

1 **Supplementary Materials**

2 **1 The RAQMS model**

3 Chemical and aerosol forecasts from the Real-Time Air Quality modeling System
4 (RAQMS) were used for flight planning activities during ARCPAC. RAQMS is a
5 unified (stratosphere/troposphere), online (meteorological, chemical, and aerosol)
6 modeling system which has been developed for assimilating satellite observations of
7 atmospheric chemical composition and providing real-time predictions of trace gas and
8 aerosol distributions (Pierce et al., 2007, 2009). The chemical formulation follows a
9 family approach with partitioning on the basis of photochemical equilibrium
10 approximations. The non-methane hydrocarbon (NMHC) chemical scheme is based on
11 the carbon bond lumped structure approach (Pierce et al., 2007). The RAQMS aerosol
12 model incorporates online aerosol modules from GOCART (Chin et al., 2003). Seven
13 aerosol species (SO_4^{2-} , hydrophobic and hydrophilic organic carbon (OC), and black
14 carbon (BC), dust, sea-salt) are transported. RAQMS biomass burning emissions use
15 twice daily ecosystem/severity based emission estimates coupled with MODIS Rapid
16 Response fire detections (Al-Saadi et al., 2008).

17 The RAQMS chemical and aerosol analysis during ARCPAC were conducted at $2^\circ \times 2^\circ$
18 horizontal resolution and included real-time assimilation of cloud-cleared Ozone
19 Monitoring Experiment (OMI) total column O_3 measurements, and stratospheric O_3
20 profiles from the Microwave Limb Sounder (MLS) on the NASA Aura satellite. MODIS
21 aerosol optical depth (AOD) retrievals from instruments onboard the Terra and Aqua
22 satellites were also assimilated. A Mie code based look-up table of speciated aerosol
23 mass extinction coefficients and relative humidity dependent hygroscopic growth factors
24 was used to convert the predicted aerosol mass to speciated extinction, which is
25 integrated vertically to obtain a first guess AOD for assimilation. During the chemical
26 and aerosol assimilation cycle the RAQMS meteorological forecasts are reinitialized
27 from NOAA Global Forecasting System (GFS) analyses at 6 h intervals.

28 **2 Movies of RAQMS constituent evolution and transport**

29 Three Quicktime[®] movies are available in compressed format. The first movie
30 (RAQMS_April_2008_290K_BCOC.mov) shows particulate BC/OC from all sources,
31 the second (RAQMS_April_2008_290K_SO4.mov) particulate SO₄⁼ from all sources,
32 and the third (RAQMS_April_2008_290K_Dust.mov) dust. In each case, the color scale
33 shows the concentration of the constituent of interest on the 290K potential temperature
34 surface. White contour lines show the pressure (hPa) of the 290K isentrope, which
35 intersects the surface (bold white) over southeastern and central Asia and is in the middle
36 troposphere (where most haze layers were observed) over the Arctic. The ARCPAC
37 NOAA WP-3D flights are shown in bold white.

38 **3 Movies of FLEXPART BB and fossil fuel CO**

39 Three Quicktime[®] movies showing FLEXPART simulations of CO transport are
40 available. In the first movie (NH_BB_column_CO_mg_m2_IR.mov), contours indicate
41 the column mass (mg m⁻²) of a FLEXPART passive CO tracer emitted from biomass
42 burning sources (cyan squares) as indicated by MODIS Hotspot Active Fire Detections
43 (made available by the Food and Agriculture Organization of the United Nations (UN-
44 FAO), in partnership with the University of Maryland and NASA MODIS Rapid
45 Response). The underlying infra-red satellite images depict the temperature of the Earth's
46 surface and clouds with blues and greens indicating warmer temperatures and yellows
47 and reds indicating cooler temperatures. These Arctic composite images are produced
48 from geostationary and polar orbiting satellite retrievals by the Space Science and
49 Engineering Center, University of Wisconsin-Madison (funded by the Arctic Natural
50 Science Program, Office of Polar Programs, National Science Foundation Grant ARC-
51 0713843).

52 In the second movie (NH_anthro_column_CO_mg_m2_IR.mov), contours indicate the
53 column mass (mg m⁻²) of a FLEXPART passive CO tracer emitted from anthropogenic
54 sources in Europe, Asia and North America according to the EDGAR 3.2 Fast Track
55 2000 data set, which estimates year 2000 emissions using the EDGAR 3.2 estimates for
56 1995 and trend analyses for the individual countries. EDGAR uncertainty estimates are
57 roughly 50% or greater [Olivier and Berdowski, 2001].

58 The third FLEXPART movie (FLEXPART_BB_CO.mov) shows images of BB
59 emissions and transport as depicted in Fig. 10. Colors are column-integrated values of a
60 20-day conserved CO tracer emitted by BB sources.

61 **4 Methods and uncertainties for aerosol size distributions during** 62 **ARCPAC**

63 Size distributions were measured using 3 instruments during ARCPAC. Particles with
64 diameters from ~ 0.004 to $0.07 \mu\text{m}$ were measured with a 5-channel condensation particle
65 counter (CPC), the nucleation-mode aerosol size spectrometer NMASS (Brock et al.,
66 2000). Particles with diameters from 0.07 to $\sim 0.8 \mu\text{m}$ were measured by an ultra-high
67 sensitivity aerosol spectrometer UHSAS (Cai et al., 2008) operating behind a $1 \mu\text{m}$
68 aerodynamic diameter impactor with an substrate coated with Apiezon Type L grease.
69 Particles with diameters from ~ 0.7 to $8.9 \mu\text{m}$ were measured with a custom-built white-
70 light optical particle counter (WLOPC). The UHSAS and WLOPC sampled in the cabin
71 downstream of the low-turbulence inlet (LTI, Wilson et al. 2004), while the NMASS
72 sampled from a double diffusing inlet in a non-pressurized wing pod. The UHSAS was
73 operated in serial downstream of the dry channel ($<10\%$ relative humidity) of the cavity
74 ringdown aerosol extinction spectrometer. The WLOPC sample stream was maintained at
75 a relative humidity $<40\%$ by heating the sample line.

76 **4.1 UHSAS high gain failure**

77 On two flights during ARCPAC, 2008/04/15 and 2008/04/18, the high gain amplifier of
78 the UHSAS failed for a portion of the flight. These data are irretrievably lost. The times
79 of the failures are from 11:38:52 UTC onward on 2008/04/15, and prior to 01:03:27 on
80 the flight of 2008/04/18.

81 **4.2 UHSAS mass flow controller sensitivity to altitude**

82 The sample flow into the UHSAS instrument is controlled and measured by a mass flow
83 controller that is mounted on the exhaust side of the sample pump. This exhaust mass
84 flow controller was calibrated on the ground before ARCPAC, and the nominal flow rate
85 checked on the ground during the project. After ARCPAC, it was noted that agreement

86 between the NMASS instrument, which measures all particles larger than $\sim 0.004 \mu\text{m}$,
87 was not within expected uncertainties of UHSAS concentrations in cases where all
88 particles were large and should have been measured equally well by both instruments.
89 The mass flow controller (MFC) was then calibrated as a function of sample pressure.
90 The MFC was found to have a pressure dependency that resulted in flow variations of
91 $\sim 30\%$ over the altitude range of the aircraft. There was a consistent discrepancy in
92 concentration between the NMASS and UHSAS as a function of pressure throughout the
93 mission.

94 To try to correct for this large artifact, we have chosen all times in flight in the Arctic
95 when all particles were present in the accumulation mode and should have been counted
96 with unit efficiency by both the NMASS and UHSAS. We have corrected the UHSAS
97 concentrations based on a regression between static pressure and the ratio between the
98 NMASS and UHSAS concentrations (Fig. S1). We estimate the uncertainty in the
99 UHSAS MFC flow as being the sum in quadrature of the basic flow calibration
100 uncertainty for the NMASS and UHSAS, the uncertainty in the regression of the
101 correction curve to the UHSAS flow, and the root-mean-squared deviation of the
102 datapoints from the fit in Fig. S1. The manufacturer's stated accuracy for the MFC is
103 $0.8\% + 0.2\% \times \text{FS}$, where FS is $3.333 \text{ cm}^3 \text{ s}^{-1}$. Typical readings of flow were $0.8 \text{ cm}^3 \text{ s}^{-1}$,
104 so expected accuracy is 1.6%. The total uncertainty in the NMASS concentration is
105 estimated to be 8% based on repeated calibrations between the NMASS and a laboratory
106 CPC which is calibrated using charged particles and an electrometer. The uncertainty in
107 the pressure correction term for the UHSAS is estimated as two times the root-mean-
108 squared residual deviation of the data from the fitted curve in Fig. S1; this uncertainty is
109 14.6%. There are no substantial biases in this deviation. The above errors propagated in
110 quadrature sum to 16.7%. This is a concentration uncertainty, and does not include
111 potential sizing uncertainties, which are described below. To this concentration
112 uncertainty will be added an additional uncertainty due to flow transients during altitude
113 changes as discussed below.

114 **4.3 Transient UHSAS sample flow response to pressure changes**

115 The UHSAS, a commercial instrument, has a total internal instrument volume (optics
116 block, pump, plumbing, filters) estimated to be approximately 1 liter. The aerosol sample
117 flow enters this volume through a small focusing nozzle. The aerosol sample flow rate is
118 not directly measured; instead, the exhaust of the instrument is controlled by a mass flow
119 controller. As the aircraft ascends or descends the mass of air within the instrument must
120 decrease or increase, respectively. The only source for this mass change is through the
121 aerosol inlet, since the exhaust flow controller holds a constant mass flow rate. For
122 example, higher-than-expected inlet mass flows must occur throughout descent, even
123 while the exhaust mass flow controller indicates a constant flow rate. The particle
124 concentration appears to be higher during descents, since more air (and more particles)
125 are entering than expected based on readings from the exit mass flow controller. The
126 opposite is true during ascents. A correction to this issue would be easily calculable,
127 except that the inlet nozzle restricts the airflow entering the optics block, so that there is a
128 time lag between any pressure change and the equilibrium pressure within the UHSAS
129 instrument; this lag is dependent upon the rate of pressure change and the fluid dynamics
130 of the nozzle flow, which is Reynolds number dependent. The transient sample flow
131 effect can be remedied only by directly measuring the sample flowrate entering the
132 instrument, which we intend to do in future projects. We expect that other UHSAS
133 benchtop units (those not within cloud probe canisters) flown on research aircraft exhibit
134 similar sample flowrate problems.

135 To approximately correct for these flow transients, we have applied a correction of +15%
136 and -8% to UHSAS concentrations during aircraft ascents and descents, respectively,
137 based upon observed discrepancies in aerosol concentrations measured by the UHSAS
138 and NMASS (Fig. S2). The residual artifact in the concentration remaining after the
139 ascent/descent flow correction is estimated as up to +10/-5% during ascents, and +5/-10%
140 during descents.

141 **4.4 UHSAS counting statistics**

142 We estimate the uncertainty caused by particle counting statistics during the one-second
143 sample time based upon representative particle size distributions for the different
144 environments encountered during ARCPAC. For a very few cases encountered, particle
145 concentrations were $<30 \text{ cm}^{-3}$, the uncertainties were as large as 22%. Much more typical
146 ($>91\%$ of data on the least polluted Arctic flight, 2008/04/12) concentrations were >200
147 cm^{-3} , in which case counting statistics produced uncertainties $<8\%$.

148 **4.5 UHSAS sizing uncertainties**

149 The particle surface area and volume calculated from the UHSAS measurements depend
150 not only upon the counting accuracy of the instrument, but also upon the sizing accuracy.
151 The instrument is calibrated using ammonium sulfate particles, since their refractive
152 index at $1.053 \mu\text{m}$ lies in the middle of the typical range of refractive indices for
153 atmospheric fine particles composed of mixed sulfate salts and organic components. As
154 composition (and hence refractive index) of the atmospheric aerosol changes, the sizing
155 accuracy of the UHSAS will also change. We estimate the uncertainty in the surface area
156 and volume based upon a simulation of the scattering within the instrument using Mie
157 theory. Current understanding of the refractive index of organic material from secondary
158 organic aerosol formation and from biomass burning sources particles suggests a likely
159 range in the real component of the refractive index of $\sim 1.41\text{-}1.56$ with imaginary
160 components of $<0.01i$ at infrared wavelengths. Accounting for inorganic matter on the
161 particles, we use a real refractive index range of $1.43\text{-}1.56$ for estimating the sizing
162 uncertainties due to refractive index variation (Fig. S3). For particle diameters $<0.5 \mu\text{m}$,
163 which encompass most of the mass and surface area, the actual diameter may deviate
164 from the measured diameter by $+8\text{-}4\%$. Since this is a potential bias rather than a random
165 uncertainty, the errors propagate directly to surface as $+17\text{-}8\%$, and to volume as $+26\text{-}$
166 12% . We have not considered the possible role of incandescence and evaporation of BC
167 particles in the UHSAS, although evidence for this has been observed in the laboratory
168 for nearly pure BC particles (B. Weinzierl, personal communication, 2009).

169 **4.6 Error propagation from inversion of NMASS data**

170 The NMASS measures the concentration of all particles larger than a given diameter
171 using five discrete CPCs that have 50% counting efficiencies of 0.005, 0.008, 0.015,
172 0.030, and 0.055 μm . These data are combined with the UHSAS data using nonlinear
173 inversion technique to recover a size distribution from 0.004-0.07 μm (Brock et al.,
174 1999). The ability of this method to accurately retrieve size distributions is evaluated by a
175 Monte Carlo simulation of the inversion solution while perturbing the input data with
176 experimental uncertainties. For ARCPAC, seven representative size distributions that
177 span the range of observations were tested in the Monte Carlo simulation. Each test case
178 was simulated 1000 times, and the deviation of the retrieved number, surface and volume
179 from the known input size distribution was evaluated. The mean deviation for particle
180 number was a positive bias of +2.8% with a standard deviation of 8.6%; for surface area
181 these values were +0.7% and 1.1%, and for volume they were +0.3% and 0.3% (very
182 little volume is present in the NMASS size range). The uncertainty in total particle
183 number that is caused by inversion uncertainty in the concentration of particles with
184 diameters $<0.07 \mu\text{m}$ is +5.8%/-11.4%. Inversion-caused uncertainties are considered
185 negligible for surface and volume compared with UHSAS uncertainties.

186 **4.7 Total uncertainties in fine particle number, surface, and volume**

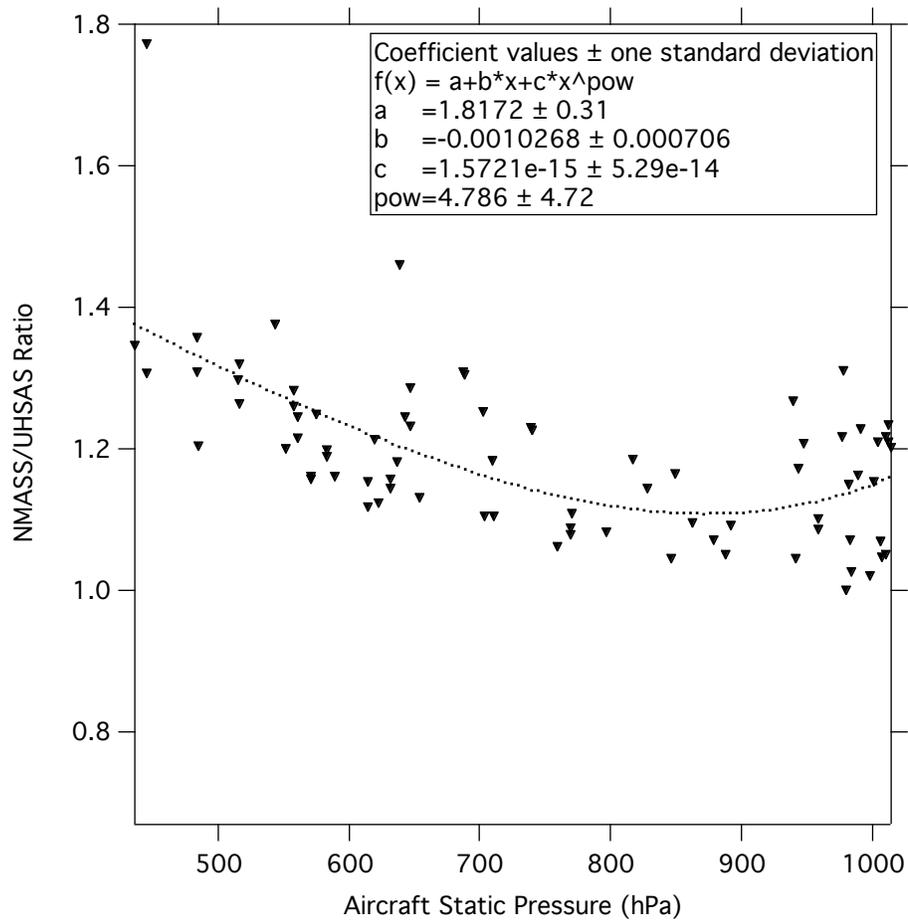
187 Fine particle number concentration uncertainties stem from the concentration uncertainty
188 from the UHSAS following pressure-dependent flow correction, counting statistics, and
189 uncertainties in the concentration due to the inversion. For typical ARCPAC arctic
190 conditions, these sum in quadrature to yield +19%/-22%. During ascents there is an
191 additional potential bias of +10/-5% added, and during descents +5/-10% is added.
192 Uncertainties in surface area and volume include the concentration uncertainties
193 combined linearly with uncertainties from sizing biases, yielding +36%/-27% for surface
194 area and +45%/-31%. During ascents there is an additional potential bias of +10/-5% and
195 during descents +5/-10%.

196 **4.8 Uncertainties in coarse particle measurements**

197 Uncertainties in the WLOPC are caused primarily by counting statistics and by sizing
198 uncertainties. Typical coarse particle concentrations were $<1 \text{ cm}^{-3}$, leading to statistical
199 uncertainties in total coarse number concentration $>12\%$ at the flow rate of $\sim 60 \text{ cm}^{-3} \text{ s}^{-1}$.
200 The uncertainty in number is much worse as particle size increases and particle number
201 concentration falls, leading to very large statistical fluctuations in particle surface and
202 volume. For example, most of the volume is in particles with diameters $>1.5 \text{ }\mu\text{m}$, and the
203 typical concentrations of particles in this size range were $<0.1 \text{ cm}^{-3}$, leading to $\pm 40\%$
204 statistical fluctuations in 1-second number concentrations. Coarse particle counting
205 uncertainties are reduced to $<10\%$ by averaging to 30 s, as was done in the archived data
206 and in the data used in this manuscript. A very few larger particles can contribute
207 substantially to particle surface and volume, however, indicating that yet longer
208 averaging times might be needed to reduce statistical fluctuations in these parameters.
209 Flow calibration uncertainty is $\sim 5\%$.

210 Sizing uncertainties for the WLOPC lead to additional uncertainties in particle surface
211 area and volume. These are difficult to quantify, since the particle refractive index is
212 unknown, and since the shape may not be spherical. Calibration repeatability is $\sim 5\%$ in
213 diameter, and variations in particle size due to refractive index changes, based on Mie
214 simulations of the instrument response, are estimated to be $+15\% / -7\%$ at the peak of the
215 volume distribution ($\sim 3 \text{ }\mu\text{m}$), leading to surface and volume uncertainties of $+32\% / -14\%$
216 and $+52\% / -20\%$, respectively. Resulting total estimated uncertainties in 30-s coarse particle
217 number concentrations are $\pm 11\%$, in coarse surface areas $+48\% / -30\%$, and in coarse
218 volumes $+73\% / -41\%$.

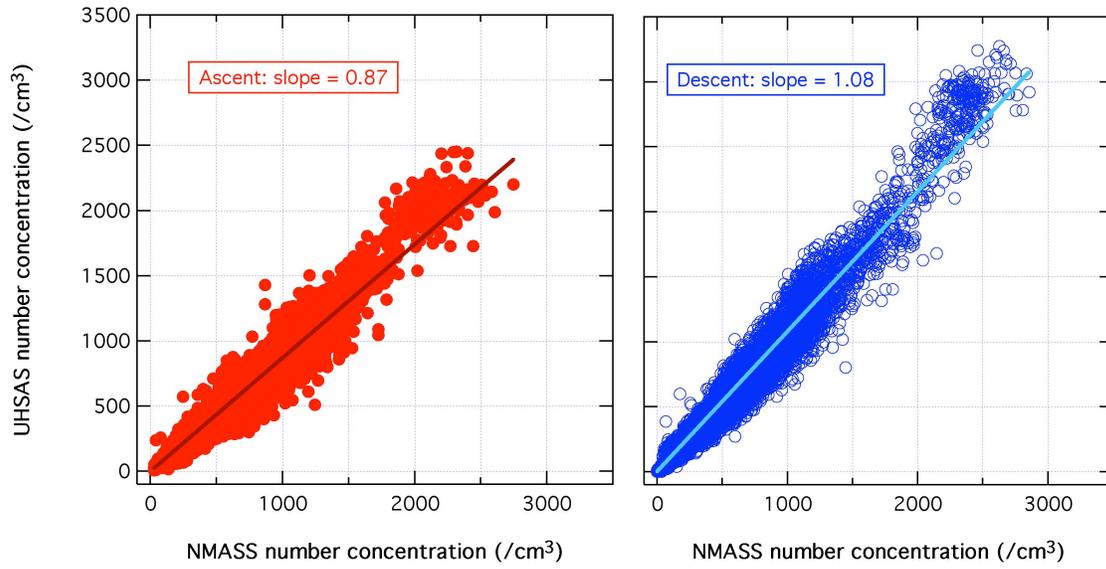
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221 Figure S1. Ratio of concentration of particles with diameters $>0.05 \mu\text{m}$ from the NMAS
222 to the total UHSAS concentration for periods of level flight when all particles are
223 believed to be in the UHSAS size range, as a function of ambient static pressure. The
224 curve is the parameterization used to correct the flow rate of the UHSAS.

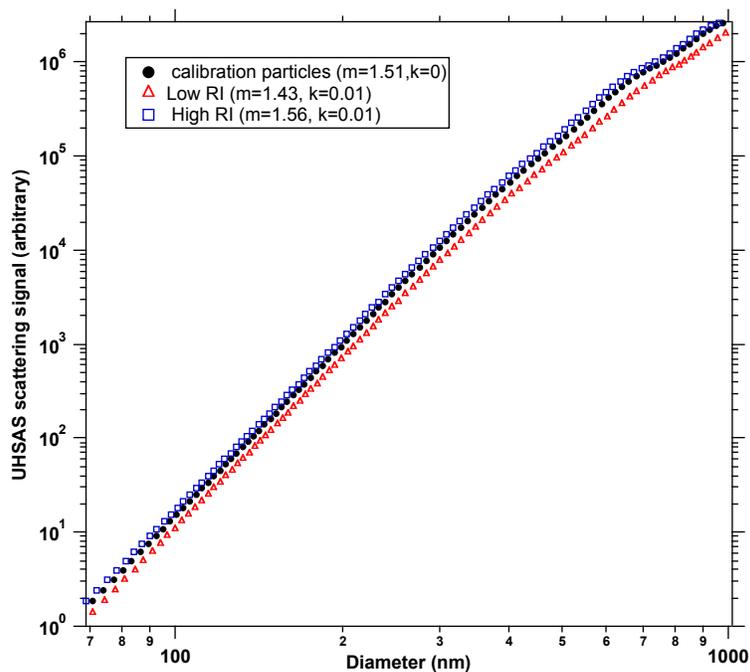
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226 Figure S2. UHSAS concentration plotted as a function of NMASS concentrations during
227 ascents and descents prior to correction. The slope is the correction applied to the data.

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230 Figure S3. Calculated scattered light intensity integrated over the UHSAS optical
231 geometry as a function of particle diameter for three different refractive indices that span
232 the range of likely values in the Arctic environment during ARCPAC. Each point is a
233 sizing bin in the UHSAS.

234 Table S1. Scientific objectives and methods of ARCPAC.

| Goals | Specific questions | Approaches |
|---|--|--|
| Improve understanding of the chemical, optical, and microphysical characteristics of aerosols in the Arctic in springtime. | <ul style="list-style-type: none"> • What is the visible extinction and absorption of the aerosol, and how do these properties vary with relative humidity? • What is the mass concentration and size distribution of BC? • To what extent are BC particles coated with other materials, and do such coatings influence the radiative and cloud-nucleating properties of the BC particles? • What is the contribution of organic material to the optical and chemical properties to the aerosol? • How do aerosol concentrations, composition, optical properties, and cloud nucleating properties above the surface relate to values measured at the surface? • What are the radiative forcings and resulting atmospheric heating rates due to the aerosol, and how do these values compare with those derived from airborne lidar, surface lidar, and surface aerosol measurements? • How do the composition and hygroscopic properties of aerosols relate to chemical processing estimated from trace gases? | <ul style="list-style-type: none"> • Use airborne and remote-sensing measurements since properties aloft are likely decoupled from ground measurements. • Make fast-response remote sensing and in situ measurements because of extreme vertical stratification and non-uniform distribution. • Make accurate and precise measurements of aerosol extinction, absorption, size distribution, composition, BC number and mass, and irradiance. • Measure the variation in optical properties with relative humidity to accurately determine radiative forcing. • Using multi-platform irradiance measurements, determine flux divergence and heating rates; compare with radiative transfer models constrained by in situ measurements |
| Determine the source types (industrial, urban, biomass, dust, sea-salt) of the aerosol components, especially absorbing components. | <ul style="list-style-type: none"> • What are the correlations between aerosol components and trace gases? • How does the composition of the aerosol and trace gases compare to that expected from transport and emission models such as FLEXPART and chemical transport models such as RAQMS? • Does the vertical distribution of aerosol properties reflect differences in source region, transport, and removal? • What are the major sources that contribute to atmospheric and surface BC during the critical springtime warming period? | <ul style="list-style-type: none"> • Make fast-response measurements of key gas-phase and aerosol species to help identify sources. • Use transport and coupled transport/chemistry models to relate the observed aerosol and gas-phase characteristics to sources and transport mechanisms and to evaluate their importance. • Where possible, couple measurements to long-term, ground-based sites to link to established climatologies |
| Determine the microphysical and optical characteristics of representative stratiform clouds in the lower Arctic troposphere in springtime, and evaluate if pollution particles affect these cloud properties. | <ul style="list-style-type: none"> • What is the number density of CCN present in aerosol layers and in clean air, and is there closure between measured CCN and that predicted from the observed aerosol composition and size distribution? • How does the number concentration of CCN, as a function of water supersaturation, vary as a function of altitude? • Is the cloud droplet number concentration in liquid and mixed-phase clouds consistent with that predicted from the observed CCN and cloud cooling rate? • What are the measured solar reflectance and transmission, the IR irradiance, and the effective radius of Arctic clouds, and how do these values vary with CCN and concentration and cloud particle phase? | <ul style="list-style-type: none"> • Measure CCN, aerosol size distribution and composition, and cloud radiative properties above and below stratiform clouds • Use non-soluble gas-phase tracers to correlate aerosol properties outside cloud to determine in-cloud initial values • Use LES and parcel models to elucidate the mechanisms of aerosol perturbation to cloud microphysical and optical properties • Compare observed and modeled values of cloud microphysical and radiative properties |

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- How do directly measured and derived cloud properties compare with remotely measured and derived parameters at the DOE ARM site?
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Improve understanding of halogen chemistry and O₃ budget in the lower troposphere of the Arctic

- What is the distribution of gas phase chlorine and bromine compounds?
 - What is the vertical distribution of sea-salt aerosol and what chemical processing has it undergone?
 - What is the relative importance of the sources of O₃ in the Arctic and subArctic lower troposphere in springtime (production vs. stratospheric vs. long-range transport)?
- Use new in situ techniques to measure Br₂, BrCl, Cl₂, and BrO
 - Sample at low altitude (<100 m) over differing snow and ice surfaces, open leads, ice-filmed leads, and land
 - Use tracer correlations to evaluate O₃ sources and sinks
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