	2.8	27.	6.5	.35	.0
24 10 83 18	3.1	.20	.43	2.1	26.	4.8	.43	.0
24 10 83 19	2.8	.16	.49	1.9	28.	3.7	.54	.0
24 10 83 20	2.3	.17	.54	2.4	28.	3.2	.52	.0
24 10 83 21	2.1	.13	.57	2.5	26.	1.2	.64	.0
24 10 83 22	2.1	.10	.60	2.1	25.	2.6	.61	.0
24 10 83 23	1.1	.18	.64	1.2	1024.	2.4	.62	.0
24 10 83 24	.4	.42	.69	1.4	23.	2.7	.62	.0

	T-AS	DT-AS	RH-AS	F-AS	D-AS	T-BR	RH-BR	P-BR
25 10 83 1	.4	.26	.70	1.4	24.	2.0	.69	.0
25 10 83 2	.2	.37	.74	1.1	19.	-.7	.80	.0
25 10 83 3	-.1	.37	.73	1.4	25.	-1.2	.92	.0
25 10 83 4	.7	.29	.70	1.6	25.	-1.0	.90	.1
25 10 83 5	1.3	.11	.69	1.4	27.	-1.1	.95	.0
25 10 83 6	1.3	.25	.74	1.5	22.	-1.0	.94	.1
25 10 83 7	1.8	.17	.85	2.3	21.	1.0	.73	.0
25 10 83 8	2.0	.11	.93	2.6	22.	3.0	.77	.2
25 10 83 9	3.0	.09	.96	4.5	23.	3.0	.87	.5
25 10 83 10	3.5	.10	.94	4.8	21.	3.4	.95	.5
25 10 83 11	4.2	.06	.89	5.0	21.	4.3	.94	.0
25 10 83 12	4.7	.05	.87	5.0	21.	4.9	.92	.0
25 10 83 13	5.2	.01	.86	5.6	21.	5.8	.85	.1
25 10 83 14	6.0	-.03	.82	5.3	22.	6.0	.85	.0
25 10 83 15	6.0	-.01	.81	5.0	21.	6.7	.82	.0
25 10 83 16	5.9	.00	.82	4.0	20.	7.2	.79	.0
25 10 83 17	6.0	.02	.85	4.0	20.	7.2	.78	.0
25 10 83 18	6.4	.02	.87	3.8	20.	7.0	.80	.0
25 10 83 19	6.9	.06	.91	4.8	21.	7.1	.82	.0
25 10 83 20	7.2	.10	.88	4.5	23.	7.7	.85	.0
25 10 83 21	7.3	.14	.96	3.9	23.	8.0	.89	.0
25 10 83 22	7.3	.16	.98	4.0	22.	8.7	.90	.0
25 10 83 23	7.5	.21	.98	3.4	22.	8.9	.91	.0
25 10 83 24	7.6	.19	.97	2.2	24.	8.9	.93	.0
26 10 83 1	7.0	.49	.98	1.2	21.	9.0	.94	.0
26 10 83 2	6.3	.94	1.00	.7	25.	9.0	.93	.0
26 10 83 3	9.5	.74	.78	3.2	28.	7.3	.98	.0
26 10 83 4	11.7	.55	.65	3.2	27.	6.0	.99	.0
26 10 83 5	12.4	.42	.61	1.8	28.	5.2	.99	.0
26 10 83 6	13.1	.35	.60	2.6	30.	5.0	.99	.0
26 10 83 7	14.1	.35	.55	4.7	29.	5.7	.98	.0
26 10 83 8	15.2	.19	.50	6.9	29.	6.0	.98	.0
26 10 83 9	15.6	.00	.50	5.0	31.	10.0	.60	.0
26 10 83 10	16.8	-.17	.47	3.5	29.	15.2	.50	.0
26 10 83 11	17.3	-.22	.45	5.3	30.	16.0	.50	.0
26 10 83 12	17.7	-.21	.43	6.1	28.	16.9	.42	.0
26 10 83 13	18.6	-.20	.40	6.4	28.	19.7	.38	.0
26 10 83 14	18.5	-.14	.38	8.3	29.	19.3	.38	.0
26 10 83 15	18.1	-.08	.39	7.6	29.	17.5	.42	.0
26 10 83 16	17.2	.03	.41	6.2	29.	16.2	.45	.0
26 10 83 17	15.8	.20	.45	4.5	26.	15.7	.47	.0
26 10 83 18	15.0	.18	.43	5.5	26.	14.2	.52	.0
26 10 83 19	14.1	.18	.51	5.1	26.	13.6	.56	.0
26 10 83 20	13.4	.20	.54	4.7	25.	12.6	.63	.0
26 10 83 21	11.8	.18	.65	3.9	23.	12.7	.66	.0
26 10 83 22	11.4	.23	.67	4.0	23.	11.4	.70	.0
26 10 83 23	10.0	.35	.75	2.9	21.	10.6	.76	.0
26 10 83 24	9.7	.28	.80	3.1	20.	10.2	.78	.0
27 10 83 1	9.6	.17	.81	5.4	23.	10.7	.78	.0
27 10 83 2	9.9	.11	.81	5.0	23.	10.3	.80	.0
27 10 83 3	9.4	.10	.85	5.6	23.	10.2	.81	.0
27 10 83 4	9.2	.14	.86	4.8	21.	9.8	.85	.0
27 10 83 5	9.8	.14	.82	5.3	23.	10.6	.79	.0
27 10 83 6	9.5	.12	.83	4.9	23.	10.4	.78	.0
27 10 83 7	9.3	.14	.83	4.1	22.	10.3	.79	.0
27 10 83 8	9.7	.07	.84	5.1	22.	11.2	.77	.0
27 10 83 9	10.0	.07	.82	5.2	24.	11.5	.76	.0
27 10 83 10	11.3	-.12	.80	4.9	24.	14.0	.56	.0
27 10 83 11	13.1	-.15	.56	5.5	25.	14.1	.44	.0
27 10 83 12	12.4	-.16	.45	6.7	27.	13.2	.43	.0
27 10 83 13	12.5	-.21	.43	5.6	26.	13.3	.44	.0
27 10 83 14	12.3	-.19	.44	5.6	27.	13.1	.42	.0
27 10 83 15	11.9	-.15	.38	5.6	26.	11.7	.43	.0
27 10 83 16	10.5	-.02	.43	5.2	27.	10.7	.45	.0
27 10 83 17	9.4	.06	.48	4.5	25.	10.0	.50	.0
27 10 83 18	8.8	.05	.53	3.6	25.	9.5	.56	.0
27 10 83 19	8.4	.03	.58	4.1	24.	9.1	.61	.0
27 10 83 20	7.9	.05	.63	3.8	25.	8.5	.63	.0
27 10 83 21	7.4	.09	.64	3.9	25.	7.9	.64	.0
27 10 83 22	7.0	.11	.64	3.5	26.	6.3	.69	.0
27 10 83 23	6.4	.12	.66	3.6	26.	5.8	.75	.0
27 10 83 24	5.7	.18	.67	2.6	26.	3.5	.84	.0

			T-AS	D-AS	RH-AS	F-AS	D-AS	T-BR	RH-BR	P-BR	
28	10	83	1	4.4	.27	.70	2.2	28.	2.2	.90	.0
28	10	83	2	4.4	.35	.74	2.4	26.	3.3	.92	.0
28	10	83	3	3.5	.31	.77	1.7	24.	3.2	.81	.0
28	10	83	4	3.6	.30	.75	2.2	20.	1.5	.91	.0
28	10	83	5	3.2	.52	.78	2.4	32.	.7	.96	.0
28	10	83	6	3.3	.59	.81	3.6	32.	1.2	.91	.0
28	10	83	7	3.1	.70	.80	3.3	33.	.6	.94	.0
28	10	83	8	4.2	.29	.69	3.1	35.	3.0	.76	.0
28	10	83	9	6.4	-.12	.64	2.3	33.	5.5	.62	.0
28	10	83	10	7.0	-.61	.64	1.6	32.	7.6	.57	.0
28	10	83	11	8.8	-.67	.53	1.8	34.	9.8	.41	.0
28	10	83	12	8.6	-.60	.47	1.3	31.	9.0	.43	.0
28	10	83	13	7.8	-.31	.47	1.2	10.	9.6	.41	.1
28	10	83	14	5.8	.01	.58	1.5	1002.	6.8	.60	.0
28	10	83	15	6.6	-.21	.58	.9	2.	5.7	.70	.0
28	10	83	16	6.4	-.21	.58	1.2	1020.	3.7	.71	.0
28	10	83	17	4.4	.38	.68	2.2	31.	2.5	.76	.0
28	10	83	18	3.7	.41	.59	3.3	34.	1.2	.76	.0
28	10	83	19	3.1	.30	.52	3.5	34.	2.0	.60	.0
28	10	83	20	2.6	.32	.55	2.8	33.	1.5	.66	.0
28	10	83	21	2.3	.32	.57	3.1	33.	.9	.71	.0
28	10	83	22	1.9	.35	.57	3.0	33.	-1.0	.81	.1
28	10	83	23	1.5	.37	.61	2.7	32.	-1.3	.84	.0
28	10	83	24	1.0	.29	.65	2.4	31.	-1.7	.81	.1
29	10	83	1	.4	.33	.71	3.1	31.	-2.0	.87	.0
29	10	83	2	-.4	.56	.75	3.4	31.	-2.5	.95	99.0
29	10	83	3	-.9	.67	.82	3.2	31.	-2.8	.95	99.0
29	10	83	4	-1.4	.29	.88	2.7	32.	-2.2	.96	99.0
29	10	83	5	-1.5	.70	.85	2.7	31.	-2.7	.96	99.0
29	10	83	6	-1.6	.55	.89	2.0	32.	-2.9	.96	99.0
29	10	83	7	-2.0	.81	.96	1.8	32.	-2.9	.98	99.0
29	10	83	8	-1.9	.58	.97	1.0	26.	-2.7	.97	99.0
29	10	83	9	-.8	.21	.93	1.2	30.	-1.0	.86	99.0
29	10	83	10	1.1	.05	.74	3.1	29.	2.0	.76	99.0
29	10	83	11	3.5	-.20	.57	2.9	26.	5.0	.51	99.0
29	10	83	12	5.2	-.41	.46	4.9	23.	6.9	.47	99.0
29	10	83	13	6.5	-.35	.46	3.7	23.	7.7	.47	99.0
29	10	83	14	5.7	-.02	.52	3.9	23.	6.9	.51	99.0
29	10	83	15	5.7	.03	.54	4.6	24.	7.0	.53	99.0
29	10	83	16	5.3	.05	.60	5.2	33.	6.6	.56	99.0
29	10	83	17	5.1	.02	.65	5.6	24.	6.2	.62	99.0
29	10	83	18	4.8	.06	.71	6.6	23.	6.1	.66	99.0
29	10	83	19	4.9	.06	.73	7.1	23.	6.3	.66	99.0
29	10	83	20	4.0	.06	.75	6.5	22.	6.1	.68	99.0
29	10	83	21	4.8	.05	.77	5.5	23.	6.2	.71	99.0
29	10	83	22	5.0	.05	.79	4.0	25.	6.1	.73	99.0
29	10	83	23	5.8	.04	.71	4.7	25.	6.7	.72	99.0
29	10	83	24	5.8	.06	.78	4.5	22.	7.0	.73	99.0
30	10	83	1	5.8	.04	.79	3.5	23.	7.1	.73	99.0
30	10	83	2	6.2	.05	.79	3.9	24.	8.0	.72	99.0
30	10	83	3	6.8	.05	.78	4.3	25.	8.4	.72	99.0
30	10	83	4	7.3	.02	.77	6.0	23.	8.2	.73	99.0
30	10	83	5	7.0	.03	.78	5.1	24.	8.3	.73	99.0
30	10	83	6	7.1	.04	.79	5.7	22.	8.6	.73	99.0
30	10	83	7	7.3	.03	.79	5.9	22.	8.8	.74	99.0
30	10	83	8	7.5	.04	.80	5.4	23.	9.0	.74	99.0
30	10	83	9	7.6	.01	.81	5.2	22.	9.1	.72	99.0
30	10	83	10	7.9	.00	.79	5.4	23.	9.7	.71	99.0
30	10	83	11	8.3	-.03	.77	5.4	23.	10.0	.66	99.0
30	10	83	12	8.9	-.07	.74	5.8	24.	10.7	.67	99.0
30	10	83	13	9.6	-.13	.72	6.0	24.	11.0	.67	99.0
30	10	83	14	9.8	-.08	.73	7.5	24.	11.0	.69	99.0
30	10	83	15	9.8	-.06	.75	6.2	23.	10.8	.73	99.0
30	10	83	16	9.1	.01	.79	6.5	23.	10.0	.79	99.0
30	10	83	17	8.9	.07	.84	7.3	23.	10.1	.80	99.0
30	10	83	18	9.1	.05	.86	6.2	22.	10.3	.79	99.0
30	10	83	19	9.1	.08	.87	4.6	24.	10.0	.73	99.0
30	10	83	20	9.0	.04	.78	6.6	25.	8.9	.80	99.0
30	10	83	21	8.0	.05	.82	4.7	25.	8.0	.76	99.0
30	10	83	22	7.4	.07	.80	5.8	25.	8.0	.70	99.0
30	10	83	23	7.0	.05	.73	7.3	24.	7.4	.73	99.0
30	10	83	24	6.4	.05	.76	6.4	24.	7.5	.73	99.0

		T-AS	DT-AS	RH-AS	F-AS	D-AS	T-BR	RH-BR	P-BR
31 10 83 1		6.3	.06	.70	7.9	23.	7.1	.75	99.0
31 10 83 2		5.3	.08	.80	5.8	23.	6.0	.76	99.0
31 10 83 3		5.6	.14	.81	4.1	20.	6.0	.81	99.0
31 10 83 4		5.6	.24	.79	2.0	24.	6.0	.66	99.0
31 10 83 5		7.0	.10	.65	5.3	29.	6.5	.76	99.0
31 10 83 6		7.9	.14	.65	3.9	29.	6.2	.66	99.0
31 10 83 7		8.2	.14	.62	3.3	28.	9.5	.56	99.0
31 10 83 8		9.1	.15	.57	5.0	30.	11.0	.51	99.0
31 10 83 9		10.6	-.01	.54	8.1	31.	12.0	.47	99.0
31 10 83 10		11.3	-.11	.51	9.3	32.	13.0	.46	99.0
31 10 83 11		12.2	-.20	.49	8.2	32.	14.1	.44	99.0
31 10 83 12		12.9	-.30	.47	5.7	32.	15.0	.40	99.0
31 10 83 13		13.8	-.22	.40	8.9	32.	14.5	.39	99.0
31 10 83 14		13.6	-.20	.38	8.9	32.	13.9	.38	99.0
31 10 83 15		12.7	-.15	.39	7.1	32.	12.0	.40	99.0
31 10 83 16		11.2	.02	.40	5.7	31.	10.3	.44	99.0
31 10 83 17		9.5	.19	.45	4.1	31.	9.4	.47	99.0
31 10 83 18		8.6	.21	.48	5.0	31.	8.2	.52	99.0
31 10 83 19		7.6	.27	.52	3.8	32.	5.8	.62	99.0
31 10 83 20		7.1	.25	.52	3.4	32.	5.0	.66	99.0
31 10 83 21		6.5	.27	.54	3.0	31.	4.6	.67	99.0
31 10 83 22		6.0	.32	.51	3.1	30.	4.2	.71	99.0
31 10 83 23		5.8	.44	.52	2.6	30.	4.1	.73	99.0
31 10 83 24		5.5	.36	.61	1.6	26.	4.0	.77	99.0
ANT. 99.		0	0	0	0	0	3	4	71
PROSENT 99.		.0	.0	.0	.0	.0	.4	.5	9.5

	T-AS	DT-AS	RH-AS	F-AS	D-AS	T-BR	RH-BR	P-BR
1 11 03 1	5.5	.24	.61	2.0	26.	3.0	.85	99.0
1 11 03 2	4.5	.45	.65	1.4	23.	3.0	.82	99.0
1 11 03 3	5.4	.22	.63	3.5	24.	6.8	.64	99.0
1 11 03 4	5.6	.10	.63	4.1	23.	6.5	.67	99.0
1 11 03 5	5.1	.13	.70	5.1	22.	6.3	.72	99.0
1 11 03 6	5.0	.13	.76	4.6	21.	6.1	.77	99.0
1 11 03 7	5.9	.17	.81	5.3	23.	7.0	.80	99.0
1 11 03 8	7.4	.09	.83	5.4	22.	8.8	.80	99.0
1 11 03 9	8.6	-.03	.84	4.5	22.	10.2	.79	99.0
1 11 03 10	9.5	-.02	.85	3.5	20.	11.0	.79	99.0
1 11 03 11	10.9	.00	.81	3.6	24.	12.7	.73	99.0
1 11 03 12	12.2	.00	.75	3.8	25.	12.9	.73	99.0
1 11 03 13	13.1	-.22	.71	4.8	23.	14.5	.67	99.0
1 11 03 14	14.7	-.19	.65	6.0	27.	16.2	.55	99.0
1 11 03 15	14.6	-.03	.56	10.5	28.	14.0	.50	99.0
1 11 03 16	12.6	.03	.56	7.1	29.	12.4	.52	99.0
1 11 03 17	11.1	.05	.55	6.9	28.	11.5	.51	99.0
1 11 03 18	10.2	.05	.54	7.7	28.	10.9	.53	99.0
1 11 03 19	9.6	.08	.54	6.9	29.	10.0	.51	99.0
1 11 03 20	8.7	.04	.57	7.1	28.	9.1	.56	99.0
1 11 03 21	7.9	.06	.55	6.9	30.	8.5	.52	99.0
1 11 03 22	7.3	.06	.54	6.1	28.	7.2	.55	99.0
1 11 03 23	6.6	.05	.59	5.9	29.	6.8	.61	99.0
1 11 03 24	6.0	.06	.64	5.3	30.	6.3	.66	99.0
2 11 03 1	6.1	.06	.62	6.1	28.	6.4	.63	99.0
2 11 03 2	6.1	.08	.61	7.0	29.	7.0	.57	99.0
2 11 03 3	6.2	.05	.56	7.9	29.	7.0	.55	99.0
2 11 03 4	5.6	.08	.59	4.6	27.	6.6	.58	99.0
2 11 03 5	6.3	.07	.51	6.8	30.	7.0	.55	99.0
2 11 03 6	6.2	.07	.54	7.3	29.	7.0	.54	99.0
2 11 03 7	5.8	.08	.57	6.2	29.	6.1	.58	99.0
2 11 03 8	5.5	.09	.59	4.5	29.	6.2	.58	99.0
2 11 03 9	6.6	.00	.55	6.7	28.	7.5	.51	99.0
2 11 03 10	7.6	-.11	.52	6.9	29.	8.9	.50	.0
2 11 03 11	8.1	-.17	.49	7.9	29.	9.4	.46	.0
2 11 03 12	8.6	-.25	.47	7.9	30.	9.9	.45	.0
2 11 03 13	9.1	-.27	.47	7.7	30.	9.9	.44	.0
2 11 03 14	9.4	-.22	.46	7.5	30.	10.0	.45	.0
2 11 03 15	8.8	-.13	.46	8.1	30.	9.4	.44	.0
2 11 03 16	7.7	.00	.47	5.0	32.	7.7	.46	.0
2 11 03 17	6.5	.17	.49	4.9	31.	7.0	.50	.0
2 11 03 18	5.4	.20	.54	3.4	31.	4.9	.54	.0
2 11 03 19	4.1	.39	.62	2.7	32.	3.9	.57	.0
2 11 03 20	4.1	.43	.61	2.1	31.	2.6	.71	.0
2 11 03 21	3.7	.51	.62	1.5	24.	2.0	.75	.0
2 11 03 22	3.6	.32	.60	1.9	27.	2.0	.71	.0
2 11 03 23	2.5	.43	.73	1.9	32.	1.4	.76	.0
2 11 03 24	2.5	.37	.67	1.2	35.	1.6	.82	.0
3 11 03 1	2.2	.56	.80	1.0	30.	1.9	.84	.0
3 11 03 2	2.2	.36	.87	1.0	33.	2.2	.85	.0
3 11 03 3	2.2	.50	.86	1.1	32.	2.4	.86	.0
3 11 03 4	2.0	.31	.86	2.0	31.	2.7	.86	.0
3 11 03 5	2.0	.21	.89	.6	1033.	2.6	.86	.0
3 11 03 6	2.1	.48	.86	.4	9.	2.6	.88	.0
3 11 03 7	2.5	.36	.87	.9	31.	2.7	.88	.0
3 11 03 8	2.5	.43	.86	1.2	1031.	2.9	.85	.0
3 11 03 9	3.4	.95	.89	1.9	17.	3.5	.88	.0
3 11 03 10	5.6	.31	.89	2.7	21.	7.9	.86	.0
3 11 03 11	7.7	-.07	.88	4.3	19.	8.8	.84	.0
3 11 03 12	8.1	-.11	.90	3.8	20.	8.9	.86	.0
3 11 03 13	7.8	-.07	.95	4.1	20.	8.1	.96	.0
3 11 03 14	7.3	-.01	1.00	4.7	20.	8.0	.98	.1
3 11 03 15	7.6	.00	.98	4.5	20.	8.3	.98	1.5
3 11 03 16	7.8	.00	.98	4.3	20.	8.8	.97	1.3
3 11 03 17	7.8	.01	.98	5.1	20.	8.7	.97	2.0
3 11 03 18	7.9	.00	.98	5.3	20.	8.9	.97	1.8
3 11 03 19	8.0	.00	.98	5.5	21.	8.9	.97	.5
3 11 03 20	8.0	.00	.98	4.0	21.	9.0	.97	.4
3 11 03 21	8.1	.00	.98	3.8	21.	9.0	.97	.1
3 11 03 22	8.1	-.01	.98	2.1	23.	9.0	.97	.1
3 11 03 23	8.1	.00	.98	2.8	22.	9.1	.97	.1
3 11 03 24	8.2	.00	.99	2.8	22.	9.0	.98	.0

			T-AS	DT-AS	RH-AS	F-AS	D-AS	T-DR	RH-DR	P-BR	
4	11	83	1	8.1	.05	.99	1.6	23.	9.0	.98	.0
4	11	83	2	8.1	.06	.98	.7	17.	8.9	.98	.0
4	11	83	3	7.9	.10	.99	.6	1034.	8.3	.98	.0
4	11	83	4	7.8	.12	.99	1.2	31.	9.2	.99	.0
4	11	83	5	7.6	.09	.98	2.1	32.	8.1	.99	.0
4	11	83	6	7.2	.03	.98	2.3	33.	8.0	.99	.0
4	11	83	7	6.6	.00	.99	2.7	33.	7.7	.99	.0
4	11	83	8	6.2	.01	.98	2.5	34.	7.2	.98	.0
4	11	83	9	6.0	-.06	.97	2.7	34.	7.0	.97	.0
4	11	83	10	6.0	-.08	.97	2.6	34.	6.9	.96	.0
4	11	83	11	6.8	-.24	.95	1.6	33.	7.1	.95	.0
4	11	83	12	7.2	-.24	.91	2.4	31.	8.7	.88	.0
4	11	83	13	7.2	-.15	.93	2.7	31.	8.3	.87	.0
4	11	83	14	7.2	-.07	.90	1.8	33.	8.1	.88	.0
4	11	83	15	7.0	.03	.86	2.1	35.	8.0	.87	.0
4	11	83	16	6.5	.13	.85	1.9	35.	7.8	.76	.0
4	11	83	17	5.1	.46	.88	2.8	35.	6.4	.91	.0
4	11	83	18	4.2	.40	.93	1.8	33.	4.0	.97	.0
4	11	83	19	3.9	.33	.98	2.5	32.	3.9	.98	.0
4	11	83	20	4.1	.22	.98	2.4	33.	4.8	.98	.0
4	11	83	21	4.0	.16	.95	2.8	33.	4.9	.93	.0
4	11	83	22	3.6	.21	.94	2.0	32.	4.9	.92	.0
4	11	83	23	2.4	.19	.97	2.5	32.	3.4	.96	.0
4	11	83	24	1.8	.05	.98	1.9	32.	2.7	.99	.0
5	11	83	1	1.4	.25	.98	2.3	34.	2.2	.99	.0
5	11	83	2	1.3	.01	.98	2.2	34.	2.0	.99	.0
5	11	83	3	1.5	.03	.98	1.9	34.	2.0	.99	.0
5	11	83	4	1.0	.35	.98	2.9	31.	1.4	.99	.0
5	11	83	5	.6	.31	.98	3.2	31.	.0	.99	.0
5	11	83	6	.2	.26	.98	2.2	32.	-.5	.99	.0
5	11	83	7	.1	.08	.98	1.8	34.	-.1	.99	.0
5	11	83	8	-.3	.01	.98	.8	31.	.2	.99	.0
5	11	83	9	-.6	.02	.98	.5	26.	.3	.99	.0
5	11	83	10	.3	.70	.98	.3	1020.	.6	.99	.0
5	11	83	11	3.7	.09	.97	2.8	23.	2.9	.99	.0
5	11	83	12	6.6	-.24	.82	3.3	23.	7.9	.76	.0
5	11	83	13	7.8	-.24	.75	4.3	23.	8.8	.72	.0
5	11	83	14	8.7	-.29	.66	4.0	22.	9.0	.66	.0
5	11	83	15	8.3	-.10	.65	3.5	23.	8.9	.65	.0
5	11	83	16	7.5	.09	.70	4.2	22.	7.9	.69	.0
5	11	83	17	7.1	.11	.73	3.8	22.	7.7	.73	.0
5	11	83	18	7.0	.10	.80	4.5	23.	7.3	.77	.0
5	11	83	19	7.6	.07	.80	5.0	24.	8.0	.79	.0
5	11	83	20	7.6	.05	.82	4.7	24.	8.1	.79	.0
5	11	83	21	7.5	.07	.84	5.3	24.	7.8	.83	.0
5	11	83	22	7.6	.09	.83	5.8	23.	7.9	.82	.0
5	11	83	23	7.5	.07	.82	6.5	24.	8.1	.79	.0
5	11	83	24	7.3	.08	.81	7.0	24.	7.9	.80	.0
6	11	83	1	6.9	.10	.81	6.0	23.	7.8	.78	.0
6	11	83	2	6.6	.11	.84	5.6	23.	7.2	.81	.0
6	11	83	3	7.0	.07	.83	6.5	24.	7.4	.82	.0
6	11	83	4	7.2	.08	.83	5.5	24.	7.9	.82	.0
6	11	83	5	7.5	.09	.83	6.0	22.	7.7	.91	.0
6	11	83	6	7.6	.17	.84	4.4	22.	7.9	.82	.0
6	11	83	7	7.9	.15	.83	5.9	23.	8.4	.82	.0
6	11	83	8	8.0	.08	.84	3.2	18.	8.3	.83	.0
6	11	83	9	8.6	.04	.93	1.7	17.	8.5	.84	.0
6	11	83	10	10.0	-.09	.73	3.8	23.	9.9	.79	.0
6	11	83	11	10.9	-.03	.68	4.8	25.	11.0	.71	.0
6	11	83	12	11.1	-.06	.67	5.1	25.	11.3	.67	.0
6	11	83	13	11.1	-.05	.67	4.7	24.	11.4	.65	.0
6	11	83	14	11.0	-.02	.68	5.4	25.	11.3	.66	.0
6	11	83	15	11.1	-.05	.67	5.1	25.	11.2	.67	.0
6	11	83	16	10.3	.04	.70	5.2	25.	10.9	.67	.0
6	11	83	17	9.5	.12	.72	4.0	23.	9.9	.68	.0
6	11	83	18	9.1	.12	.73	3.8	21.	9.7	.71	.0
6	11	83	19	8.5	.13	.75	4.1	21.	8.9	.73	.0
6	11	83	20	7.5	.14	.80	4.5	22.	8.0	.76	.0
6	11	83	21	7.1	.14	.85	4.8	22.	7.8	.73	.0
6	11	83	22	6.9	.08	.88	5.0	22.	7.5	.83	.0
6	11	83	23	6.7	.08	.88	4.7	23.	7.1	.84	.0
6	11	83	24	6.7	.09	.88	4.7	24.	6.9	.85	.0

			T-AS	DT-AS	RH-AS	F-AS	D-AS	T-BR	RH-BR	P-BR	
7	11	83	1	6.5	.10	.89	3.4	22.	6.4	.87	.0
7	11	83	2	6.5	.25	.88	4.1	22.	5.1	.96	.0
7	11	83	3	6.5	.24	.87	3.0	23.	4.6	.97	.0
7	11	83	4	6.4	.30	.83	3.4	21.	4.8	.95	.0
7	11	83	5	6.2	.26	.83	4.3	23.	4.9	.91	.0
7	11	83	6	5.8	.30	.86	4.0	23.	5.8	.86	.0
7	11	83	7	5.5	.39	.90	3.7	22.	5.2	.89	.0
7	11	83	8	6.0	.22	.90	4.2	23.	5.9	.88	.0
7	11	83	9	6.0	.10	.87	4.1	22.	6.9	.83	.0
7	11	83	10	8.0	.01	.81	4.4	22.	7.6	.90	.0
7	11	83	11	8.9	-.07	.78	4.2	21.	8.7	.76	.0
7	11	83	12	9.5	-.09	.73	3.3	23.	9.3	.73	.0
7	11	83	13	9.8	-.07	.76	3.0	21.	9.6	.73	.0
7	11	83	14	10.0	-.11	.76	2.5	20 10.	9.8	.74	.0
7	11	83	15	9.7	-.09	.78	4.0	21.	9.6	.76	.0
7	11	83	16	9.4	-.04	.79	2.9	21.	9.5	.76	.0
7	11	83	17	9.3	-.02	.81	1.9	20.	9.0	.78	.0
7	11	83	18	9.3	-.03	.83	2.6	20.	8.9	.82	.0
7	11	83	19	9.3	-.02	.83	2.9	21.	9.1	.82	.0
7	11	83	20	9.6	-.04	.81	2.9	22.	9.0	.83	.0
7	11	83	21	9.1	-.05	.86	2.1	19.	8.9	.86	.0
7	11	83	22	9.0	-.05	.93	3.3	21.	8.9	.92	.0
7	11	83	23	8.9	-.06	.94	2.4	21.	8.9	.93	.0
7	11	83	24	8.7	-.06	.97	2.3	21.	8.8	.94	.0
8	11	83	1	8.7	-.07	.97	3.1	21.	8.7	.94	.0
8	11	83	2	8.6	-.07	.97	2.8	21.	8.7	.95	.0
8	11	83	3	8.4	-.05	.96	2.5	21.	8.5	.94	.0
8	11	83	4	8.3	-.08	.96	2.0	19.	8.4	.94	.0
8	11	83	5	8.1	-.08	.96	2.4	19.	8.3	.94	.0
8	11	83	6	8.0	-.07	.97	1.6	19.	8.2	.94	.0
8	11	83	7	8.0	-.08	.98	1.8	19.	8.1	.95	.0
8	11	83	8	7.8	-.08	.98	1.7	20.	8.0	.95	.0
8	11	83	9	7.9	-.09	.96	1.6	21.	8.0	.94	.0
8	11	83	10	8.1	-.12	.92	1.8	20.	8.0	.92	.0
8	11	83	11	8.3	-.17	.91	1.4	20.	8.0	.92	.0
8	11	83	12	8.3	-.18	.91	1.6	20.	8.1	.91	.0
8	11	83	13	8.3	-.10	.89	1.9	21.	8.0	.90	.0
8	11	83	14	8.1	-.14	.88	2.4	22.	8.0	.89	.0
8	11	83	15	8.0	-.12	.88	2.6	21.	7.9	.88	.0
8	11	83	16	7.7	-.08	.89	2.5	20.	7.9	.87	.0
8	11	83	17	6.8	.12	.92	1.6	19.	7.6	.88	.0
8	11	83	18	6.1	.23	.97	1.6	17.	6.2	.95	.0
8	11	83	19	5.6	.50	.99	1.8	21.	5.5	1.01	.0
8	11	83	20	5.4	.53	.99	1.8	22.	5.1	1.01	.0
8	11	83	21	5.8	.39	.97	1.6	22.	4.8	1.02	.0
8	11	83	22	5.8	.32	.96	1.0	25.	4.6	1.02	.0
8	11	83	23	6.3	.24	.96	1.8	26.	4.9	1.00	.0
8	11	83	24	7.1	.19	.92	2.1	26.	5.2	1.00	.0
9	11	83	1	7.1	.24	.95	1.7	22.	4.6	1.01	.0
9	11	83	2	6.8	.24	.98	1.8	21.	4.7	1.02	.0
9	11	83	3	6.2	.30	.99	.7	10 22.	4.9	1.02	.0
9	11	83	4	4.9	1.31	1.00	1.3	34.	4.8	1.02	.0
9	11	83	5	4.5	1.12	1.00	1.7	34.	4.6	1.02	.0
9	11	83	6	4.4	.95	.99	2.0	35.	3.5	1.02	.0
9	11	83	7	4.7	.23	.98	2.1	34.	4.0	1.02	.0
9	11	83	8	4.6	.11	.99	1.7	33.	4.3	1.02	.0
9	11	83	9	5.5	.33	.97	1.7	1.	4.7	1.01	.0
9	11	83	10	7.1	.06	.90	3.1	3.	4.8	99.00	.0
9	11	83	11	7.0	-.18	.78	3.6	4.	6.4	99.00	.0
9	11	83	12	7.9	-.17	.71	2.6	4.	7.1	99.00	.0
9	11	83	13	7.6	-.19	.74	2.8	3.	7.4	99.00	.0
9	11	83	14	7.3	-.16	.75	2.4	5.	99.0	99.00	.0
9	11	83	15	6.8	-.13	.72	2.4	2.	99.0	99.00	.0
9	11	83	16	6.5	-.09	.76	2.3	3.	8.6	.71	.0
9	11	83	17	6.1	-.10	.76	2.0	4.	8.4	.72	.0
9	11	83	18	5.9	-.08	.77	2.6	5.	8.0	.76	.0
9	11	83	19	5.7	-.06	.77	1.0	7.	7.4	.81	.0
9	11	83	20	5.6	-.06	.79	.4	6.	7.5	.80	.0
9	11	83	21	5.6	.03	.80	.6	14.	7.4	.81	.0
9	11	83	22	5.5	-.05	.82	1.2	22.	7.4	.81	.0
9	11	83	23	5.0	.06	.86	.9	19.	7.3	.81	.0
9	11	83	24	5.1	.05	.85	.7	19.	6.8	.86	.0

	T-AS	DT-AS	RH-AS	F-AS	D-AS	T BR	RH-BR	P-BR
10 11 83 1	5.2	.02	.87	1.1	11.	7.0	.88	.0
10 11 83 2	5.2	.10	.87	.9	13.	7.2	.89	.0
10 11 83 3	5.2	.09	.88	.7	12.	7.3	.88	.0
10 11 83 4	5.0	.05	.90	.3	9.	7.2	.89	.0
10 11 83 5	5.1	.05	.89	.6	5.	7.1	.89	.0
10 11 83 6	5.1	-.04	.88	1.1	4.	7.1	.87	.0
10 11 83 7	5.0	-.11	.91	1.8	5.	7.2	.87	.0
10 11 83 8	4.7	-.12	.92	1.1	4.	7.1	.87	.0
10 11 83 9	4.5	-.15	.90	1.3	2.	6.8	.87	.0
10 11 83 10	4.9	-.21	.85	.6	1003.	6.7	.82	.0
10 11 83 11	5.4	-.27	.83	.5	1008.	6.6	.81	.0
10 11 83 12	5.8	-.37	.81	1.1	1.	7.4	.80	.0
10 11 83 13	7.3	-.66	.73	1.2	1.	7.5	.76	.0
10 11 83 14	7.7	-.59	.70	1.5	33.	8.1	.74	.0
10 11 83 15	8.5	-.33	.74	1.5	31.	8.4	.71	.0
10 11 83 16	4.3	.07	.84	1.8	33.	5.6	.85	.0
10 11 83 17	2.8	.25	.88	1.8	32.	3.6	.96	.0
10 11 83 18	2.2	.33	.94	2.6	35.	3.4	.97	.0
10 11 83 19	1.6	.35	.97	2.7	35.	2.6	.97	.0
10 11 83 20	1.2	.29	.98	3.4	35.	3.0	.97	.0
10 11 83 21	.6	.27	.98	3.1	33.	2.4	.97	.0
10 11 83 22	.4	.15	.98	3.4	31.	1.7	.98	.0
10 11 83 23	.0	.32	.95	3.5	33.	.9	.98	.0
10 11 83 24	-.1	.28	.95	3.5	32.	.4	.98	.0
11 11 83 1	-.4	.40	.92	3.1	34.	-.2	.98	.0
11 11 83 2	-.6	.43	.90	2.7	32.	.3	.98	.0
11 11 83 3	-.2	.58	.89	2.8	32.	2.1	.78	.0
11 11 83 4	.3	.45	.76	3.2	1.	1.6	.82	.0
11 11 83 5	.7	.22	.63	2.6	1.	2.2	.69	.0
11 11 83 6	.4	.23	.55	1.6	36.	1.7	.66	.0
11 11 83 7	-.1	.27	.60	2.8	2.	-.6	.82	.0
11 11 83 8	-.2	.27	.59	2.8	2.	-.9	.84	.0
11 11 83 9	1.1	-.04	.58	2.4	2.	.3	.71	.0
11 11 83 10	2.5	-.25	.54	1.9	1.	2.4	.61	.0
11 11 83 11	2.8	-.51	.56	1.8	3.	4.4	.53	.0
11 11 83 12	3.0	-.52	.47	1.6	2.	5.0	.49	.0
11 11 83 13	3.9	-.59	.42	1.5	36.	5.3	.45	.0
11 11 83 14	3.6	-.56	.41	1.0	34.	4.4	.47	.0
11 11 83 15	2.0	-.13	.47	1.0	26.	2.9	.57	.0
11 11 83 16	.9	.11	.52	1.2	23.	1.4	.67	.0
11 11 83 17	.1	.50	.60	1.5	22.	.6	.72	.0
11 11 83 18	-.1	.37	.62	1.1	23.	.4	.77	.0
11 11 83 19	-.5	.41	.68	1.2	21.	.3	.81	.0
11 11 83 20	-.7	.41	.70	.7	15.	.2	.84	.0
11 11 83 21	-1.2	.24	.75	.6	1031.	-.3	.87	.0
11 11 83 22	-1.6	.38	.87	1.5	32.	-1.0	.89	.0
11 11 83 23	-1.9	.43	.84	1.9	34.	-1.5	.94	.0
11 11 83 24	-2.2	.32	.88	1.5	32.	-1.7	.95	.0
12 11 83 1	-2.3	.20	.93	1.9	32.	-1.6	.94	.0
12 11 83 2	-2.4	.21	.93	1.6	33.	-1.6	.96	.0
12 11 83 3	-2.3	.13	.95	2.4	32.	-1.6	.97	.0
12 11 83 4	-2.2	.08	.92	2.0	35.	-1.5	.97	.0
12 11 83 5	-2.2	.01	.90	1.7	34.	-1.4	.98	.0
12 11 83 6	-2.1	.10	.90	2.4	35.	-.9	.96	.0
12 11 83 7	-2.0	.15	.92	2.1	34.	-.8	.94	.0
12 11 83 8	-2.2	.41	.91	2.5	34.	-.7	.94	.0
12 11 83 9	-1.7	.04	.91	2.6	32.	-.7	.93	.0
12 11 83 10	-1.2	-.10	.87	2.2	35.	.1	.92	.0
12 11 83 11	-.2	-.05	.78	3.0	3.	.7	.83	.0
12 11 83 12	.8	-.12	.63	2.3	2.	1.6	.71	.0
12 11 83 13	1.1	-.13	.60	2.0	0.	2.7	.62	.0
12 11 83 14	1.1	-.10	.53	2.2	3.	3.0	.59	.0
12 11 83 15	1.0	-.05	.54	1.5	5.	3.0	.57	.0
12 11 83 16	.9	.00	.56	2.4	5.	2.4	.60	.0
12 11 83 17	.3	.05	.63	3.2	5.	2.5	.61	.0
12 11 83 18	-.2	.04	.70	2.6	6.	2.1	.66	.0
12 11 83 19	-.2	.01	.74	2.6	3.	1.9	.72	.0
12 11 83 20	.2	-.01	.76	3.3	5.	2.1	.74	.0
12 11 83 21	.2	-.03	.80	2.3	5.	2.4	.75	.0
12 11 83 22	-.1	-.08	.89	2.0	5.	2.2	.87	.0
12 11 83 23	-.1	-.07	.93	1.9	8.	1.9	.92	.0
12 11 83 24	.3	-.05	.97	2.0	6.	1.6	.96	.0

	T-AS	DT-AS	RH-AS	F-AS	D-AS	T-BR	RH-BR	F-BR
13 11 83 1	-.3	-.04	.96	2.1	9.	1.6	.96	.0
13 11 83 2	-.2	-.02	.92	2.2	10.	1.7	.94	.0
13 11 83 3	-.2	-.03	.88	2.0	10.	1.9	.90	.0
13 11 83 4	-.2	-.04	.87	2.5	10.	1.8	.89	.0
13 11 83 5	-.2	-.04	.87	1.7	10.	2.0	.86	.0
13 11 83 6	-.4	-.06	.88	1.3	10.	1.9	.91	.0
13 11 83 7	-.4	-.03	.86	1.6	12.	1.4	.93	.0
13 11 83 8	-.5	-.01	.90	.8	26.	1.3	.94	.0
13 11 83 9	-.5	-.09	.88	.8	27.	1.3	.95	.0
13 11 83 10	-.3	-.08	.90	1.3	27.	1.3	.96	.0
13 11 83 11	.1	-.17	.88	.6	26.	1.4	.95	.0
13 11 83 12	.3	-.15	.90	.7	26.	1.8	.94	.0
13 11 83 13	.6	-.21	.87	.7	23.	2.3	.93	.0
13 11 83 14	.8	-.19	.84	1.5	24.	2.4	.86	.0
13 11 83 15	1.1	-.26	.80	1.0	25.	2.8	.81	.0
13 11 83 16	.1	-.01	.83	1.4	25.	1.4	.91	.0
13 11 83 17	-.5	-.07	.86	1.3	27.	.2	.95	.0
13 11 83 18	-.4	-.03	.90	1.1	30.	-.5	.97	.0
13 11 83 19	-.7	-.03	.96	1.8	33.	.0	.97	.0
13 11 83 20	-.7	-.01	.97	2.4	31.	.7	.97	.0
13 11 83 21	-.6	-.02	.96	3.1	31.	.4	.98	.0
13 11 83 22	-.6	-.11	.94	3.1	31.	.3	.98	.0
13 11 83 23	-.9	-.20	.94	3.1	32.	-.5	.98	.0
13 11 83 24	-.9	-.14	.88	3.9	32.	-.6	.98	.0
14 11 83 1	-1.1	.16	.95	3.2	32.	-.9	.98	.0
14 11 83 2	-1.3	.25	.95	3.0	32.	-1.4	.98	.0
14 11 83 3	-1.5	.35	.91	3.0	31.	-1.6	.98	.0
14 11 83 4	-1.6	.40	.92	3.3	32.	-1.3	.98	.0
14 11 83 5	-1.4	.37	.89	3.9	32.	-1.5	.97	.0
14 11 83 6	-1.6	.45	.88	3.4	32.	-1.9	.97	.0
14 11 83 7	-1.6	.46	.89	3.4	32.	-2.1	.97	.0
14 11 83 8	-1.9	.66	.92	3.4	32.	-1.8	.97	.0
14 11 83 9	-1.3	.51	.89	3.3	32.	-.1	.96	.0
14 11 83 10	.1	.15	.99	2.9	33.	.9	.86	.0
14 11 83 11	1.4	-.23	.78	2.1	32.	2.7	.76	.0
14 11 83 12	2.4	-.01	.69	1.6	30.	4.1	.74	.0
14 11 83 13	5.3	-.48	.58	.7	26.	4.3	.74	.0
14 11 83 14	3.6	.84	.68	.7	25.	3.5	.83	.0
14 11 83 15	3.3	1.58	.73	2.8	24.	3.0	.88	.0
14 11 83 16	4.9	.49	.65	1.8	24.	2.6	.90	.0
14 11 83 17	6.0	.39	.63	2.8	29.	2.9	.92	.0
14 11 83 18	6.3	.28	.63	1.2	30.	3.5	.93	.0
14 11 83 19	7.0	.31	.60	2.3	28.	4.1	.91	.0
14 11 83 20	7.5	.13	.60	2.9	27.	5.4	.86	.0
14 11 83 21	7.2	.25	.63	3.8	30.	6.9	.76	.0
14 11 83 22	5.9	.43	.69	2.0	33.	4.4	.87	.0
14 11 83 23	5.2	.55	.70	2.3	36.	2.6	.81	.0
14 11 83 24	4.9	.46	.56	2.5	0.	5.8	.61	.0
15 11 83 1	5.2	.29	.48	2.0	35.	4.6	.61	.0
15 11 83 2	3.9	.51	.59	3.4	32.	1.9	.80	.0
15 11 83 3	2.7	1.40	.71	3.2	31.	1.4	.86	.0
15 11 83 4	2.3	1.04	.70	3.3	31.	.4	.92	.0
15 11 83 5	1.9	.72	.67	3.0	31.	.5	.86	.0
15 11 83 6	.4	.96	.81	2.7	32.	1.1	.81	.0
15 11 83 7	.1	.94	.80	3.4	32.	.6	.88	.0
15 11 83 8	-1.0	.85	.92	2.6	34.	-.5	.96	.0
15 11 83 9	-.1	.33	.74	2.7	33.	.4	.91	.0
15 11 83 10	3.3	-.09	.73	2.0	33.	3.4	.67	.0
15 11 83 11	5.1	-.07	.54	2.5	32.	5.4	.61	.0
15 11 83 12	5.3	.06	.52	3.3	32.	6.5	.60	.0
15 11 83 13	6.2	-.17	.50	2.4	34.	7.1	.51	.0
15 11 83 14	7.2	-.32	.49	3.1	32.	8.4	.48	.0
15 11 83 15	6.8	-.11	.47	2.7	33.	6.4	.61	.0
15 11 83 16	5.3	.15	.54	3.0	31.	4.4	.61	.0
15 11 83 17	3.8	.40	.60	2.6	32.	4.4	.66	.0
15 11 83 18	2.8	1.84	.65	3.4	32.	1.9	.80	.0
15 11 83 19	3.0	.73	.63	3.1	32.	1.4	.81	.0
15 11 83 20	3.5	.48	.54	3.1	32.	.6	.87	.0
15 11 83 21	2.0	.78	.65	3.2	32.	.7	.81	.0
15 11 83 22	1.0	1.13	.73	3.4	33.	.5	.85	.0
15 11 83 23	.1	1.86	.80	2.4	33.	.2	.89	.0
15 11 83 24	-.4	.72	.87	2.7	31.	.6	.91	.0

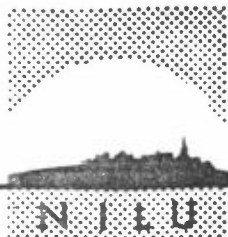
	T-AS	DT-AS	RH-AS	F-AS	D AS	T-BR	RH-BR	P-BR
16 11 83 1	-1.5	1.21	.90	2.3	32.	.2	.90	.0
16 11 83 2	-1.8	1.47	.91	1.8	33.	-.1	.94	.0
16 11 83 3	-1.0	.73	.97	2.1	32.	-.6	.95	.0
16 11 83 4	-2.4	.50	.94	2.5	34.	.1	.94	.0
16 11 83 5	-2.4	.50	.93	2.6	33.	-.4	.91	.0
16 11 83 6	-2.4	.37	.91	3.1	33.	-.5	.95	.0
16 11 83 7	-2.7	.32	.90	2.6	33.	-.6	.96	.0
16 11 83 8	-2.4	.29	.89	3.2	34.	-.8	.91	.0
16 11 83 9	-2.0	.03	.92	3.2	32.	.2	.91	.0
16 11 83 10	-1.6	-.11	.91	2.0	32.	.4	.87	.0
16 11 83 11	-.7	-.22	.87	2.4	32.	1.3	.86	.0
16 11 83 12	1.0	-.53	.75	1.4	34.	2.9	.76	.0
16 11 83 13	2.4	-.44	.68	2.4	32.	3.4	.70	.0
16 11 83 14	2.2	-.19	.67	2.1	1.	99.0	.68	.0
16 11 83 15	2.4	-.08	.63	2.4	33.	99.0	.76	.0
16 11 83 16	.3	.30	.72	2.0	33.	99.0	.81	.0
16 11 83 17	-.4	.45	.74	2.1	33.	99.0	.90	.0
16 11 83 18	-1.5	.51	.89	2.2	33.	99.0	.92	.0
16 11 83 19	-1.9	.50	.90	2.2	33.	99.0	.94	.0
16 11 83 20	-2.2	.48	.95	2.2	33.	99.0	.96	.0
16 11 83 21	-2.5	.34	.96	2.4	33.	99.0	.97	.0
16 11 83 22	-2.7	.36	.93	2.4	33.	99.0	.98	.0
16 11 83 23	-3.0	.27	.96	2.4	33.	99.0	.98	.0
16 11 83 24	-3.4	.33	.93	2.3	34.	99.0	.99	.0
17 11 83 1	-3.4	.33	.92	2.4	34.	99.0	.98	.0
17 11 83 2	-3.7	.34	.96	2.3	33.	99.0	.98	.0
17 11 83 3	-3.8	.32	.96	2.0	34.	99.0	.99	.0
17 11 83 4	-4.1	.40	.95	2.8	34.	99.0	.98	.0
17 11 83 5	-4.2	.26	.96	3.0	33.	99.0	.99	.0
17 11 83 6	-4.4	.26	.96	2.1	33.	99.0	.99	.0
17 11 83 7	-4.5	.24	.96	2.2	33.	99.0	.99	.0
17 11 83 8	-4.6	.23	.96	2.4	33.	99.0	.99	.0
17 11 83 9	-4.2	.04	.96	2.4	33.	99.0	.99	.0
17 11 83 10	-3.5	-.09	.96	1.8	32.	99.0	.99	.0
17 11 83 11	-2.6	-.31	.96	2.0	33.	99.0	.92	.0
17 11 83 12	-1.6	-.51	.90	1.5	33.	-1.5	.89	.0
17 11 83 13	.1	-.56	.82	.8	33.	-.4	.85	.0
17 11 83 14	1.3	-.71	.73	.5	32.	-.3	.83	.0
17 11 83 15	.5	-.32	.75	.6	4.	-.3	.83	.0
17 11 83 16	-1.5	.34	.85	.7	0.	-1.3	.87	.0
17 11 83 17	-1.8	.39	.84	1.3	34.	-2.1	.91	.0
17 11 83 18	-2.1	.34	.88	2.6	34.	-2.5	.93	.0
17 11 83 19	-2.5	.25	.92	2.2	33.	-2.5	.93	.0
17 11 83 20	-3.0	.23	.95	2.2	33.	-2.8	.94	.0
17 11 83 21	-3.3	.23	.95	2.4	34.	-3.3	.96	.0
17 11 83 22	-3.0	.27	.93	2.7	33.	-3.3	.96	.0
17 11 83 23	-2.7	.25	.91	3.7	33.	-3.2	.94	.0
17 11 83 24	-3.1	.32	.92	3.2	34.	-2.7	.92	.0
18 11 83 1	-3.2	.39	.91	2.9	34.	-3.0	.93	.0
18 11 83 2	-3.3	.60	.92	2.6	33.	-3.0	.93	.0
18 11 83 3	-3.0	.87	.91	3.4	34.	-3.2	.93	.0
18 11 83 4	-3.2	.48	.94	3.0	33.	-2.4	.92	.0
18 11 83 5	-3.3	.54	.95	3.7	33.	-2.6	.94	.0
18 11 83 6	-2.5	.45	.93	3.0	34.	-2.5	.94	.0
18 11 83 7	-2.4	.67	.95	3.4	33.	-1.5	.91	.0
18 11 83 8	-2.5	.43	.97	3.5	32.	-1.6	.92	.0
18 11 83 9	-1.8	.62	.95	3.7	33.	-1.6	.94	.0
18 11 83 10	.3	1.30	.85	3.9	32.	-1.3	.92	.0
19 11 83 11	1.8	1.12	.78	3.8	32.	.5	.81	.0
18 11 83 12	3.5	-.04	.68	2.9	32.	3.2	.68	.0
18 11 83 13	6.3	-.34	.58	2.4	31.	4.4	.64	.0
18 11 83 14	6.8	-.16	.54	2.6	31.	3.8	.69	.0
18 11 83 15	6.1	.03	.54	1.8	33.	3.6	.72	.0
18 11 83 16	4.3	.51	.55	1.5	31.	1.6	.80	.0
18 11 83 17	2.2	1.18	.67	.3	29.	.3	.87	.0
18 11 83 18	.0	1.52	.88	.4	0.	-1.3	.93	.0
18 11 83 19	-.4	1.81	.96	2.0	34.	-1.5	.95	.0
18 11 83 20	-.9	1.22	.95	2.4	34.	-2.3	.97	.0
18 11 83 21	-1.6	.97	.98	2.8	33.	-2.4	.97	.0
18 11 83 22	-1.8	.57	.98	2.2	33.	-1.3	.96	.0
18 11 83 23	-2.2	.62	.98	1.9	34.	-1.6	.96	.0
18 11 83 24	-2.2	.60	.98	2.4	32.	-2.5	.97	.0

	T-AS	DT-AS	RH-AS	F-AS	D-AS	T-BR	RH-BR	P-BR
19 11 83 1	-2.6	.22	.98	2.3	32.	-2.4	.97	.0
19 11 83 2	-3.1	.55	.98	1.9	32.	-2.1	.97	.0
19 11 83 3	-3.2	.20	.98	2.3	32.	-2.7	.97	.0
19 11 83 4	-3.6	.43	.96	2.7	32.	-2.7	.97	.0
19 11 83 5	-3.6	.31	.96	2.4	34.	-2.9	.97	.0
19 11 83 6	-3.3	.13	.96	2.6	31.	-2.8	.96	.0
19 11 83 7	-2.9	.48	.97	1.7	31.	-2.7	.96	.0
19 11 83 8	-2.7	.33	.97	.8	1036.	-2.5	.96	.0
19 11 83 9	-2.4	.97	.97	1.1	1022.	-2.4	.96	.0
19 11 83 10	-1.4	1.35	.98	2.0	20.	-2.3	.96	.0
19 11 83 11	.4	.45	.93	3.4	20.	-1.6	.96	.0
19 11 83 12	2.3	.21	.86	3.4	23.	1.7	.85	.0
19 11 83 13	4.2	.01	.80	5.3	23.	3.7	.88	.0
19 11 83 14	5.0	-.01	.79	5.2	21.	4.9	.98	.0
19 11 83 15	5.7	.04	.77	7.4	24.	5.7	.75	.0
19 11 83 16	5.9	.04	.78	7.1	23.	6.5	.73	.0
19 11 83 17	6.2	.06	.77	6.1	23.	6.7	.74	.0
19 11 83 18	6.6	.14	.73	5.9	24.	6.8	.73	.0
19 11 83 19	7.2	.06	.65	6.4	25.	6.7	.68	.0
19 11 83 20	7.1	.06	.63	6.6	24.	7.4	.64	.0
19 11 83 21	7.2	.10	.62	6.2	24.	7.3	.61	.0
19 11 83 22	7.5	.07	.61	5.3	25.	7.2	.63	.0
19 11 83 23	7.3	.04	.54	4.2	26.	7.6	.57	.0
19 11 83 24	6.9	.02	.58	6.8	29.	6.8	.58	.0
20 11 83 1	4.5	-.01	.68	8.2	29.	6.5	.60	.0
20 11 83 2	3.8	-.02	.64	8.3	29.	4.0	.65	.0
20 11 83 3	3.6	.02	.61	6.1	28.	3.7	.61	.0
20 11 83 4	3.9	.03	.54	4.1	28.	3.2	.61	.0
20 11 83 5	3.8	.03	.62	3.7	27.	2.9	.64	.0
20 11 83 6	4.0	.06	.63	4.9	27.	2.9	.68	.0
20 11 83 7	4.9	.01	.56	5.8	20.	3.7	.60	.0
20 11 83 8	4.8	.07	.54	4.4	29.	4.5	.56	.0
20 11 83 9	5.6	.00	.51	7.0	30.	4.6	.53	.0
20 11 83 10	6.3	-.10	.50	9.0	31.	5.7	.50	.0
20 11 83 11	6.5	-.16	.47	9.2	32.	6.4	.48	.0
20 11 83 12	6.8	-.20	.42	8.8	32.	6.8	.44	.0
20 11 83 13	7.1	-.21	.36	8.6	32.	6.8	.42	.0
20 11 83 14	6.8	-.16	.27	7.2	33.	6.7	.38	.0
20 11 83 15	5.6	-.05	.29	7.5	33.	6.7	.34	.0
20 11 83 16	4.4	.08	.34	5.4	31.	5.5	.35	.0
20 11 83 17	3.5	.11	.41	4.3	32.	4.4	.38	.0
20 11 83 18	3.0	.11	.47	4.2	31.	1.7	.51	.0
20 11 83 19	2.7	.15	.47	4.1	32.	.9	.56	.0
20 11 83 20	2.5	.06	.44	5.5	31.	-.6	.68	.0
20 11 83 21	2.1	.05	.43	5.4	31.	2.4	.50	.0
20 11 83 22	1.5	.05	.44	5.0	31.	1.7	.49	.0
20 11 83 23	1.2	.03	.43	5.7	32.	.6	.48	.0
20 11 83 24	.8	.05	.44	5.0	32.	.8	.48	.0
21 11 83 1	.3	.08	.45	4.6	33.	.0	.51	.0
21 11 83 2	-.4	.02	.51	3.6	1.	-1.3	.56	.0
21 11 83 3	-.7	-.05	.65	3.5	35.	-.3	.66	.0
21 11 83 4	-1.0	.05	.71	3.5	33.	-.7	.69	.0
21 11 83 5	-1.6	.17	.68	2.5	34.	-2.3	.74	.0
21 11 83 6	-1.2	.16	.57	3.5	32.	-3.3	.66	.0
21 11 83 7	-1.2	.15	.51	4.7	33.	-1.3	.52	.0
21 11 83 8	-1.1	.12	.49	4.4	33.	-1.3	.51	.0
21 11 83 9	-.9	.08	.45	3.9	32.	-1.3	.48	.0
21 11 83 10	.1	-.13	.44	5.9	32.	-.1	.45	.0
21 11 83 11	.7	-.26	.41	6.1	32.	1.0	.41	.0
21 11 83 12	1.3	-.35	.35	4.4	34.	1.4	.38	.0
21 11 83 13	2.1	-.36	.32	4.4	33.	1.3	.36	.0
21 11 83 14	1.8	-.27	.32	3.5	35.	1.5	.36	.0
21 11 83 15	1.2	-.09	.33	4.9	33.	.8	.37	.0
21 11 83 16	.3	.03	.35	5.1	34.	.0	.39	.0
21 11 83 17	-.7	.15	.38	4.1	35.	-.8	.45	.0
21 11 83 18	-1.1	.15	.42	2.8	32.	-2.3	.51	.0
21 11 83 19	-1.7	.21	.48	2.4	31.	-3.3	.51	.0
21 11 83 20	-2.1	.10	.52	1.6	29.	-4.1	.63	.0
21 11 83 21	-2.6	.35	.58	2.0	36.	-4.5	.69	.0
21 11 83 22	-2.1	.30	.57	2.6	34.	-4.7	.70	.0
21 11 83 23	-2.3	.25	.52	3.0	33.	-4.3	.66	.0
21 11 83 24	-2.4	.25	.55	3.4	33.	-3.2	.63	.0

	T-AS	DT-AS	RH-AS	F-AS	D-AS	T-BR	RH-BR	P-BR
22 11 83 1	-2.7	.27	.56	2.1	34.	-3.3	.68	.0
22 11 83 2	-2.8	.28	.55	2.5	32.	-4.3	.67	.0
22 11 83 3	-2.9	.31	.53	3.1	32.	-6.3	.74	.0
22 11 83 4	-3.0	.25	.63	2.7	32.	-5.3	.67	.0
22 11 83 5	-2.7	.29	.70	3.3	30.	-2.5	.58	.0
22 11 83 6	-2.9	.35	.67	2.3	33.	-3.2	.66	.0
22 11 83 7	-3.1	.37	.64	1.4	32.	-4.3	.76	.0
22 11 83 8	-2.5	.09	.61	2.2	28.	-4.0	.69	.0
22 11 83 9	-2.4	.07	.58	2.3	23.	-2.5	.60	.0
22 11 83 10	-2.3	-.03	.60	3.7	22.	-1.7	.57	.0
22 11 83 11	-1.9	-.02	.60	3.9	20.	-1.3	.58	.0
22 11 83 12	-1.7	-.06	.63	2.0	16.	-1.3	.59	.0
22 11 83 13	-2.1	-.12	.86	1.4	15.	-1.5	.92	.5
22 11 83 14	-1.2	-.31	.91	1.7	1002.	-1.0	.90	.0
22 11 83 15	-3.0	-.07	.90	4.8	35.	-2.3	.87	.0
22 11 83 16	-3.0	.01	.83	5.3	35.	-2.6	.81	.0
22 11 83 17	-3.3	.02	.79	5.3	35.	-2.7	.76	.0
22 11 83 18	-3.1	.10	.76	4.5	35.	-3.1	.76	.0
22 11 83 19	-2.6	.10	.71	3.5	31.	-2.3	.70	.0
22 11 83 20	-2.8	.21	.68	3.4	33.	-2.3	.69	.0
22 11 83 21	-3.0	.25	.63	3.8	34.	-2.6	.64	.0
22 11 83 22	-3.3	.25	.68	3.2	30.	-4.0	.71	.0
22 11 83 23	-2.7	.19	.62	4.4	32.	-2.7	.65	.0
22 11 83 24	-2.3	.13	.54	4.7	33.	-3.3	.65	.0
23 11 83 1	-2.6	.17	.51	3.7	33.	-2.6	.57	.0
23 11 83 2	-3.2	.26	.52	2.7	0.	-3.5	.61	.0
23 11 83 3	-2.8	.21	.48	3.6	33.	-4.3	.58	.0
23 11 83 4	-3.4	.22	.57	2.6	32.	-5.0	.66	.0
23 11 83 5	-3.5	.20	.57	2.9	31.	-5.3	.66	.0
23 11 83 6	-4.4	.25	.69	1.7	32.	-6.7	.76	.0
23 11 83 7	-4.8	.22	.74	1.8	30.	-7.1	.82	.0
23 11 83 8	-5.2	.35	.75	3.1	33.	-7.5	.86	.0
23 11 83 9	-4.9	.58	.75	2.8	32.	-7.5	.89	.0
23 11 83 10	-3.4	.11	.71	2.2	31.	-6.7	.82	.0
23 11 83 11	-2.5	-.41	.69	2.1	33.	-4.3	.69	.0
23 11 83 12	-2.0	-.38	.62	2.4	32.	-2.5	.66	.0
23 11 83 13	-1.7	-.22	.59	2.0	31.	-2.1	.59	.0
23 11 83 14	-1.8	-.09	.54	2.1	34.	-2.2	.58	.0
23 11 83 15	-2.6	.16	.53	1.3	1029.	-2.5	.62	.0
23 11 83 16	-3.5	.35	.59	.8	13.	-3.5	.68	.0
23 11 83 17	-3.2	.30	.59	.8	1004.	-4.2	.73	.0
23 11 83 18	-3.1	.39	.60	.7	10.	-3.8	.75	.0
23 11 83 19	-2.9	.31	.59	.9	23.	-3.7	.78	.0
23 11 83 20	-2.3	.23	.59	1.3	26.	-3.6	.77	.0
23 11 83 21	-1.4	.00	.60	2.7	27.	-2.6	.67	.0
23 11 83 22	-1.2	.01	.59	1.8	27.	-2.5	.71	.0
23 11 83 23	-1.3	.03	.62	2.2	27.	-2.4	.73	.0
23 11 83 24	-1.0	.04	.61	2.6	27.	-2.3	.73	.0
24 11 83 1	-1.7	.29	.64	1.2	25.	-2.5	.77	.0
24 11 83 2	-1.2	.11	.63	2.2	27.	-3.3	.80	.0
24 11 83 3	-1.1	.09	.67	1.8	25.	-3.2	.81	.0
24 11 83 4	-1.6	.24	.72	1.9	23.	-2.6	.83	.0
24 11 83 5	-1.5	.33	.68	2.4	23.	-2.5	.86	.0
24 11 83 6	-.6	.25	.69	2.8	24.	-.3	.75	.0
24 11 83 7	-.9	.32	.75	1.0	33.	.0	.80	.0
24 11 83 8	-1.4	.43	.80	1.0	1023.	-.7	.82	.0
24 11 83 9	-.5	.59	.83	1.6	15.	-1.3	.89	.0
24 11 83 10	1.0	.37	.80	1.5	1024.	.3	.85	.0
24 11 83 11	3.6	-.28	.70	2.0	25.	.4	.87	.0
24 11 83 12	4.2	-.18	.60	2.9	27.	4.0	.69	.0
24 11 83 13	4.1	-.12	.72	5.4	24.	4.7	.68	.0
24 11 83 14	3.9	-.09	.73	5.5	22.	4.7	.71	.0
24 11 83 15	3.7	-.02	.80	4.8	22.	4.5	.73	.0
24 11 83 16	3.4	.03	.83	4.4	23.	4.5	.78	.0
24 11 83 17	3.3	.03	.87	5.1	22.	4.2	.81	.0
24 11 83 18	3.6	.09	.88	4.2	22.	3.6	.86	.0
24 11 83 19	3.8	.06	.88	4.6	22.	4.2	.86	.0
24 11 83 20	3.0	.08	.88	5.0	22.	4.5	.84	.0
24 11 83 21	3.5	.09	.87	5.7	22.	3.7	.84	.0
24 11 83 22	3.0	.11	.87	4.2	22.	3.9	.83	.0
24 11 83 23	3.0	.06	.83	5.3	23.	3.8	.80	.0
24 11 83 24	2.9	.04	.85	5.5	22.	3.7	.79	.0

			T-AS	DT-AS	RH-AS	F-AS	D-AS	T-DR	RH BR	P-BR	
25	11	03	1	3.0	.03	.05	4.2	22.	3.7	.00	.0
25	11	03	2	3.0	.07	.03	4.2	22.	3.5	.02	.0
25	11	03	3	3.4	.05	.03	5.5	23.	3.0	.00	.0
25	11	03	4	3.4	.06	.04	4.5	22.	4.5	.79	.0
25	11	03	5	3.4	.06	.05	5.3	23.	4.4	.79	.0
25	11	03	6	3.5	.04	.05	5.2	23.	4.4	.00	.0
25	11	03	7	3.4	.04	.04	4.5	24.	4.5	.79	.0
25	11	03	8	3.1	.06	.05	3.3	22.	4.1	.00	.0
25	11	03	9	3.0	.06	.04	2.2	22.	3.7	.01	.0
25	11	03	10	3.7	.01	.02	2.6	23.	4.3	.78	.0
25	11	03	11	4.6	-.03	.03	3.3	23.	4.7	.70	.0
25	11	03	12	4.7	-.05	.00	3.0	21.	5.5	.02	.0
25	11	03	13	4.3	.02	.03	1.8	17.	5.3	.05	.3
25	11	03	14	4.1	.14	.08	3.0	20.	1.7	.94	.6
25	11	03	15	4.5	.09	.06	4.5	21.	4.9	.94	.0
25	11	03	16	4.6	.08	.07	4.0	21.	5.3	.94	.0
25	11	03	17	4.7	.04	.07	2.2	15.	5.3	.94	.0
25	11	03	18	4.7	.04	.08	1.3	19.	5.4	.95	.0
25	11	03	19	4.7	.10	.08	1.2	15.	4.0	.97	.0
25	11	03	20	5.1	.09	.08	1.9	17.	4.6	.97	.0
25	11	03	21	5.6	.03	.09	2.0	20.	5.8	.97	.0
25	11	03	22	6.0	.01	1.00	2.6	19.	6.5	.97	.0
25	11	03	23	6.2	.00	.99	1.9	17.	6.7	.97	.0
25	11	03	24	6.4	.00	.97	2.3	15.	6.7	.97	1.7
26	11	03	1	6.5	.00	.99	2.0	15.	6.5	.97	.0
26	11	03	2	6.6	.01	.99	1.4	10.	6.7	.97	.1
26	11	03	3	6.4	.11	.97	.0	1016.	7.0	.97	.0
26	11	03	4	5.0	.51	.98	.5	15.	6.4	.97	.2
26	11	03	5	4.4	.20	.98	2.6	32.	5.6	.97	.0
26	11	03	6	4.0	.05	.98	2.3	32.	5.3	.97	.0
26	11	03	7	3.7	-.01	.98	2.5	32.	4.5	.97	.0
26	11	03	8	3.5	-.03	.98	2.6	33.	4.4	.97	.0
26	11	03	9	3.4	-.05	.98	3.5	33.	4.2	.97	.0
26	11	03	10	3.5	-.08	.98	3.3	32.	4.3	.97	.0
26	11	03	11	3.4	-.10	.98	2.5	33.	4.4	.96	.0
26	11	03	12	3.5	-.13	.98	1.9	34.	4.3	.96	.0
26	11	03	13	4.3	-.24	.98	2.0	34.	3.0	.96	.0
26	11	03	14	3.1	.33	.97	1.2	33.	3.6	.95	.0
26	11	03	15	2.2	.21	.97	1.3	7.	3.5	.95	.0
26	11	03	16	1.2	.40	.96	1.0	2.	2.9	.96	.0
26	11	03	17	.7	.13	.97	1.0	1010.	2.2	.96	.0
26	11	03	18	.2	.26	.97	.8	1032.	1.7	.96	.0
26	11	03	19	.3	.26	.97	2.4	32.	.7	.96	.0
26	11	03	20	.3	.14	.97	3.0	32.	.5	.96	.0
26	11	03	21	-.1	.49	.97	2.9	32.	.5	.96	.0
26	11	03	22	.4	.64	.97	2.5	0.	.6	.96	.0
26	11	03	23	1.5	.37	.97	3.8	2.	1.2	.96	.0
26	11	03	24	2.0	.03	.92	3.6	4.	1.7	.96	.0
27	11	03	1	1.9	-.06	.87	3.5	4.	2.8	.03	.0
27	11	03	2	1.4	-.09	.84	4.2	5.	2.5	.02	.0
27	11	03	3	.0	-.11	.82	4.4	7.	2.1	.01	.0
27	11	03	4	.1	-.11	.82	4.2	5.	1.4	.00	.0
27	11	03	5	-.4	-.13	.82	4.8	5.	.9	.79	.0
27	11	03	6	-1.0	-.14	.81	5.7	4.	.4	.79	.0
27	11	03	7	-1.4	-.14	.81	5.4	5.	-.3	.78	.0
27	11	03	8	-1.7	-.14	.81	5.6	5.	-.5	.79	.0
27	11	03	9	-2.0	-.14	.80	6.1	5.	-.7	.78	.0
27	11	03	10	-2.2	-.14	.79	5.9	4.	-1.0	.78	.0
27	11	03	11	-2.3	-.14	.79	6.0	4.	-.8	.77	.0
27	11	03	12	-2.6	-.18	.78	5.6	3.	-1.4	.75	.0
27	11	03	13	-2.9	-.16	.76	5.7	4.	-1.5	.73	.0
27	11	03	14	-3.0	-.16	.75	5.6	3.	-1.7	.72	.0
27	11	03	15	-3.0	-.14	.72	6.3	3.	-2.0	.71	.0
27	11	03	16	-2.9	-.14	.72	5.6	3.	-2.1	.69	.0
27	11	03	17	2.9	-.12	.70	5.5	3.	-1.8	.68	.0
27	11	03	18	-2.8	-.13	.68	6.2	3.	-1.7	.60	.0
27	11	03	19	-3.1	-.10	.65	6.2	3.	-2.0	.65	.0
27	11	03	20	-3.2	-.09	.60	6.3	3.	-2.3	.63	.0
27	11	03	21	-3.3	-.09	.58	5.2	2.	-2.3	.59	.0
27	11	03	22	-3.5	-.09	.58	5.5	2.	-2.5	.58	.0
27	11	03	23	-3.7	-.09	.57	6.1	1.	-2.6	.56	.0
27	11	03	24	-4.1	-.07	.57	5.9	2.	-2.8	.57	.0

	T-AS	DT-AS	RH-AS	F-AS	U-AS	T-BR	RH-BR	F-BR
28 11 83 1	-4.3	-.06	.57	5.5	1.	-3.5	.58	.0
28 11 83 2	-4.4	-.06	.56	4.6	1.	-3.5	.56	.0
28 11 83 3	-4.3	-.06	.54	4.6	0.	-3.6	.55	.0
28 11 83 4	-4.4	-.03	.52	4.4	0.	-3.5	.52	.0
28 11 83 5	-4.6	-.01	.52	4.4	1.	-3.7	.52	.0
28 11 83 6	-4.8	.00	.54	4.0	36.	-3.9	.52	.0
28 11 83 7	-4.8	.04	.55	3.8	35.	-4.3	.54	.0
28 11 83 8	-5.1	.07	.55	3.6	36.	-4.5	.55	.0
28 11 83 9	-4.8	-.01	.54	3.6	1.	-4.5	.55	.0
28 11 83 10	-4.1	-.16	.53	3.9	1.	-4.3	.53	.0
28 11 83 11	-3.6	-.23	.51	3.9	1.	-3.6	.52	.0
28 11 83 12	-3.3	-.27	.49	3.9	2.	-3.3	.51	.0
28 11 83 13	-3.0	-.27	.48	3.9	2.	-2.5	.49	.0
28 11 83 14	-3.4	-.21	.49	3.8	2.	-2.7	.50	.0
28 11 83 15	-3.9	-.13	.49	3.7	2.	-3.0	.51	.0
28 11 83 16	-4.3	.06	.53	2.7	2.	-3.5	.53	.0
28 11 83 17	-5.5	.12	.54	2.1	2.	-4.4	.55	.0
28 11 83 18	-5.8	.11	.50	2.0	2.	-4.7	.57	.0
28 11 83 19	-5.4	.02	.58	3.7	3.	-5.2	.58	.0
28 11 83 20	-5.7	-.01	.60	3.7	3.	-5.5	.60	.0
28 11 83 21	-6.1	.06	.64	2.7	1.	-5.5	.63	.0
28 11 83 22	-6.4	.14	.67	2.5	1.	-5.8	.69	.0
28 11 83 23	-6.8	.16	.71	1.6	36.	-6.2	.70	.0
28 11 83 24	-6.4	.07	.71	1.9	35.	-6.2	.71	.0
29 11 83 1	-5.9	-.13	.73	1.4	36.	-5.4	.70	.0
29 11 83 2	-5.6	-.13	.72	1.4	1.	-5.3	.71	.0
29 11 83 3	-5.5	-.13	.77	1.8	35.	-4.7	.72	.0
29 11 83 4	-5.5	-.13	.77	2.3	0.	-4.5	.74	.0
29 11 83 5	-5.4	-.14	.78	2.1	0.	-4.6	.73	.0
29 11 83 6	-5.3	-.13	.81	1.3	7.	-4.5	.74	.0
29 11 83 7	-5.1	-.10	.87	1.1	7.	-4.3	.78	.0
29 11 83 8	-5.0	-.09	.90	1.0	7.	-4.3	.84	.0
29 11 83 9	-4.7	-.09	.91	.8	1.	-4.3	.87	.0
29 11 83 10	-4.6	-.11	.93	1.6	1.	-3.7	.90	.2
29 11 83 11	-4.2	-.14	.92	1.8	1.	-3.5	.92	.5
29 11 83 12	-3.8	-.19	.92	1.7	1.	-3.3	.92	.7
29 11 83 13	-3.7	-.19	.92	1.4	0.	-2.9	.92	.6
29 11 83 14	-3.7	-.17	.90	1.3	35.	-2.7	.92	.6
29 11 83 15	-3.7	-.12	.89	1.5	0.	-2.7	.92	.6
29 11 83 16	-3.8	-.09	.94	2.5	35.	-2.6	.92	.4
29 11 83 17	-4.3	.08	.91	1.8	0.	-2.7	.92	.2
29 11 83 18	-4.9	.24	.94	2.7	0.	-3.3	.91	.1
29 11 83 19	-5.0	.23	.93	2.4	1.	-4.4	.92	.0
29 11 83 20	-5.3	.30	.89	2.8	35.	-4.6	.92	.0
29 11 83 21	-5.2	.22	.92	3.4	34.	-4.7	.91	.0
29 11 83 22	-4.6	.03	.92	3.2	34.	-4.5	.92	.0
29 11 83 23	-4.4	-.01	.90	2.8	33.	-3.5	.90	.0
29 11 83 24	-4.3	-.05	.91	3.1	34.	-3.3	.89	.0
30 11 83 1	-4.1	-.05	.88	3.1	35.	-2.8	.88	.0
30 11 83 2	-4.0	-.06	.88	2.8	0.	-2.8	.87	.0
30 11 83 3	-3.8	-.05	.87	2.5	1.	-2.7	.86	.0
30 11 83 4	-3.7	-.06	.83	3.1	2.	-2.6	.84	.0
30 11 83 5	-3.9	-.05	.80	3.5	2.	-2.5	.80	.0
30 11 83 6	-4.2	.00	.81	3.3	2.	-2.5	.78	.0
30 11 83 7	-4.2	-.04	.80	2.9	2.	-2.7	.78	.0
30 11 83 8	-4.2	-.03	.78	3.2	2.	-3.4	.79	.0
30 11 83 9	-4.9	.04	.77	2.6	1.	-3.5	.77	.0
30 11 83 10	-4.6	-.09	.70	2.5	36.	-3.5	.74	.0
30 11 83 11	-4.2	-.27	.74	2.7	35.	-4.4	.76	.0
30 11 83 12	-4.1	-.43	.71	2.6	35.	-3.5	.71	.0
30 11 83 13	-3.5	-.32	.71	3.1	33.	-3.3	.69	.0
30 11 83 14	-4.0	-.27	.73	2.8	32.	-3.0	.71	.0
30 11 83 15	-4.7	-.05	.73	3.0	32.	-4.5	.74	.0
30 11 83 16	-5.9	.22	.80	2.4	32.	-6.2	.84	.0
30 11 83 17	-6.2	.20	.84	3.1	32.	-7.4	.89	.0
30 11 83 18	-7.0	.34	.88	2.6	32.	-7.9	.91	.0
30 11 83 19	-7.0	.33	.91	2.9	31.	-8.4	.92	.0
30 11 83 20	-7.3	.39	.90	3.0	33.	-8.7	.92	.0
30 11 83 21	-7.6	.32	.80	3.1	34.	-8.4	.92	.0
30 11 83 22	-7.9	.29	.90	2.9	33.	-8.9	.92	.0
30 11 83 23	-8.5	.38	.90	2.7	33.	-9.6	.91	.0
30 11 83 24	-8.7	.45	.90	1.9	33.	-9.2	.91	.0
ANT. 99.	0	0	0	0	0	24	6	33
PERCENT 99.	.6	.6	.0	.0	.0	3.3	.9	4.6



NORSK INSTITUTT FOR LUFTFORSKNING

(NORGES TEKNISK-NATURVITENSKAPELIGE FORSKNINGSRÅD)
 POSTBOKS 130, 2001 LILLESTRØM
 ELVEGT. 52.

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RAPPORTTYPE Oppdragsrapport	RAPPORT NR. OR 32/84	ISBN--82-7247-501-4
DATO JUNI 1984	ANSV.SIGN. O.F.Skogvold	ANT. SIDER 68
TITTEL Meteorologiske data fra nedre Telemark høsten 1983		PROSJEKTLEDER B. Sivertsen
		NILU PROSJEKT NR. O-7618
FORFATTER(E) Kjell Skaug		TILGJENGELIGHET** A
		OPPDRAKSGIVERS REF.
OPPDRAKSGIVER SFT, Kontrollseksjonen		
3 STIKKORD (å maks. 20 anslag) Meteorologiske data Statist.bearbeiding		
REFERAT (maks. 300 anslag, 5-10 linjer) Presentasjon av statistisk bearbeiding av meteorologiske data fra nedre Telemark i perioden 1.9.83-30.11.83.		
TITLE Meteorological data from nedre Telemark, autumn 1983		
ABSTRACT (max. 300 characters, 5-10 lines. An evaluation of meteorological data from the southern Telemark area from September 1, 1983 to November 30, 1983 shows autumn wind frequency distribution similar to previous years with dominant winds from the north-northwest. The average wind speed of 3.2 m/s was slightly higher than normal. Whereas Sep. had more rain than usual, Oct. and Nov. had less. Dispersion conditions were close to normal. The monthly average temperature for October was 1.5°C higher than a ten year average, while the September and November averages were close to the ten year average.		

**Kategorier: Åpen - kan bestilles fra NILU A
 Må bestilles gjennom oppdragsgiver B
 Kan ikke utleveres C